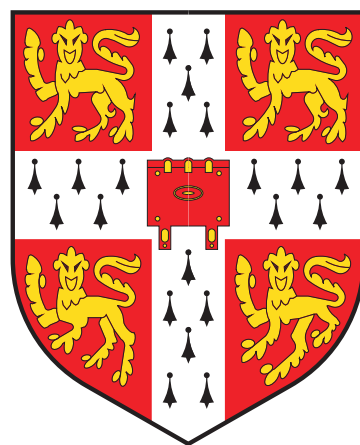# INORGANIC NANOARCHITECTURES BY ORGANIC SELF-ASSEMBLY

A dissertation submitted for the degree of Doctor of Philosophy by

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Foreword by Prof. Ullrich Steiner

The dissertation in a nutshell.

Preface

The focus of this thesis lies in the use of soft matter self-assembly as a design tool for the bottom-up manufacture of functional inorganic nanoarchitectures. Several routes are explored, starting from structure formation of hybrid materials on the 10-nm length scale to their application in photonic and optoelectronic devices. Considering the underlying principles and accomplished results, the outline of the thesis is structured as follows:

Chapter 1 - 4: Introduction to fundamental aspects of experimental and techniques.

Chapter 5 - 7: Material morphology control and implementations in thin-film architectures.

Chapter 8 - 10: Photonic structures designed by soft-matter self-assembly.

The fundamental principles of soft-matter self-assembly are discussed in Chapter 1, including the driving mechanisms for structure formation in block copolymers (BCP), colloidal and hybrid systems as well as their implementation in soft nanotechnology. The optics of thin films and interfaces is subject of Chapter 2, an important aspect of many results presented in the following chapters. Dye-sensitised solar cells were a main device platform for the implementation and validation of the proposed material functionality. Chapter 3 is therefore devoted to explaining the main principles of this photovoltaic concept and describing current challenges for further efficiency improvements. The final chapter of the introductory part, Chapter 4, then represents an overview of the material fabrication and characterisation techniques that were employed in the course of this work.

Experimental results of the doctoral research are presented in Chapters 5 to 10. In Chapter 5 the developed routes for BCP-induced structure control of inorganic nanomaterials are described. These findings were of central importance for many applications presented in the following. The morphological control that is offered by soft matter co-assembly allows to finely control crystallisation and electronic properties of mesoporous networks. This is explored in Chapter 6, which contains the study of crystal growth in BCP-derived TiO_2 nanostructures during high temperature calcination and its effect on the performance of dye-sensitised solar cells. The sacrificial use of organic material suffers from considerable shrinkage, occurring during the several fabrication steps from solution processing of the hybrid mixture to the crystallisation of the inorganic material at high temperatures. In Chapter 7, a protocol is developed that enables to overcome this drawback and allow the formation of sufficiently thick films without the typically occurring crack formation and delamination.

Soft matter self-assembly allows fine tuning of inorganic material formation on the $10 - 500\,\text{nm}$ length scale and therefore enables to design material architectures with interesting photonic properties. This is the motivation for Chapters 7 - 10. Control over sub-wavelength properties, such as pore dimensions, pore volume and film thickness of the resulting inorganic films enabled the stacking of individual mesoporous layers into a multilayer lattice of alternating high and low refractive index, a mesoporous Bragg reflector (MDBR). A BCP-based route to tunable MDBRs is presented in Chapter 8. The combination of BCP and colloidal self-assembly was used to establish a TiO_2 electrode architecture, where a high surface area mesoporous underlayer is coupled to an optically and electronically active three dimensional photonic crystal. This concept is demonstrated in Chapter 9, including the experimental characterisation of such a photonic electrode architecture in terms of light harvesting and device performance in a dye-sensitised solar cell. Detailed control over the pore architecture allowed the fabrication of dielectric thin films with such ultralow refractive indices that they enable the incorporation of high refractive index photocatalytic TiO_2 nanocrystals. A new materials strategy for self-cleaning antireflective coatings is presented in Chapter 10, which is compatible with low processing temperatures and therefore applicable for a variety of substrate materials.

Finally, Chapter 11 concludes the work by summarising the results and identifying possible directions for future studies.

Acknowledgements

A great number of people helped, taught, inspired and cheered me during my doctorate, which made my time in Cambridge only so incredibly enjoyable and successful.

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The Kapitza Building is real hot spot for good science and I want to acknowledge the great help and stimulation I received from the Nanophotonics and Optoelectronics groups. Thanks to Prof. Jeremy Baumberg for generously letting me use the Nanophotonics facilities and advice whenever needed. Niraj Lal was a true buddy inside and outside the optics lab. My desk neighbor Dinesh Kabra was a constant source of happiness and knowledge. The same applies to Sumeet Mahajan, thank you all for your time and helpfulness and the interesting discussions. A number of people helped me improving this dissertation by proofreading and valuable discussions. My gratitude goes to Nicky Humphry-Baker, Alex Finnemore, James Hugall, Kevin Musselman, Matthew Hawkeye and Niraj Lal, your efforts are very much appreciated.

The outcome of this thesis would not have been possible without the excellent collabo-

List of abbreviations

1D	one-dimensional
2D	two-dimensional
3D	three-dimensional
ARC	antireflective coatings
BCC	body-centred cubic
BCP	block copolymer
BET	Brunauer, Emmett &Teller
BJH	Barrett, Joyner & Halenda
DLS	dynamic light scattering
DSC	dye-sensitised solar cell
e^{-1}	electron
EM	electromagnetic
FWHM	full width at half maximum
FTO	fluorine-doped tin oxide
FCC	face-centered cubic
IPCE	incident photon to electron conversion efficiency
MDBR	mesoporous Bragg reflector
NP	nanoparticle
PC	photonic crystal
PEO-*b*-PPO-*b*-PEO	poly(ethylene oxide-*block*-propylene oxide-*block*-ethylene oxide) - Pluronic
PET	poly(ethylene terephthalat)
PHB-*b*-PEO	poly(ethylene-co-butylene-*block*-ethylene oxide) - KLE
PI-*b*-PEO	poly(isoprene-*block*-ethylene oxide)
SAXS	small angle X-ray scattering
SC	simple cubic
SDA	structure directing agent
SEM	scanning electron microscopy
TCE	transparent conducting electrode
TEM	transmission electron microscopy
TGA	thermogravimetric analysis
WAXS	wide-angle X-ray scattering

Contents

Self-assembly of soft matter

Molecular self-assembly is a common principle of structure formation in natural and synthetic materials. This chapter aims to explain the underlying driving forces, from a broad perspective to the specific materials systems used in this work.

Self-assembly is an enticing concept for anyone concerned about how to design and fabricate a materials structure. In a broad sense, the term defines formation processes which are reversible and driven by the cooperative assembly of predefined components into an ordered superstructure [1]. Assembly may occur between molecules, i.e. intermolecular or intramolecular in the form of folding along certain parts of a macromolecule. Furthermore, one may distinguish between static and dynamic self-assembly processes [2]. The former is used for systems that are, once formed, at a global or local equilibrium and therefore stable. Dynamic self-assembly, in contrast, is unstable and only occurs during the dissipation of energy, i.e. in self-organised systems like molecular motors or biological cells.

The driving forces for self-assembly are in general weak, non-covalent, intermolecular forces like van der Waals, electrostatic or hydrophobic interactions as well as coordination or hydrogen bonds. Beyond the molecular level, gravitational attraction, external electromagnetic fields, magnetic, capillary and entropic interactions may be other driving forces for structure formation of mesoscopic or macroscopic objects. The energy dissipated by intermolecular or mesoscopic forces is generally comparable to the thermal energy that allows the system to reach its thermodynamic equilibrium through fluctuations in position and orientation.

1.1   Self-assembly in nature

Figure 1.1 shows three widely recognised examples of static self-assembly occurring in nature: lipid bilayer formation, protein folding and double helix formation of complementary strands of deoxyribonucleic acid (DNA). Phospholipids are the common building blocks for lipid bilayers, shown in Figure 1.1a-d. The macromolecules consist of a polar, hydrophilic head and two apolar, hydrophobic tails. In an aqueous medium, ensembles of phospholipids self-assemble into micellar or bilayer morphologies due to the energetically unfavourable interaction between their apolar tails and the surrounding water. The resulting configuration depends on the balance of energy costs for the exposure of hydrophobic tails at the bilayer's edges as compared to the curvature of the membrane into a closed spherical shape [3]. Lipid bilayers are of central importance in their function as cell membranes in most living organisms.

Protein folding is another phenomenon in biology, where hydrophobicity effect plays a key role for structure formation. The elementary building blocks of proteins are amino acids, whose linear sequence is called the primary structure. Particular sections within the primary structure can be generally distinguished as hydrophobic or hydrophilic, illustrated in Figure 1.1e as black or white spheres. Similarly to phospholipid systems, the molecule is therefore amphiphilic and tends to minimise the number of contact points between the hydrophobic elements of the chain and the surrounding water. This results in intermolecular self-assembly, i.e. folding of the protein into structural motifs, such as α-helices and β-sheets (secondary structure) and further assembly into an energy-minimal global three-dimensional arrangement
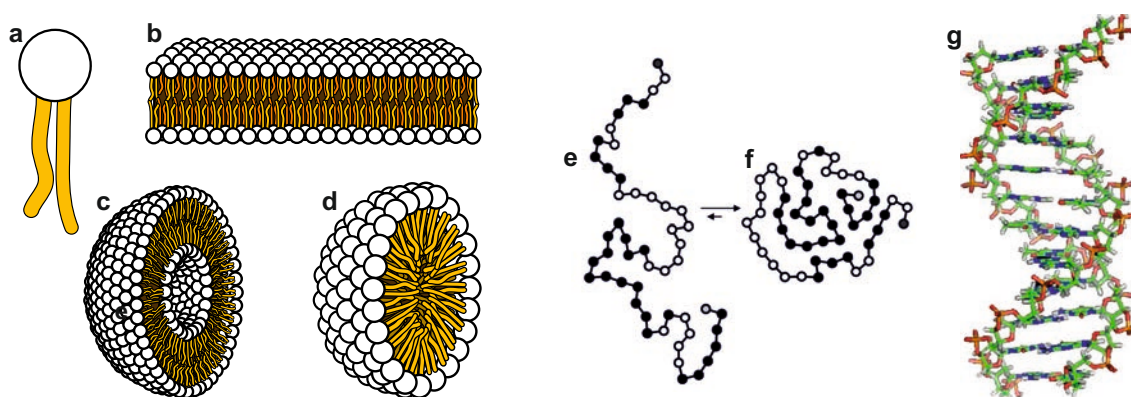
Figure 1.1: **Self-assembly in biological systems. a)** Phospholipid molecules consist of a polar, hydrophilic head and two apolar, hydrophobic tails. Depending on the energy-minimal configuration, ensembles of phospholipids in an aqueous environment self-assemble into **b)** lipid bilayer sheets, **c)** liposomes, **d)** and micelles. **e)** - **f)** Illustration of the protein folding mechanism. **g)** Double helix structure, formed by the self-assembly of two complementary strands of deoxyribonucleic acid. **a) - f)** *reproduced with permission from [4].*

of the chain and its side groups (tertiary structure) [3].

A further prominent example for molecular self-assembly in nature is the formation of DNA into its tertiary structure, the double helix. The driving force for structure formation is the binding of each nucleotide component in a DNA strand with a complementary base pair. Adenine preferentially binds with thymine via two hydrogen bonds, guanine pairs with cytosine via three hydrogen bonds. Continuous hybridisation and melting enables the complementary molecular strands to reach their thermodynamic equilibrium in form of the double helix structure [5].

1.2 Self-assembly in synthetic systems

Advances in chemical synthesis of macromolecules as well as further understanding of structure-function interplay in devices have fostered the field of soft nanotechnology over the last 20 years. In contrast to top-down materials fabrication approaches, such as photon or electron beam lithography, soft nanotechnology relies on the self-assembling nature of synthetically designed building blocks to enable morphology control on the nanometre-scale. The structure formation of homopolymers, block copolymers (BCP) and colloids was of particular importance for this work and will therefore be discussed in the following sections. Other materials systems employed in soft nanotechnology include emulsions [6, 7], synthetic DNA [5, 8, 9] as well as lyotropic [10, 11, 12] and thermotropic liquid crystals [13, 14].

1.2.1 Phase separation of polymer blends

Homopolymers are macromolecules that consist of covalently bonded identical repeat units. The mixing behaviour of a blend of chemically different polymer chains can be well described by a mean free approach, introduced by Huggins [15] and Flory [16] in 1942. The Flory-Huggins equation of the Gibbs free energy $G(T, P)$ for a blend of polymer A and B at temperature T is known as:

$$\Delta G_{\text{mix}} = \Delta H_{\text{mix}} - T \Delta S_{\text{mix}}. \tag{1.1}$$

Accordingly, the thermodynamics of polymer blends is governed by the competing influence of enthalpic and entropic terms in the free energy of mixing. Flory and Huggins approached the change of enthalpy ΔH by a mean-field theory, taking into account possible interaction conformations of neighbouring monomers and their effects on the total enthalpy of the system in a lattice model:

$$\Delta H_{\text{mix}} = f_A f_B \chi_{\text{AB}}, \tag{1.2}$$

where f_A and $f_B = 1 - f_A$ are the occupied volume fractions of polymer A and polymer B, respectively. The dimensionless interaction parameter χ_{AB} is defined as

$$\chi = \chi_{\text{AB}} = \frac{Z}{k_B T}\left(w_{\text{AB}} - \frac{1}{2}(w_{\text{AA}} + w_{\text{BB}})\right), \tag{1.3}$$

where Z is the number of nearest-neighbour contacts, and w_{AB}, w_{AA} and w_{BB} are the interaction energies per monomer between respective monomers[i].

The entropic change ΔS can be described by a combinatorial treatment, in which each monomer occupies a lattice site. The entropy is given by the number of possible arrangements Ω of the involved monomer units under the given boundary conditions

$$S = k_B \ln \Omega. \tag{1.4}$$

Accordingly, the mixing-related gain in entropy due to an increase in spatial uncertainty is

$$\Delta S_{\text{mix}} = -k_B \left(\frac{f_A}{N_A} \ln f_A + \frac{f_B}{N_B} \ln f_B\right), \tag{1.5}$$

with N_A and N_B for the degree of polymerisation of polymer A and polymer B, i.e. the number of subunits per chain.

Inserting the equations 1.2 and 1.5 into equation 1.1 leads to the Flory-Huggins description of the mixing behaviour of polymer blends:

$$\frac{\Delta G_{\text{mix}}}{k_B T} = \chi f_A f_B + \frac{f_A}{N_A} \ln f_A + \frac{f_B}{N_B} \ln f_B. \tag{1.6}$$

Differential calculus of equation 1.6 allows to construct phase diagrams and predict the stability of blends as a function temperature and volume ratio, as shown in Figure 1.2c.

The tendency of long chain molecules to phase separate can be directly recognised from equations 1.2 and 1.5. While the enthalpic term ΔH in equation 1.2 is proportional to the number of monomers, the entropic term is decreased by a factor of $1/N$ compared to a blend of unconnected monomers. A critical value of $\chi_c \cdot N$ can be derived from the differentiation of $\Delta G(f_A, N, \chi)$ for the symmetrical case of $N_A = N_B$. The condition $\chi \cdot N = 2$ separates the situation in which mixtures of all compositions are stable ($\chi \cdot N < 2$) from the situation in which mixtures at some compositions will phase separate ($\chi \cdot N > 2$). Polymers are macromolecules

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[i]In practice χ may have more complex dependence on the temperature, for example $\chi = A/T + B$
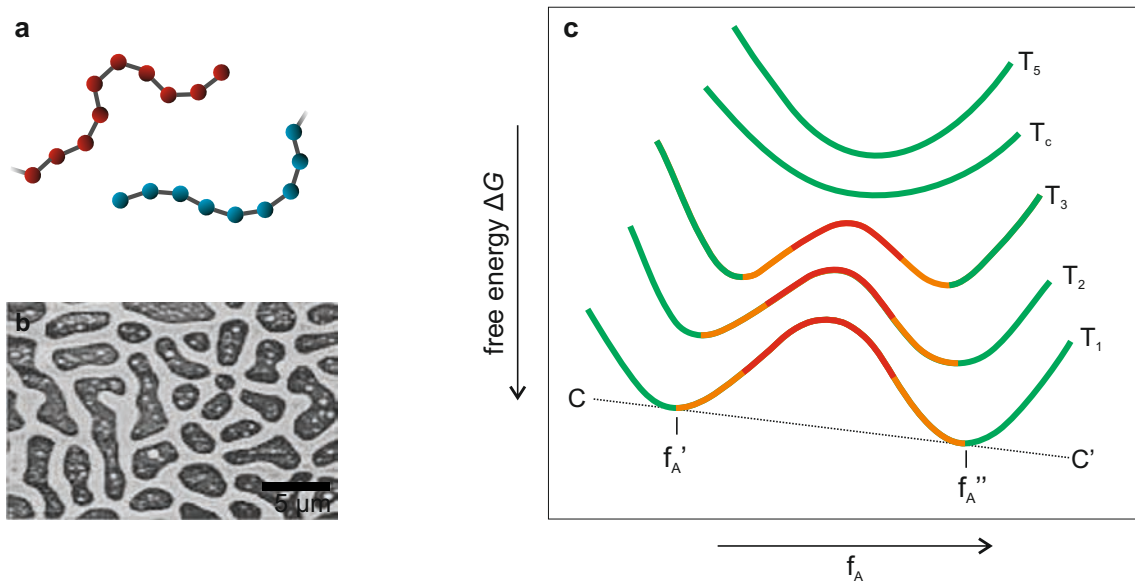
Figure 1.2: **Phase separation of polymer blends. a)** Schematic of two chemically distinct homopolymer chains. **b)** Atomic force microscopy image of a phase separated polymer film, consisting of poly(styrene) and poly(methyl methacrylate)-rich domains. **c)** Stability of a binary polymer blend as a function of temperature and volume composition. Green, orange and red regions indicate stable, metastable and unstable regions, respectively. Below a critical temperature T_c, the tie line $\overline{CC'}$ through the local minima $(\partial \Delta G/\partial f)_{T,p} = 0$ defines the coexisting compositions f'_A and f''_A, which separate the one-phase and two-phase region. For $(\partial^2 \Delta G/\partial f^2)_{T,p} \leq 0$, the blend will spontaneously phase separate into domains with compositions f' and f'' via spinodal decomposition. In the metastable region (orange) phase separation is thermodynamically favourable but hindered by an energy barrier. The so-called binodal decomposition eventually occurs via nucleation and growth. *b) Adapted with permission from [17]. Copyright 1997 American Chemical Society.*

and typically have large values of N. Therefore even a very small positive value of χ, stemming from a very weak repulsive monomer - monomer interaction will result in phase separation of the system [3, 18, 19].

1.2.2 Structure formation in block copolymer systems

BCPs are a subclass of polymers where linear blocks of chemically different monomer units are covalently linked. Depending on the number and arrangement of constituting blocks, a variety of BCP architectures exist, e.g. diblock poly(A-*block*-B), triblock poly(A-*b*-B-*b*-A, A-*b*-B-*b*-C) and starblock copolymers [20]. Due to the covalent bonds of the chemically incompatible blocks, phase separation in BCP systems cannot extend to macroscopic length scales but is restricted to the dimensions of the polymer coil, typically in the range of 5 - 100 nm.

The phase separation of a symmetric BCP A-*b*-B with $f_A = f_B$ into lamellar arrays of A-

rich and B-rich domains is a direct consequence of the spatial constraint to phase separate on the macromolecular length scale. Yet, the theoretical description of the BCP phase behaviour in the melt has to take additional contributions into account which affect the lamellar spacing d. The enthalpic term, favouring the minimisation of interfacial energy, is now counterbalanced by free energy contributions that arise from the maximisation of the chains conformational entropy and, thus, oppose stretching of the chains. This entropic force for an ideal chain can be expressed by a Hookian term, reflecting the chains elasticity $\mathbf{F}_{el} = (3k_B T)/(Na^2)\mathbf{R}$, where $\mathbf{R}$ is the extended end-to-end distance of the chain, and a is a monomer size scale that depends on the local structure of the chain [18].

The sum of interaction and elastic energies per copolymer chain in the strong segregation limit can be described as

$$\frac{G_{\mathrm{LAM}}}{k_B T} = \frac{\gamma \Sigma}{k_B T} + \frac{3(d/2)^2}{2Na^2}. \tag{1.7}$$

The first term accounts for enthalpic interactions that are confined to the A‑B interface, as a product of the interfacial area per chain Σ and the interfacial tension γ, which can be estimated by $\gamma = (k_B T/a^2)\sqrt{\chi}$ according to a classical theory of polymer-polymer interfaces [3]. Σ correlates to the chains fundamental characteristics N and a through the volume filling condition $\Sigma d/2 = Na^3$ (assuming incompressibility).

By minimising Equation 1.7 with respect to d follows an expression for the equilibrium lamellar period (d_0):

$$d_0/2 \sim a\chi^{1/6}N^{2/3}. \tag{1.8}$$

The optimum lamellar domain period therefore scales as the two-thirds power of the copolymer molecular weight, which is in good agreement with experimental results [21].

In contrast to the above described microphase separation, the energy per chain in a homogeneous disordered phase can be approximated by the A‑B contact area:

$$\frac{G_{\mathrm{DIS}}}{k_B T} \approx \chi f_A f_B N = \chi N/4. \tag{1.9}$$

As a direct consequence, the order-disorder transition (ODT) occurs at $G_{\mathrm{DIS}} = G_{\mathrm{LAM}}$, i.e. $N \cdot \chi_{AB} = 10.4$. This is consistent with a more accurate mean field approach, yielding $N \cdot \chi_{AB} = 10.5$.

The outlined theory is a simplification and describes microphase separation adequately in the so-called strong segregation limit ($\chi N > 100$), where the domains are essentially phase-pure and the interfaces sharply defined [22]. In the intermediate segregation regime below $\chi N \sim 100$ the step-like interface blurs out. In the weak segregation limit the polymer concentration ultimately resembles a sinusoidal profile [23]. A unified self-consistent mean-field

approach has been developed that describes the system well in all regimes of χN [24].

Symmetric lamellar domains are in general planar as interface curvature would result in an enthalpic penalty. For a rising volume asymmetry of the blocks, this configuration becomes increasingly unfavourable as longer blocks are more strongly stretched than shorter ones. Curvature of the interface towards the smaller block leads to a reduction of the systems free energy, resulting in a change of morphology from the lamellar phase to a bicontinuous gyroid phase (G), as shown in Figure 1.3a. Further increase of asymmetry causes the formation of an hexagonal arrangement of cylindrical domains (C), followed by a body-centred cubic arrangement of spheres (S), close-packed spheres (CPS) and ultimately a disordered phase for the compositional extremes. The unified self-consistent mean free theory allows to determine the resulting equilibrium morphology as a function of f_A and χN, shown in Figure
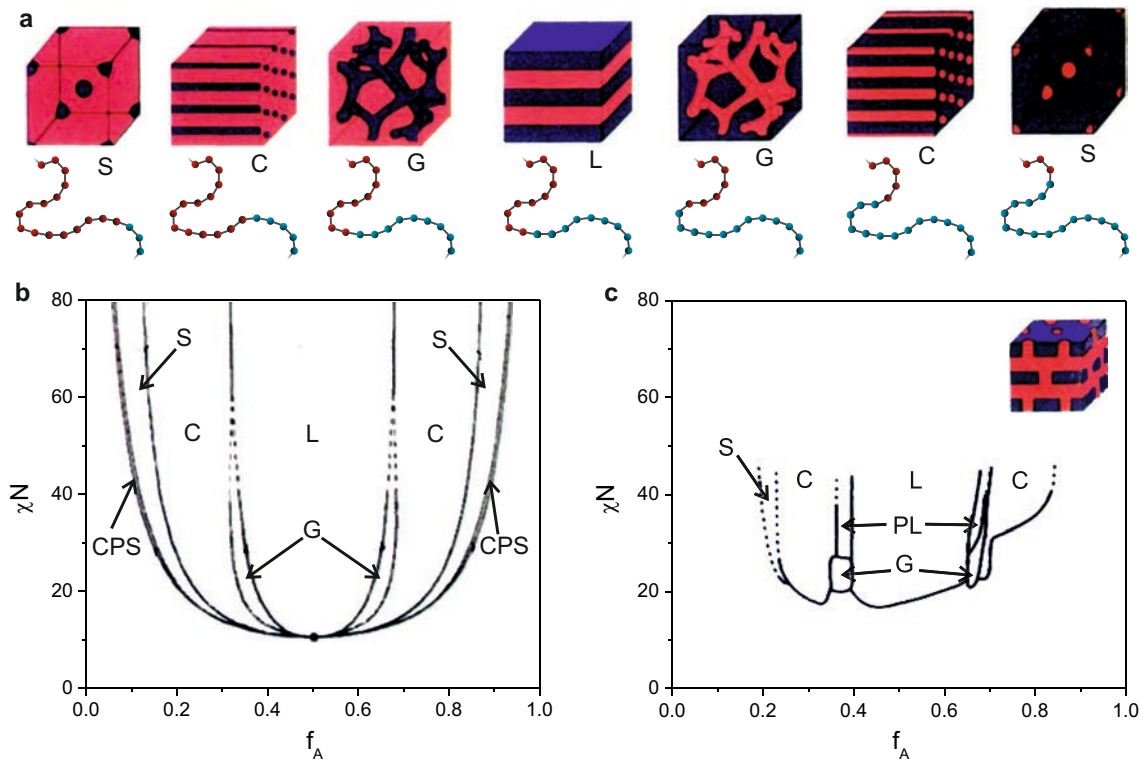
Figure 1.3: **Phase separation of diblock copolymers. a)** Schematic of diblock copolymer chain asymmetry and corresponding morphological arrangement after phase separation. Self-consistent mean-field theory predicts five arrangements at thermodynamic equilibrium with decreasing asymmetry: close-packed spheres (CPS, not shown), body-centred cubic arrangement of spheres (S), hexagonally packed cylinders (C), the gyroid (G) and lamellar phase (L). **b)** The phase diagram can be parameterised by the volume fraction of block A (f_A) and the combined parameter χN. **c)** Experimental data of BCP model systems like poly(isoprene-*b*-styrene) are in good agreement with calculations [25]. ***a) - c)** Adapted with permission from [20]. Copyright 1999 American Institute of Physics.*

1.3b. This is in good agreement with correlated experimental data of amorphous BCP model systems like poly(isoprene-*b*-styrene), compared in Figure 1.3c. Additional phases like the perforated lamellae (PL) or double diamond (D) have been experimentally observed. These morphologies are kinetically long lived and metastable but not in thermodynamic equilibrium [26]. When extending the polymer architecture to three individual blocks, the interplay between AB-, BC- and AC-blocks gives rise to a ternary phase diagram with more than a dozen equilibrium morphologies. [20, 27, 28]

The ability of BCP self-assembly to control material arrangement on the nanometre scale into highly ordered morphologies is promising for technological applications. Many (opto-)electronic devices such as batteries, fuel cells, photovoltaic cells and supercapacitors are highly interface sensitive and rely on efficient transport of charge and chemical reactants on the nanometre scale [29, 30, 31]. Numerous other photonic and biotechnological applications would greatly benefit from one-dimensional arrays [32, 33], interpenetrated networks [34, 35] or chiral material arrangements [36]. Yet, the previously discussed BCP self-assembly mechanisms are generally only valid for the phase separation of amorphous BCPs near thermodynamic equilibrium. Ensuring adequate experimental conditions in thin film processing is particular challenging due to the greatly increased evaporation kinetics and the interaction affinity of one of the blocks with the air or substrate interface [37, 38]. These issues may be circumvented by tuning the chemical properties of the substrate [39, 40], aligning the thin films in an electric field [41, 42] and post-treating the films in a controlled solvent atmosphere [43, 44].

A key challenge that remains for BCP-assembled device applications is the fact that accessible model systems do not exhibit the appropriate functionality. Widely used polymer blocks such as polystyrene, polyisoprene, polyethylene oxide, polymethyl methacrylate or polylactic acid lack photoactivity, conductivity or chemically stability to meet materials requirements in devices. In contrast device-active materials like conjugated polymers are typically stiff, often crystalline and exhibit low N due to the greatly enhanced complexity of chemical synthesis, which poses major obstacles for exploiting BCP microphase separation in functional devices [45, 46, 47].

1.2.3   Block copolymer-directed co-assembly of inorganic material

To-date technological benefit of BCP pattern generation has mostly been achieved by a sacrificial use of the self-assembly process as nanoscale templates to structure inorganic materials in thin films. After phase separation one of the blocks is selectively removed to form a porous template with a well-defined morphology. The pores can then be used as lithographic masks

or refilled with a functional material of choice e.g. by solution impregnation, electrophoretic deposition or atomic layer deposition. This can be extended to a double templating approach in order to obtain the functional material in the complimentary morphology or for backfilling of the array with a second functional material. [48, 49, 50]. While pattern replication by sacrificial templating can be remarkable, fabrication is often complex due to inherent difficulties associated with the infiltration, such as clogging of the pores, the formation of blocking layers or insufficient thermal stability of the polymer mask.

A more direct route is the BCP-directed co-assembly of functional materials. In this case the macromolecules are used as structure-directing agents (SDAs) to guide the nanoscale assembly of inorganic material. After removal of the organic material by etching or high temperature calcination, the inorganic material then resembles the morphology imposed by the structure-directing host. Early approaches were based on low molecular weight cationic surfactants in combination with silicates derived by sol-gel chemistry [10, 11]. Based on Coulomb interactions, the inorganic material was selectively incorporated into the surfactant's polar component. After calcination the silicates exhibited a highly ordered pore structure on the $1 - 10\,\mathrm{nm}$ length scale as a direct consequence of the liquid crystalline array formation of the organic SDA. This concept was subsequently extended to anionic [51] and non-ionic surfactants, i.e. BCPs [52]. The use of BCPs allowed to expand the attainable pore size through the increase in molecular weight and enforce phase separation due to high χ and N of the amphiphilic couples. By employing poly(isoprene-*block*-ethylene oxide) of molecular weight $\geq 10\,\mathrm{kg/mol}$, Wiesner and coworkers managed to overcome micellar material arrangements and reported hybrid morphologies which closely resembled BCP phases at thermodynamic equilibrium, such as lamellae and hexagonally packed cylinders [53].

Several conditions have to be fulfilled in order to reach BCP phase behaviour in a co-assembly approach:

1. Intermolecular forces of the introduced inorganic material, such as Coulomb interactions and hydrogen bonding, need to be selective with one of the BCP's blocks [54].

2. The incorporated inorganic sol has to be small relative to the radius of gyration of the polymer chain to allow incorporation of guest material without perturbing the polymer's chain conformation [55].

3. Microphase separation needs to occur on significantly faster time scales than the competing gelation process of the inorganic material, arising from condensation reactions of the typically prehydrolysed sol. This can be achieved by a sufficiently large χN parameter and a stabilised nanoparticle sol [56].

4. The solvent system has to dissolve all material components and enable even and slow evaporation of the volatile species [57].

Figure 1.4a shows a schematic illustration of the co-assembly process. Intimate mixing on the molecular level of the inorganic component with one of the polymer blocks allows the build-up of a two-domain system with well-defined interfaces [59]. In the example of Figure 1.4b one domain is purely PI, opposing a domain consisting of PEO and aluminosilicate sol [58]. The resulting morphologies can be finely tuned by the volume ratio of PEO and inorganic material in this ternary materials system. Yet, the system can be treated as quasi-binary due to the intimate mixing of PEO and inorganic sol. The ternary system therefore differs from a BCP system with three independent blocks, such as poly(isoprene-*b*-styrene-*b*-ethylene oxide) [28].

A crucial requirement for the final conversion of the hybrid assembly into a purely inorganic array of high structural order is the stability of the inorganic morphology upon removal of the SDA. The guest material therefore needs to form a continuous network which requires to swell the hybrid assembly into the so-called dense nanoparticle regime [58, 60]. Typically, the inorganic guest outweighs the volume fraction of the polymer block it mixes with. While
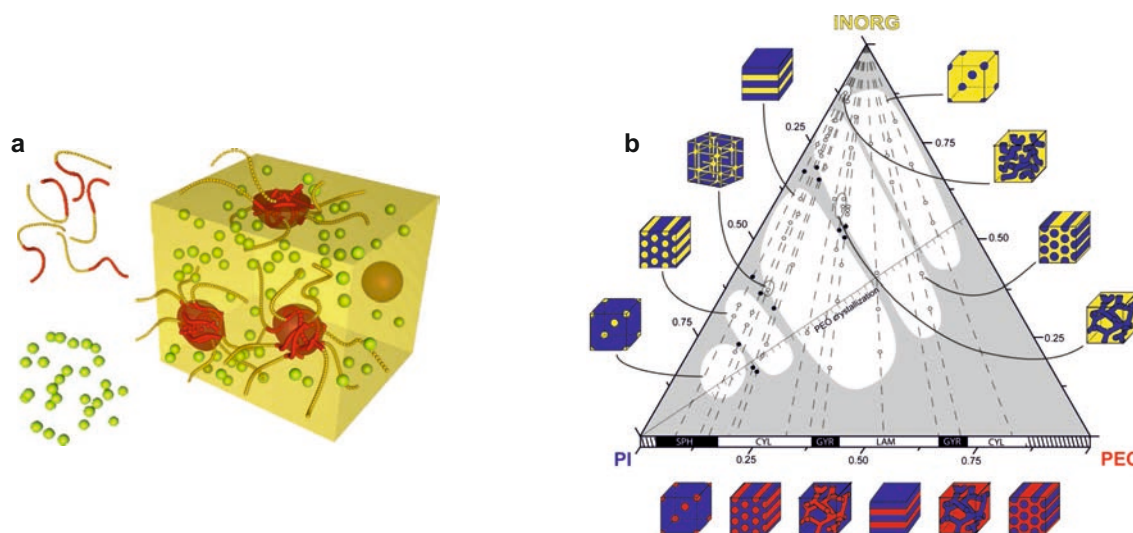
Figure 1.4: **Block copolymer-directed co-assembly of inorganic material. a)** Typically, an amphiphilic BCP and inorganic material in form of a sol are mixed in solution. Upon the evaporation of solvent, the inorganic sol resides in the hydrophilic block due to attractive intermolecular forces. The spatial arrangement of the inorganic guest material is therefore guided by the microphase separation process of the BCP host. **b)** The resulting hybrid morphologies can be mapped in a ternary phase diagram which is parameterised by the volume fractions of organic hydrophobic (PI), organic hydrophilic (PEO) and inorganic component (INORG). ***b)*** *Reprinted with permission from [58]. Copyright 2009 American Chemical Society.*

this is now common practice in experiments, theoretical models still fall short of such high nanoparticle loadings [61, 62]. These are typically based on a combination of polymer self-consistent field theory with density functional theory to account for the mixture of soft, flexible chains with hard interdispersed spheres.

1.2.4   Colloidal self-assembly

The self-assembly of colloidal spheres presents another attractive platform for soft nanotechnology, in particular because colloids can crystallise into highly ordered 2D or 3D arrays.

Colloidal interactions

Colloid-colloid interactions in solution originate from a variety of attractive or repelling intermolecular forces. On the shortest length scale the impossibility of spatial overlap between hard spheres leads to repulsive excluded-volume interactions. Furthermore, entropic forces arise in dense concentrations due to the system's tendency to raise its conformational entropy. In addition, dipole-dipole interactions give rise to van der Waals forces between colloids, as schematically shown in Figure 1.5a. These are prevalent even for particles that have no permanent dipole due to fluctuations in electron density. A temporary dipole can induce a dipole in nearby particles, leading to a short-range attraction. For macroscopic spheres with known material distribution, the overall force can be calculated as the sum of all interacting pairs:

$$U(r) = -\frac{A_H R_1 R_2}{6r(R_1 + R_2)},$$

(1.10)

where r is the distance between the spheres centre of mass, R_1 and R_2 are the radii of the spheres ($r \gg R_1, R_2$) and A_H is the Hamaker constant. A_H is a material property and includes the number of atoms per unit volume and the coefficient of particle-particle pair interaction [63]. The Hamaker theory gives a good approximation but is not exact. A more accurate description, based on quantum field theory, has been developed by Lifshitz [64]. This model takes into account multi-body intermolecular interactions and the finite speed for electric field propagation in a surrounding medium, leading to a retardation effect of the dipole-dipole interaction for larger separations, where $U(r) \sim r^{-7}$. The surface of colloidal particles is typically charged, leading to electrostatic interactions as illustrated in Figure 1.5b. In an electrolyte solution the charges are screened by dissolved ions. These build-up a dense shell (Stern layer) and wider diffuse layer of opposite charges. The electrostatic potential $\Psi(x)$, which is generally given by the Poisson equation for a distribution of net charges, is now affected by the local density of counterions. This leads to the Poisson-Boltzmann equation:

$$\frac{d^2\Psi}{dx^2} = -\left(\frac{zen_0}{\epsilon\epsilon_0}\right)\exp^{-\frac{ze\Psi}{k_BT}}, \tag{1.11}$$

where Ψ is the electrostatic potential, x is the distance from the spheres surface, $z \cdot e$ is the charge of the ions and n_0 is ionic concentration in the bulk solution. In the limit of small Ψ, Debye and Hückel approximated this term with [65]

$$\psi(x) = \psi_0\exp^{-\kappa x}, \tag{1.12}$$

where

$$\kappa = \left(\frac{2e^2n_0z^2}{\epsilon\epsilon_0k_BT}\right)^{1/2}. \tag{1.13}$$

The characteristic length κ^{-1} is known as the Debye screening length. At distances $x \gg \kappa^{-1}$ electrostatic interactions become negligible. For monovalent salts of concentration c (mol/l), the screening length is $\kappa^{-1} = 0.304c^{-0.5}$ nm, thus $\kappa^{-1}_{c=1} = 0.3$ nm and $\kappa^{-1}_{c=0.001} = 9.6$ nm.

Further intermolecular forces develop when the colloidal surfaces are grafted with polymer chains, shown in Figure 1.5c. In a good solvent a repelling force arises for approaching spheres due to an increase of polymer concentration and thus an osmotic pressure in the gap. In contrary, grafted polymers in a poor solvent result in an overall attraction. When polymers are not grafted onto the surface but dissolved in a colloidal solution, approaching spheres will exclude the solute within the gap. The local decrease in osmotic potential leads to a further attraction of the spheres, illustrated in Figure 1.5d.

These origins of intermolecular forces allow to finely tune colloidal interactions by:

  - adjusting the ionic concentration of the electrolyte

  - grafting of polymers onto the colloids surface (short vs. long-chain, low vs. high density, high vs. low solubility)

  - addition of solutes on the intermediate length scale between colloids and solvent molecules

When repulsive interactions are dominant at all separation lengths, colloidal suspensions are stabilised and will not coagulate. For constituents of regular shape and narrow size distribution the evaporation of solvent, i.e. a dramatic increase in concentration can lead to a phase transformation from a disordered arrangement to a crystalline array. The regular packing of colloids into 2D or 3D lattices is a well-established tool in soft nanotechnology. Examples include the use of colloidal arrays as lithographic masks [66] or for a variety of photonic applications [67].
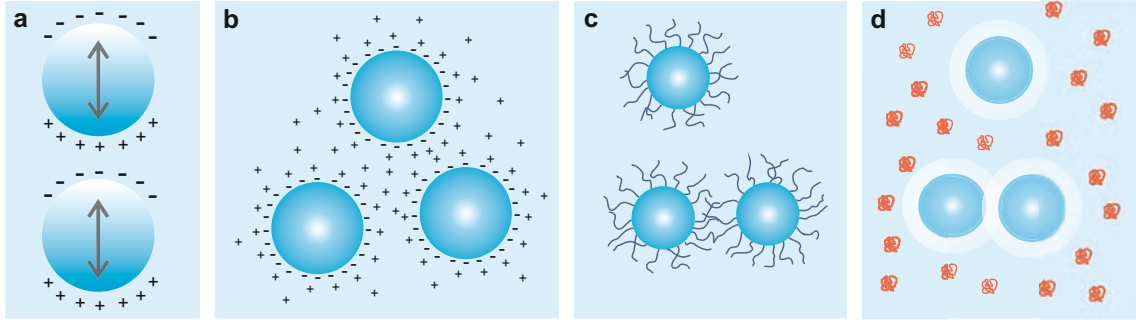
Figure 1.5: **Colloidal interactions. a)** Van der Waals forces (attractive, short range) arise from dipole-dipole interactions due to fluctuations in the electron density. **b)** Electrostatic interactions (repulsive, long range) stem from charge distribution on the colloid surface. The charge compensation can be described as a double layer, consisting of a dense shell (Stern layer) and wider diffuse layer of opposite charges. **c)** Grafted polymer on the colloids surface can lead to a repulsive force upon spatial overlap due to the osmotic pressure arising from the increased polymer concentration. In contrast, a poor solvent will lead to colloidal attraction. **d)** The addition of a solute on the intermediate length scale (i.e. homopolymers) leads to attractive forces due to the osmotic pressure which arises from the exclusion of this component in a depletion zone.

Colloidal self-assembly

While the origin of face-centred cubic (FCC) packing of spheres in 3D is still under debate [68], the formation mechanism in 2D is widely understood and is schematically shown in Figure 1.6 [69]. The ordering process is initiated once the solvent layer thickness is on the order of the particle diameter. Capillary forces arise from the liquid meniscus formed around the partially immersed sphere, which drives nearby spheres into close packing. By variation of particle size, concentration, electrolyte concentration, evaporation rate and surface tension, Denkov *et al.* substantiated that neither electrostatic repulsion nor van der Waals attraction are the main driving forces for the self-assembly [69]. The attractive horizontal force F_x arises from the slope of the three-phase contact line, that leads a variation of the surface tension force along the x-axis [69]:

$$F_x \sim \frac{2\pi\sigma r_c^2}{L} \sin^2(\psi_c) \ \text{ for } \ r_c \ll L \ll \left(\frac{\sigma}{(\Delta\rho)g}\right)^{0.5}, \tag{1.14}$$

where σ is the surface tension of the liquid, r_c is the radius of the three-phase contact line at the sphere's surface and ψ_c is the mean meniscus slope angle at the contact line. The shape of the menisci is described by the Young-Laplace equation and depends on the distance between the colloids as well as the layer thickness l_0 and the particles wettability which is determined by the contact angle α. An additional attractive term related to the higher hydrostatic pressure

in the gas phase than the pressure in the liquid at $z > l_0$ can be neglected on the sub-μm length scale. Similar to the formation of a coffee stain, the pinning of the contact line at the edge of the droplet causes replenishing of the evaporated liquid by flux from the interior. This leads to convective transport of spheres to the outer edge of the suspension droplet, which drives further assembly (shown in Figure 1.6b) [70].

For the deposition of highly ordered colloidal arrays in 3D, the vertical evaporation-induced self-assembly method introduced by Colvin *et al.* has proven most effective [71]. A schematic is shown in 1.6c. The underlying formation mechanism that drives the colloids into a multi-layered FCC lattice arrangement remains unclear. Norris *et al.* hypothesised that solvent flow through the interstitial spaces of closed-packed spheres play a major role in the evaporation-induced opal growth [68]. The flow, driven by the capillary suction of the menisci, may draw the spheres into the interstitial spaces, i.e. lead to the close packing in the thermodynamically favourable FCC lattice, even though the process takes place at non-equilibrium conditions. The origin of the high crystal quality in this vertical deposition technique may be due to the fact that concentration, rearrangement and lattice formation of the spheres all occurs simultaneously, which is fundamentally different to the horizontal capillary deposition described previously. Alternative methods for 3D colloidal crystallisation include field-induced, flow-induced and restricted-volume deposition [72]. Yet, the vertical deposition method is to-date considered to deliver the highest crystal quality [67].

While the assembly of sub-μm sized colloidal spheres in a FCC crystal represents a 3D dielectric lattice, the architecture does not allow the formation of a full photonic band gap [73]. Infiltrating the structure with materials of refractive index $n > 2.8$ and subsequently removing the spheres can result in an inverse opal structure that inhibits photon propagation in a certain frequency range [74]. This can be achieved by physical infiltration, i.e. impregnation of the structure with nanoparticles or molecular solutions as well as materials growth in the porous network by chemical reactants, such as atomic layer, chemical vapour, sol-gel or electrochemical deposition (chemical infiltration) [67]. Material infiltration does not only offer the possibility to increase the dielectric contrast but also allows the incorporation of active elements.

The stepwise assembly, drying and infiltration of colloidal arrays typically leads to significant volume contraction in the fabrication process, which can result in cracking and loss of long range order. A promising route to somewhat circumvent this problem is the simultaneous co-assembly of spheres and inorganic material. In this case, convective flow drives the guest material into the interstitial pores during the self-assembly process. Subsequent removal of the polymer spheres then leads directly to an inverse opal structure [75, 76].

The "Holy Grail" for self-assembled materials with enhanced optical response would be
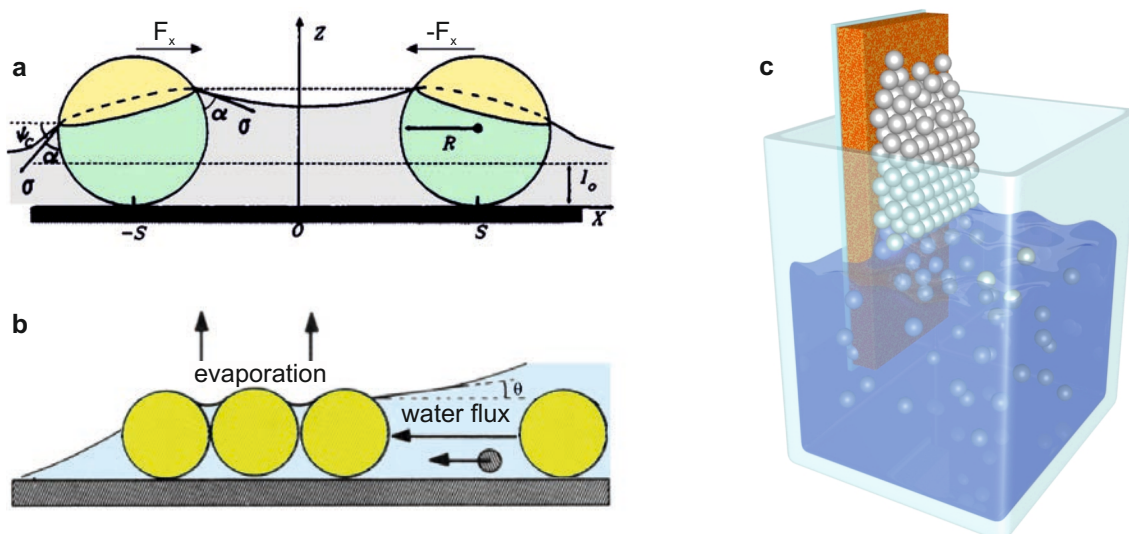
Figure 1.6: **Colloidal interaction and evaporation induced self-assembly. a)** Capillary forces lead to the attraction of nearby spheres when partially immersed in a liquid. **b)** Pinning of the contact line leads to convective transport of spheres to the edge of the suspension, which drives further assembly. **c)** The so-called evaporation-induced self-assembly method leads to the crystallisation of spheres into a three dimensional FCC lattice. Capillary forces are driving the spheres to the meniscus formed between the solution and the vertical substrate, whereas repulsive entropic and electrostatic forces between the spheres facilitate movement and therefore formation of the energetically favoured FCC structure. ***a), b): Adapted with permission from [69]. Copyright 1992 American Chemical Society.***

the assembly of a diamond structure, i.e. a FCC crystal with a base of two constituents. From a photonic crystal perspective, this is widely seen as ideal structure, offering the possibility of a full photonic band gap in the visible range already for opaline arrays [67, 77]. Pathways have been proposed by using oppositely charged particles [78] or a binary mixture of colloidal spheres with selective etching properties [79, 80], but experimental realisations have not been shown.

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Optical aspects of thin films and interfaces

Much of the presented work has been devoted to the design of photonic structures by soft matter self-assembly. This chapter shall give a general introduction to the optics of thin films and interfaces and furthermore explain the main concepts and techniques that were used to analyse the experimental results.

2.1 Propagation of light at an optical interface - reflection and refraction

The propagation of electromagnetic (EM) waves in an optical medium is fully described by the four Maxwell equations, in the classical limit [1]. This leads to boundary conditions for the parallel ($\parallel$) and perpendicular ($\perp$) field components which need to be met when a beam of light hits a planar interface between two homogeneous lossless dielectric media with permittivity ϵ_1 and ϵ_2, and permeability μ_1, and μ_2, as illustrated in Figure 2.1a [2].

$$\epsilon_1 E_1^{\perp} = \epsilon_2 E_2^{\perp} \tag{2.1}$$

$$B_1^{\perp} = B_2^{\perp} \tag{2.2}$$

$$\mathbf{E}_1^{\parallel} = \mathbf{E}_2^{\parallel} \tag{2.3}$$

$$\mathbf{B}_1^{\parallel}/\mu_1 = \mathbf{B}_2^{\parallel}/\mu_2. \tag{2.4}$$

These four equations 2.1-2.4 are the basis for the theory of reflection and refraction at optical interfaces. With a monochromatic planar incident wave of form $E_i = E_{0,i} \exp[i(\mathbf{k}_i \mathbf{r} - \omega_i t)]$ one can derive from equation 2.3 the law of reflection [3]:

$$\theta_i = \theta_r = \theta_1, \tag{2.5}$$

as well as Snell's law of refraction:

$$n_1 \sin \theta_1 = n_2 \sin \theta_2. \tag{2.6}$$

The relative amplitudes of incident, reflected and refracted waves depend on their polarisation with respect to the plane of incidence. Incoming light can be decomposed into orthogonal and linearly polarised waves, with $\mathbf{E}$-field components perpendicular ($\mathbf{E}_s$) and parallel ($\mathbf{E}_p$) to the plane of incidence. Based on equations 2.3 and 2.4 the so-called Fresnel coefficients can be derived:

$$r_s = \frac{E_{r,s}}{E_{i,s}} = \frac{n_1 \cos \theta_1 - n_2 \cos \theta_2}{n_1 \cos \theta_1 + n_2 \cos \theta_2}, \tag{2.7}$$

$$t_s = \frac{E_{t,s}}{E_{i,s}} = \frac{2 n_1 \cos \theta_1}{n_1 \cos \theta_1 + n_2 \cos \theta_2}, \tag{2.8}$$

$$r_p = \frac{E_{r,p}}{E_{i,p}} = \frac{n_2 \cos \theta_1 - n_1 \cos \theta_2}{n_2 \cos \theta_1 + n_1 \cos \theta_2}, \tag{2.9}$$

$$t_p = \frac{E_{t,p}}{E_{i,p}} = \frac{2 n_1 \cos \theta_1}{n_2 \cos \theta_1 + n_1 \cos \theta_2}. \tag{2.10}$$

Figure 2.1b shows the corresponding reflectance $\mathcal{R}$ and refraction, i.e. transmittance $\mathcal{T}$, at a air-glass interface with $\mathcal{R}_{s,p} = r_{s,p}^2$ and $\mathcal{T}_{s,p} = (n_2 \cos \theta_2 / n_1 \cos \theta_1) \cdot t_{s,p}^2$, respectively. The Brewster angle θ_B follows from $r_p = 0$ and Snell's law with $\theta_B = \arctan(n_2/n_1)$.
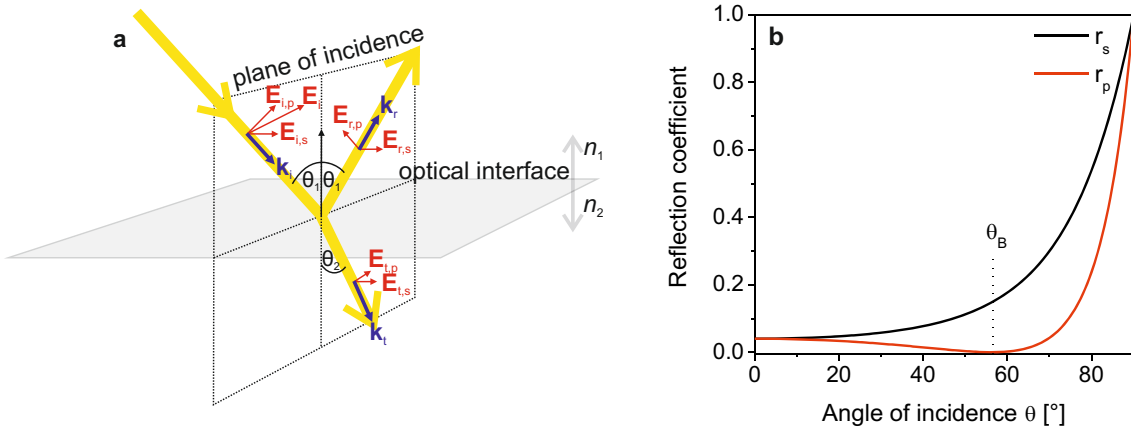
Figure 2.1: **Reflection and refraction at an optical interface. a)** Incident ($\mathbf{E}_i$, $\mathbf{k}_i$), reflected ($\mathbf{E}_r$, $\mathbf{k}_r$) and refracted ($\mathbf{E}_t$, $\mathbf{k}_t$) EM waves at the interface between two homogeneous, isotropic and lossless dielectric media. The electric field can be decomposed into parallel ($\mathbf{E}_p$) and perpendicular ($\mathbf{E}_s$) components with respect to the plane of incidence. **b)** Reflection coefficients at an air-glass interface for parallel (r_p) and perpendicular (r_s) polarised incident light as a function of angle of incidence (θ). At the Brewster angle $\theta_B = 56.5°$ all parallel polarised light is refracted ($r_p = 0$), i.e. the reflected light is fully polarised perpendicularly to the plane of incidence.

2.2   Thin film interference

The characteristic reflection of a thin film is the consequence of multiple beam interference. As shown in Figure 2.2a, the presence of two optical interfaces, each with its characteristic Fresnel coefficients for reflection and transmission, results in a division of the incident beam into a multitude of coherent waves. If the reflection coefficients are non-negligible, this results in a number of higher order reflected waves that all contribute to the colour appearance of the film, a characteristic of its thickness (h_{film}) and refractive index (n_1). The optical path difference Δ of two adjacent rays is given by:

$$\Delta = 2n_1 h_{\text{film}} \cos\theta_1, \tag{2.11}$$

with a corresponding phase shift $\phi_m = (m+1)\cdot(2\pi/\lambda)\cdot\Delta$, where m is the number of total internal reflections. $\mathbf{E}_1$ is therefore out-of-phase by 180° compared to all higher order reflected waves ($\mathbf{E}_2$, $\mathbf{E}_3$, ...), where m is always an odd number. The resulting overall amplitude is then given by a geometric series, where r_{ij} and t_{ij} correspond to the Fresnel coefficients at the optical interface i and j denoted in order of the propagation direction of the ray [4]. This applies for perpendicular polarisation (with $r_{\text{s},ij}$ and $t_{\text{s},ij}$) and parallel polarisation (with $r_{\text{p},ij}$ and $t_{\text{p},ij}$).

$$\frac{E_\text{r}}{E_0} = r_{01} + t_{01}r_{12}t_{10}\exp^{-2i\phi}\sum_{n=1}^{\infty}(-1)^n(r_{12}r_{10})^n\exp^{-2in\phi}$$

$$\tag{2.12}$$

$$= r_{01} + \frac{t_{01}r_{12}t_{10}\exp^{-2i\phi}}{1 + r_{10}r_{12}\exp^{-2i\phi}} = \frac{r_{01} + r_{12}\exp^{-2i\phi}}{1 + r_{10}r_{12}\exp^{-2i\phi}},$$

with $t_{01}t_{10} = \sqrt{1 - r_{01}^2}\sqrt{1 - r_{10}^2} = 1 - r_{01}^2$, assuming lossless dielectric media. The reflectivity of a thin film is then given by

$$\mathcal{R} = \frac{I_\text{r}}{I_0} = \frac{\left(r_{01} + r_{12}\exp^{-2i\phi}\right)\left(r_{01} + r_{12}\exp^{2i\phi}\right)}{\left(1 + r_{01}r_{12}\exp^{-2i\phi}\right)\left(1 + r_{01}r_{12}\exp^{2i\phi}\right)}$$

$$\tag{2.13}$$

$$= \frac{r_{01}^2 + r_{12}^2 + 2r_{01}r_{12}\cos 2\phi}{1 + r_{01}^2 r_{12}^2 + 2r_{01}r_{12}\cos 2\phi}.$$

For illustration, a computer-simulated colour reflection of a thin water film is shown in Figure 2.2. According to equation 2.11, the conditions for multiple beam interference depend on the film thickness (h) and the angle of inclination (θ), here plotted in polar coordinates.
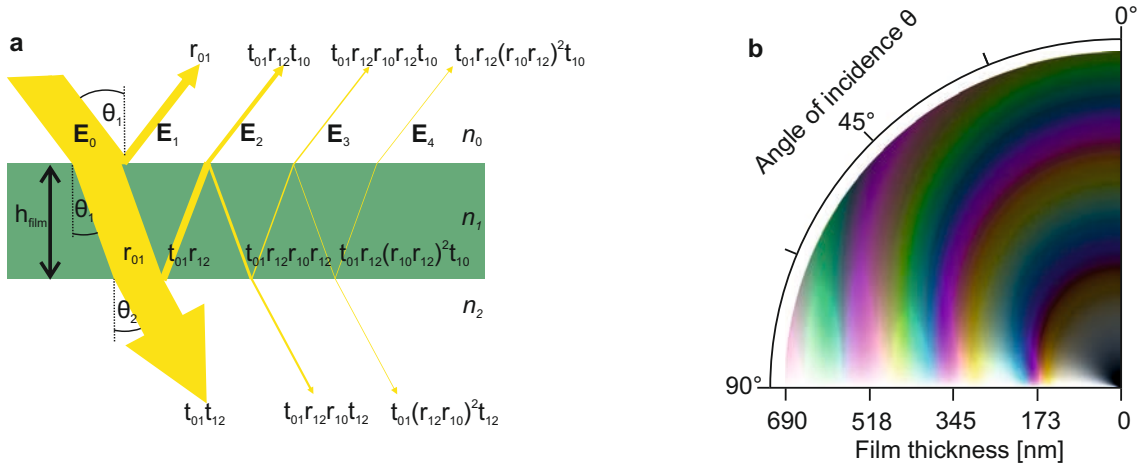
Figure 2.2: **Thin film interference. a)** The Fresnel equations determine the reflection and transmission coefficients of EM waves at each optical interface. The overall reflectivity of a thin film is therefore a superposition of a multitude of beams with different optical paths. **b)** Computer-simulation illustrating the colour reflection of a thin water film plotted in polar coordinates as a function of the film thickness (r) and the angle of incidence (θ) for unpolarised standard daylight illumination (D65). *b) Reproduced with permission from [5].*

2.3 Model of multilayer reflectivity

2.3.1 Rouard's method

The optical response of a multilayer stack, i.e. a layer sequence of thin films, results from the reflection and refraction characteristics at each of its optical interfaces. In analogue to the mathematical treatment for thin film interference, Rouard extended the method of summation from one layer with two interfaces to k layers and $k + 1$ interfaces in a step-wise procedure [4, 6]. Following his technique the optical properties of the kth individual layer (in terms of reflection coefficient and accompanying phase change) at the bottom of the stack are replaced by a single surface with the appropriate characteristics. This is then incorporated into the calculation for the adjacent $(k - 1)^{\text{th}}$ layer and so on. Based on equation 2.12 it follows for the amplitude ρ_k and phase δ_k of the light reflected from the kth layer:

$$\rho_k \exp^{i\delta_k} = \frac{r_k + r_{k+1} \exp^{-2i\phi_k}}{1 + r_k r_{k+1} \exp^{-2i\phi_k}}. \tag{2.14}$$

The kth layer is subsequently treated as a surface with the effective Fresnel coefficient $\rho_k \exp^{i\delta_k}$. The parameter ρ_k can be calculated via the complex conjugate

$$\rho_k^2 = \frac{r_k^2 + r_{k+1}^2 + 2r_k r_{k+1} \cos 2\phi_k}{1 + r_k^2 r_{k+1}^2 + 2r_k r_{k+1} \cos 2\phi_k}. \tag{2.15}$$

δ_k can be written as [4]

$$\delta_k = \eta_k - \xi_k, \tag{2.16}$$

with

$$\tan \xi_k = \frac{r_{k+1} \sin 2\phi_k}{r_k + r_{k+1} \cos 2\phi_k} \tag{2.17}$$

and

$$\tan \eta_k = \frac{r_k r_{k+1} \sin 2\phi_k}{1 + r_k r_{k+1} \cos 2\phi_k}. \tag{2.18}$$

For the adjacent $(k-1)^{\text{th}}$ layer this results in

$$\rho_{k-1} \exp^{i\delta_{k-1}} = \frac{r_{k-1} + \rho_k \exp^{-i\delta_k} \exp^{-2i\phi_{k-1}}}{1 + r_{k-1}\rho_k \exp^{-i\delta_k} \exp^{-2i\phi_{k-1}}}, \tag{2.19}$$

where ρ_{k-1} and δ_{k-1} can be calculated accordingly following equations 2.15 - 2.18. This process is repeated k-times to obtain the reflection coefficient of the overall system ρ_1.

2.3.2   Transfer matrix method

An alternative route to calculate the optical response of a multilayer stack is the so-called transfer matrix approach, which relates the electric and magnetic field at both interfaces of an optical element via a characteristic matrix [7, 8]. Assume an incoming beam at normal incidence and a single layer of optical thickness l in-between two optical media, i.e. a sequence media 0 | layer 1 | media 2. The boundary conditions, introduced in equations 2.1-2.4, have to be fulfilled at interface 01:

$$E_{0\text{i}} + E_{0\text{r}} = E_{1\text{i}} + E_{1\text{r}} \tag{2.20}$$

$$n_0 E_{0\text{i}} - n_0 E_{0\text{r}} = n_1 E_{1\text{i}} n_1 E_{1\text{r}}, \tag{2.21}$$

and at interface 12:

$$E_{1\text{i}} \exp^{ikl} + E_{1\text{r}} \exp^{-ikl} = E_t \tag{2.22}$$

$$n_1 E_{1\text{i}} \exp^{ikl} - n_1 E_{1\text{r}} \exp^{-ikl} = n_2 E_t. \tag{2.23}$$

This set of equations can be combined to

$$1 + \frac{E_{0\text{r}}}{E_{0\text{i}}} = \left(\cos kl - i\frac{n_2}{n_1} \sin kl \right) \frac{E_t}{E_{0\text{i}}} \tag{2.24}$$

$$n_0 - n_o \frac{E_{0\text{r}}}{E_{0\text{i}}} = \left(-in_1 \sin kl + n_2 \cos kl \right) \frac{E_t}{E_{0\text{i}}}, \tag{2.25}$$

or equivalently in a matrix representation

$$\begin{pmatrix} 1 \\ n_0 \end{pmatrix} + \begin{pmatrix} 1 \\ -n_0 \end{pmatrix} \frac{E_{0r}}{E_{0i}} = \begin{pmatrix} \cos kl & (-i/n_1)\sin kl \\ -in_1 \sin kl & \cos kl \end{pmatrix} \begin{pmatrix} 1 \\ n_2 \end{pmatrix} \frac{E_t}{E_{0i}}. \tag{2.26}$$

For clarity, equation 2.26 can be written as

$$\begin{pmatrix} 1 \\ n_0 \end{pmatrix} + \begin{pmatrix} 1 \\ -n_0 \end{pmatrix} r = M \begin{pmatrix} 1 \\ n_2 \end{pmatrix} t, \tag{2.27}$$

where r is the reflection coefficient, t is the transmission coefficient and M is the transfer matrix. The extension to the optical response of N-layers is then accordingly

$$\begin{pmatrix} 1 \\ n_0 \end{pmatrix} + \begin{pmatrix} 1 \\ -n_0 \end{pmatrix} r = M_1 M_2 M_3 ... M_N \begin{pmatrix} 1 \\ n_2 \end{pmatrix} t = M_{tot} \begin{pmatrix} 1 \\ n_2 \end{pmatrix} t, \tag{2.28}$$

where M_{tot} is the product of the individual transfer matrices.

A multilayer stack of particular interest is a distributed Bragg reflector (DBR), which consists of an periodic sequence of high and low refractive index layers. Strong reflection arises when all reflected beams are of equal phase and therefore interfere constructively at the front surface. This is fulfilled for $n_{low}h_{low} = n_{high}h_{high} = \lambda/4$. DBRs are therefore typically denoted as quarter-wave stacks [9]. The product of two adjacent transfer matrices is therefore

$$\begin{pmatrix} 0 & -i/n_{low} \\ -in_{low} & 0 \end{pmatrix} \begin{pmatrix} 0 & -i/n_{high} \\ -in_{high} & 0 \end{pmatrix} = \begin{pmatrix} n_{high}/n_{low} & 0 \\ 0 & -n_{low}/n_{high} \end{pmatrix}, \tag{2.29}$$

and correspondingly for the overall optical element with $2N$ layers

$$M = \begin{pmatrix} n_{high}/n_{low} & 0 \\ 0 & -n_{low}/n_{high} \end{pmatrix}^N = \begin{pmatrix} \left(n_{high}/n_{low}\right)^N & 0 \\ 0 & \left(-n_{low}/n_{high}\right)^N \end{pmatrix}. \tag{2.30}$$

The reflectance of the multilayer stack can then be obtained by solving equation 2.27 for r

$$\mathcal{R} = |r|^2 = \left[\frac{\left(n_{high}/n_{low}\right)^{2N} - 1}{\left(n_{high}/n_{low}\right)^{2N} + 1} \right]^2 \tag{2.31}$$

The position of the reflectance maximum can be calculated by geometric considerations [10]:

$$m\lambda_{max} = 2\left(h_1 \sqrt{n_1^2 - n_0^2 \sin\theta_i} + h_2 \sqrt{n_2^2 - n_0^2 \sin\theta_i}\right), \tag{2.32}$$

where $h_{1,2}$ and $n_{1,2}$ are the layer thickness and refractive index of component 1 and 2, respectively and $m \in \mathbb{N}$.

To model multilayer structures in this work, Rouard's technique was implemented into a "MatLab" algorithm that was developed by Dr. Mathias Kolle [10]. An alternative method based on a transfer matrix algorithm was used for comparison [11]. The optical constants of the building blocks were determined individually by spectroscopic ellipsometry. Figure 2.3a shows example calculations for interference-based antireflective coatings (ARC) which consist of one or two layers on a glass substrate to allow for amplitude and phase matching [12]. Wavelength-dependent optical constants were used to account for the optical dispersion of the used materials. In Figure 2.3b an optical model is presented for stacks of $\lambda/4$ layers with alternating high and low refractive index layers on a glass substrate. An odd number of overall layers corresponds high refractive index layers situated at the air-stack and stack-substrate interfaces.
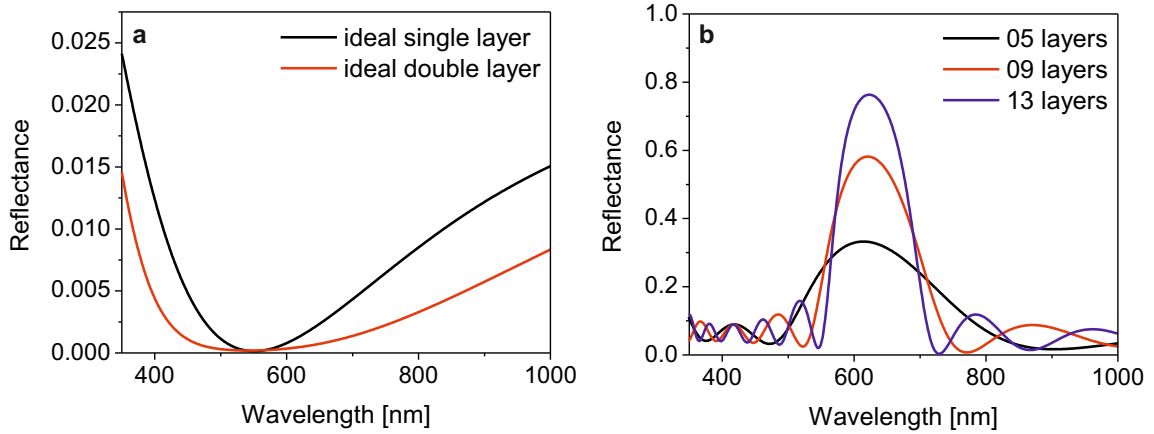
Figure 2.3: **Modelling of multilayer interference. a)** Calculated reflectance at normal incidence for interference-based antireflective coatings (ARC) optimised for $\lambda = 550$ nm. An ideal single layer ARC yields $n_{ARC} = 1.22$ and $h_{ARC} = 112$ nm to fulfill the amplitude and phase matching conditions on a glass substrate ($n_{subs} = 1.50$). The ideal double layer configuration is calculated for comparison, with $n_{ARC_{low}} = 1.11$, $h_{ARC_{low}} = 123$ nm, $n_{ARC_{high}} = 1.36$ and $h_{ARC_{high}} = 101$ nm. **b)** Reflectance at normal incidence for multilayer stacks consisting of an odd number of alternating $\lambda/4$ layers of high and low refractive index on a glass substrate, with $n_{high} = 1.69$, $h_{low} = 75$ nm, $n_{low} = 1.41$, $h_{high} = 130$ nm and $n_{subs} = 1.50$.

2.4   From periodic multilayer stacks to photonic crystals

The model calculation presented in 2.3b illustrates the change in optical response when extending the number of building blocks of a DBR. A further increase in the number of layers or contrast in refractive index ultimately leads to sharply defined, frequency-dependent reflection and transmission characteristics. The alternating sequence of high and low refractive index layers represents a dielectric lattice and can therefore be regarded as a one-dimensional (1D) photonic crystal. Similar to electron propagation in atomic crystals, the periodic modulation of the dielectric creates a potential landscape which determines the propagation directions of photons within the material as a function of frequency. In the case of high symmetries and dielectric contrast, a full three-dimensional photonic band gap can develop for a defined frequency range. This concept was first introduced by Yablonovitch [13] and John [14] and has become a very active field of research ever since [15, 16].

The main function, that contains all the information for a given dielectric system is the magnetic vector field $\mathbf{H}(\mathbf{r}, t) = \mathbf{H}(\mathbf{r})e^{i\omega t}$. Based on the fact that macroscopic electromagnetism is governed by the four Maxwell equations, a so-called master equation can be deduced:

$$\nabla \times \left(\frac{1}{\varepsilon(\mathbf{r})} \nabla \times \mathbf{H}(\mathbf{r}) \right) = \frac{\omega^2}{c^2} \mathbf{H}(\mathbf{r}), \tag{2.33}$$

which is the analogon to the Schrödinger equation for the quantum mechanical consideration of an electron. See reference [17] for a comprehensive derivation.

The periodicity of the system is given by the permittivity $\varepsilon(\mathbf{r}) = \varepsilon(\mathbf{r} + \mathbf{R})$ for all lattice vectors $\mathbf{R}$. It is essential that $\nabla \mathbf{H} = 0$, i.e. the vector field has to be source- and sink-free as well as transverse. Assuming that the Maxwell operator $\hat{\Theta} = \nabla \times \left(\varepsilon(\mathbf{r})^{-1} \nabla \times \right)$ is a linear Hermitian operator, one can use a variational theorem to determine the normal modes and frequencies:

$$E_{\text{var}} = \frac{(\mathbf{H}, \hat{\Theta}\mathbf{H})}{\mathbf{H}, \mathbf{H}} \tag{2.34}$$

The band structure functions $\omega_n(\mathbf{k})$ of a photonic crystal can therefore be exactly calculated *ab initio* from $\varepsilon(\mathbf{r})$ by applying a computational scheme to solve the master equation for the magnetic modes of the photonic crystal under the given boundary conditions. Typical approaches are the finite difference time domain method [18] or the planar wave expansion method [19], which is presented for a 1D model system in reference [10]. Accordingly, the bandwidth of the fundamental reflection peak $\Delta\lambda_{\text{max}}$ (full width at half max) for a photonic crystal-like DBR can be calculated [17]

$$\Delta\lambda_{\text{max}} = \frac{4\lambda_{\text{max}}}{\pi} \sin^{-}1\left(\frac{n_{\text{high}} - n_{\text{low}}}{n_{\text{high}} + n_{\text{low}}} \right). \tag{2.35}$$

2.5 Optical properties of porous thin films

In many different aspects, this work explores structure control in mesoporous materials on the 10 nm length scale. Conceptually, block copolymer (BCP) self-assembly offers precise control over the pore architecture, pore size and pore volume (i.e. porosity) in thin dielectric films. The optical properties of mesoporous materials are not simply a consequence of the constituent materials' crystal band structures, but are dependent on pore dimensions and volume on sub-optical length scales. While generally the real and imaginary parts of the refractive index are an intrinsic property of the material, these can be finely tuned by adjusting the porosity as well as infiltration and blending of the mesostructure with other materials.

Metamaterials are a particular example where morphological arrangement on the sub-wave-length scale is of central importance to the resulting optical properties [20, 21]. The experimental realisation of a material with negative refractive index $n = \sqrt{\mu\varepsilon} < 0$ typically requires negative permeability μ and the permittivity ε in the same frequency range. This can be realised by a so-called split-ring resonator geometry, experimentally achieved for microwave to infrared frequencies [22, 23, 24]. Currently, access to visible frequencies is impeded by resolution limits in the fabrication process. Alternative approaches have been developed but their experimental realisation remains a major challenge [25]. An alternative concept is a chiral route to negative refraction [26]. In a chiral medium the refractive index is polarisation-dependent. The band splitting of the resonant transverse modes leads to a range of frequencies, where the group velocity $v_g = \partial\omega/\partial k$ has an opposite sign to the phase velocity $v_p = \omega/k$, leading to $n < 0$ for a certain polarisation. The validity of this concept has already been shown at terahertz frequencies [27]. However, like for other metamaterial concepts, such as split-ring resonators, it proofs difficult to scale down the structural feature sizes to achieve negative refraction in the visible spectral range.

As outlined in Section 1.2.2 the self-assembly of BCP systems allows access to well defined nanoarchitectures. BCP morphologies have unit-cells far smaller than the wavelength of light, which makes this system a interesting platform for the bottom-up assembly of optical metamaterials. A possible materials route to BCP-templated arrays is illustrated in Figure 2.4, where the metal structure is fabricated in four steps: (1) BCP self-assembly in a thin film, (2) selective etching of one of the polymer blocks, (3) backfilling of the template with a metal, such as silver or gold and (4) selective etching of the residual polymer components [28]. Of particular relevance to optical applications are bicontinuous gyroid morphologies. For a di-block copolymer, the double gyroid consists of two network structures of block A separated by a complementary matrix of block B (Figure 2.4a) [29]. This is the equilibrium arrangement if one of the polymer blocks exhibits a volume fraction of $33 - 37\,\%$ [30]. When extending

from an diblock copolymer, with segments A and B, to a three component system, with blocks A, B and C, the compositional window for the symmetric double gyroid morphology is significantly larger in a ternary phase diagram where the blocks arrange in an ABCBA core-shell structure (Figure 2.4b, space group: $Ia\overline{3}d$ (Q^{230})). Additionally, a three component system allows access to a chiral phase morphology (Figure 2.4c, space group: $Il4_132$ (Q^{214})) [31, 32].

In fact, linear dichroism and gyrotropic light propagation has been experimentally shown for a chiral alternating gyroid structure made of gold, analogue to Figure 2.4c [33]. Theoretical models predict a negative refractive index in the visible and near-infrared range for a symmetric double gyroid morphology after infiltration with silver or aluminium [28].

In lossless dielectric films, the effect of morphology on the optical response is much less pronounced. For model systems with spherical pores in a symmetric arrangement as illustrated in Figure 2.5a, the pore size and spatial periodicity (SC, BCC, FCC) have no effect on the resulting optical properties. These are simply determined by the pore volume for pore diameters $d_{iam} \gg \lambda$ and sufficiently thick films $h_{film}/d_{iam} \geq 150$ [34]. Nevertheless, the spatial arrangement of material will have an influence on how porosity can be controlled and adjusted. The
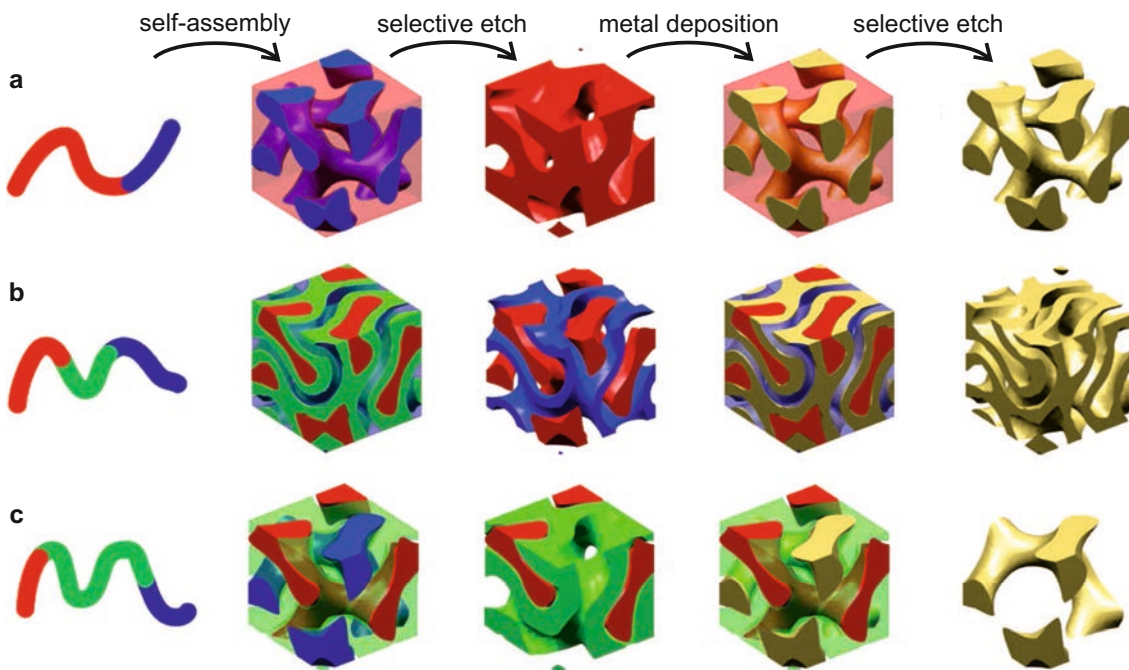
Figure 2.4: **BCP route to metamaterials at visible frequencies.** The templating approach involves four processing steps: (1) BCP self-assembly in a thin film, (2) selective etching of one of the polymer blocks, (3) backfilling of the template with a metal and (4) selective removal of the residual polymer components. The resulting network symmetry depends on the employed BCP: **a)** Diblock copolymer yielding a double gyroid morphology. **b)** Triblock terpolymer resulting in a double gyroid morphology. **c)** Triblock terpolymer route to an alternating gyroid, a chiral morphology. *a) - c) Adapted with permission from [28]. Copyright 2011 Wiley.*

conventional sintering of nanoparticles to form mesoporous films only allows a variation of porosity between $\approx 30\,\% - 40\,\%$ [35]. This is due to the fact that porosity is generated by the random close packing of nanoparticles, which somewhat limits the control over pore size and pore volume [36]. By blending with additional sacrificial material, porosity can be increased up to $60\,\%$ [37]. In contrast, the use of BCPs as templates or structure directing agents for the assembly of inorganic films offers a much higher control over pore size and porosity, even if the film morphology may not be of particular importance. This aspect is further explored in Chapter 5.

Mesoporous materials exhibit pores of $5 - 50\,\text{nm}$ length scale, too small to be resolved using visible light. As a consequence, the compositional arrangement can be treated as an effective medium, with optical constants that depend on the volume fractions of the constituents. There are a number of different physical models that relate the macroscopic properties of a medium to the relative volume fraction of its components. The most intuitive approach has been established by Birchak *et al.*, which describes the effective index of the medium by the linear combination of its volume fractions, i.e.

$$n_{\text{eff}} = (1 - f_{\text{p}})n_{\text{m}} + f_{\text{p}}n_{\text{p}}, \tag{2.36}$$

where f_{p} is the volume fraction of the pores, and n_{m} and n_{p} are the refractive indices of the matrix and pore forming material, respectively [38].

A physical model for the relation between the dielectric constant of an lossless optical medium and the polarisability of its constituent molecules has been introduced by Mossotti and Clausius [39, 40].

$$\frac{n_{\text{eff}}^2 - 1}{n_{\text{eff}}^2 + 2} = \frac{4\pi}{3}\alpha q, \tag{2.37}$$

where n_{eff} is the effective refractive index of the overall medium, α is the molecular polarisability and q is the number of molecules per unit volume. Their analytic solution is based on a dielectric medium which is built up of polarisable objects in empty space in a perfectly mixed, homogeneous and isotropic configuration [41]. When α is modified to account for the local field of nearby atoms, the Clausius-Mossotti model is also valid for homogeneous solid state materials [42].

The extension of the Clausius-Mossotti equation to a mixture of constituents and volume fractions was developed by L. Lorenz and H.A. Lorenz [43, 44].

$$\frac{n_{\text{eff}}^2 - 1}{n_{\text{eff}}^2 + 2} = f_1\left(\frac{n_1^2 - 1}{n_1^2 + 2}\right) + f_2\left(\frac{n_2^2 - 1}{n_2^2 + 2}\right), \tag{2.38}$$

where n_1 and n_2 are the refractive indices of component 1 and 2 and f_1 and f_2 are their volume fractions [45]. The Clausius-Mossotti-Lorenz-Lorenz model assumes mixing of polarisable objects on the molecular level. It does not take into account that the constituents may form domains that are large enough to exhibit their own dielectric identity.

The Maxwell-Garnett model considers mesoscopic domains by shifting from a vacuum lattice with polarisable point objects to a host-guest approach for the dielectric components. The minority component (n_p, f_p) then forms inclusions, i.e. pores, in a host matrix that is formed by the majority component (n_m).

$$\frac{n_{eff}^2 - n_m^2}{n_{eff}^2 + 2n_m^2} = f_p \frac{n_p^2 - n_m^2}{n_p^2 + 2n_m^2}. \tag{2.39}$$

The host-guest model assumes $f_m >> f_p$ and $n_m > n_p$. In cases where the volume fraction of pores becomes comparable or predominant, this approach may not be valid. A more general expression is

$$\frac{n_{eff}^2 - n_h^2}{n_{eff}^2 + 2n_h^2} = f_a \frac{n_a^2 - n_h^2}{n_a^2 + 2n_h^2} + f_b \frac{n_b^2 - n_h^2}{n_b^2 + 2n_h^2}, \tag{2.40}$$

where n_h^2, n_a^2 and n_b^2 are the refractive indices of the host and components a and b, respectively. This is equivalent to the Clausius-Mossotti-Lorenz-Lorenz equation for $n_h^2 = 1$. The expression leads to the Maxwell-Garnett model for $n_h^2 = n_{eff}^2$. For a self-consistent approach with $n_h^2 = n_{eff}^2$ equation 2.40 reduces to

$$(1 - f_b) \frac{n_a^2 - n_{eff}^2}{n_a^2 + 2n_{eff}^2} + f_b \frac{n_b^2 - n_{eff}^2}{n_b^2 + 2n_{eff}^2} = 0. \tag{2.41}$$

This is the so-called Bruggeman effective medium approximation. The predictions of the four models are exemplified in Figure 2.5b for an porous material with $n_m = 2$ in air ($n_p = 1$). For $f_{p,air} = 0.3$ the deviation between Bruggeman ($n_{eff} = 1.69$), Birchak ($n_{eff} = 1.70$) and Maxwell-Garnett ($n_{eff} = 1.71$) is well within the experimental uncertainty. In contrast, the deviation becomes significant for highly porous materials.
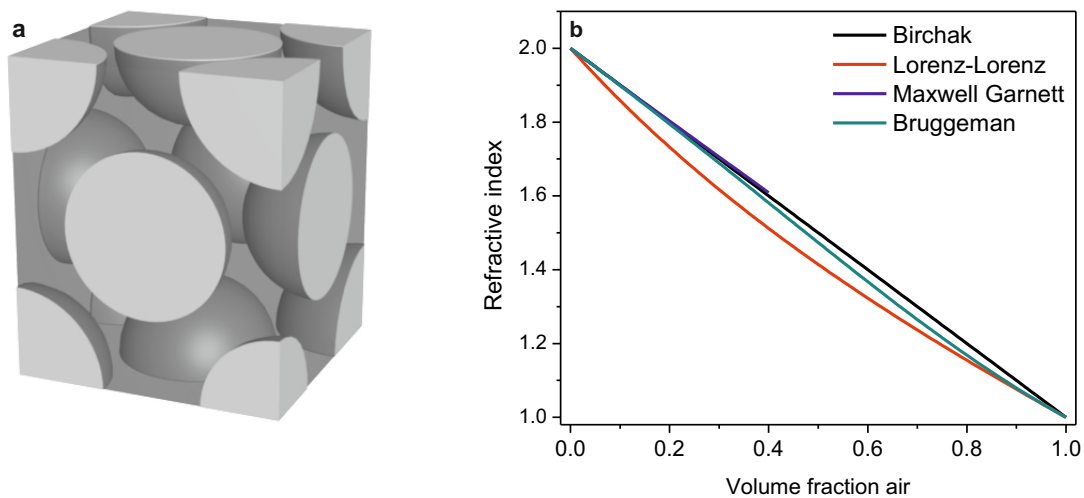
Figure 2.5: **Effective medium approximation. a)** Schematic of a two component film with close-packed pores. **b)** Refractive index vs. porosity for different effective medium approximations with $n_{high} = 2$. The Maxwell-Garnett model assumes one majority component and $n_m > n_p$, which is only valid in a limited range. *a) Adapted with permission from [46]. Copyright Mathias Kolle.*

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Chapter 3

Structure-function interplay in dye-sensitised solar cells

The design, fabrication and characterisation of novel electrode architecture for dye-sensitised solar cells was of central importance for this thesis. The following chapter aims to explain the fundamental principles of this photovoltaic concept, elucidate the interplay between the electrode architecture and device function and highlight possible ways to increase the power conversion efficiency.

Absorption of light followed by the generation and transport of charge carriers to the electrodes are the principal functions of any photovoltaic cell. In conventional p-n junction-based photovoltaic devices these tasks are carried out by the same material, an inorganic semiconductor. The working principle of dye-sensitised solar cells is fundamentally different and takes inspiration from photosynthesis [1]. Light absorption and charge generation occur separately in specifically designed device components. The light harvesting complex is a photoactive dye molecule which is anchored to the surface of a wide band-gap semiconductor and surrounded by a redox medium. Upon absorption of light, incident photons stimulate the dye molecule to form an excitonic state.

With appropriate energy-level alignment of the device components, charge separation occurs at the interface to the electron and hole conducting materials. Electrons are injected into the conduction band of an inorganic semiconductor and transported to the electrode. Regeneration of the oxidised dye takes place via an electron-donor species, typically an iodine $(3I^-/I_3^-)$-based liquid electrolyte. Initial work dates back as early as 1887 when James Moser showed the extension of the absorption spectrum of a photoelectrochemical cell by the sensitisation with a light-absorbing dye molecule [2]. Yet, the acceptance of DSCs as a promising photovoltaic concept only arose from the seminal work of O'Regan and Grätzel who introduced a novel electrode architecture in the form of a mesoporous TiO_2 film with 780-fold

surface area. The associated substantial increase in dye-loading led to an order of magnitude rise in the conversion efficiency of incident photons to electrons [3]. The strategy of sintering nanometre-sized TiO_2 particles to form an electron conducting random network of extremely large surface area is still widely used today and a central part of the conventional device architecture, shown in Figure 3.1.

Like any single-junction photovoltaic cell, conventional dye-sensitised solar cells obey the Shockley–Queisser limit for the power conversion of the sun's black body radiation, shown in Figure 3.1b. Accordingly, the ideal excitation energy ΔE should be $\sim 1.1\,\text{eV}$ ($\lambda \geq 1125\,\text{nm}$), which would result in a power conversion efficiency of 33.7 %, if the dye's excitation energy could be fully converted into electrical energy [4]. These values are far from reach in any experimental realisation. Historically, the ruthenium-based photosensitisers N3 (1991, [5]), N719 (1999, [6]) and N749 (2001, [7]) were milestones in dye synthesis and enabled power conversion efficiency records of 10.0 % [5], 10.6 % [8] and 11.1 % [9], respectively. Recently, a shift from the iodine to a cobalt-based electrolyte in combination with the development of an organic donor-π-acceptor porphyrin dye enabled to increase the current benchmark to 12.3 % [10].

A typical current-voltage curve of a DSC under illumination with simulated sunlight is shown in Figure 3.1c. The performance is typically normalised to the area of the illumination and given as a density, such as the current density J [mA/cm^2] or the power density P [mW/cm^2]. The current output follows a classical diode characteristics with an offset due to the generated photocurrent, here plotted with a positive sign [11]. Forward bias signifies applying a negative potential to the n-type working electrode. The operating regime of a solar cell thus lies in forward bias between $0\,\text{V}$ and the open circuit potential V_{oc}, where the overall cell current is zero. The maximum photocurrent generated at $0\,\text{V}$ is defined as as short circuit current (J_{sc}). The corresponding generated power density of the device ($P = J \cdot V$) peaks at the maximum power point (P_{max}), which determines the optimum forward bias (V_{max}) and the related current density (J_{max}). The fill factor (FF) quantifies the deviation of the current-voltage characteristics from a square curve and is therefore a key quality factor of the device, with

$$FF = \frac{J_{max}\,V_{max}}{J_{sc}\,V_{oc}} = \frac{P_{max}}{J_{sc}\,V_{oc}}. \tag{3.1}$$

The power conversion efficiency η is the ratio of generated power density to incident illumination irradiance:

$$\eta = \frac{P_{max}}{P_{in}} = \frac{J_{sc}\,V_{oc}\,FF}{P_{in}}. \tag{3.2}$$

The current-voltage curve shown in Figure 3.1c corresponds to an efficiency η of 10.6 % and a fill factor FF of 0.75. Another fundamental device parameter is the so-called incident-photon-

to-electron conversion efficiency (IPCE), which correlates the number of generated electrons, measured as photocurrent at 0 V, to the incident photon flux at a particular wavelength.

$$\text{IPCE} = \frac{n_{\text{electrons}}(\lambda)}{n_{\text{photons}}(\lambda)} = \frac{J_{\text{sc}}}{P_{\text{in}}} \frac{\text{hc}}{\text{e}\lambda} \tag{3.3}$$

A characteristic plot of IPCE(λ) for conventional devices employing the sensitisers N719 and N749 is shown in Figure 3.1d.
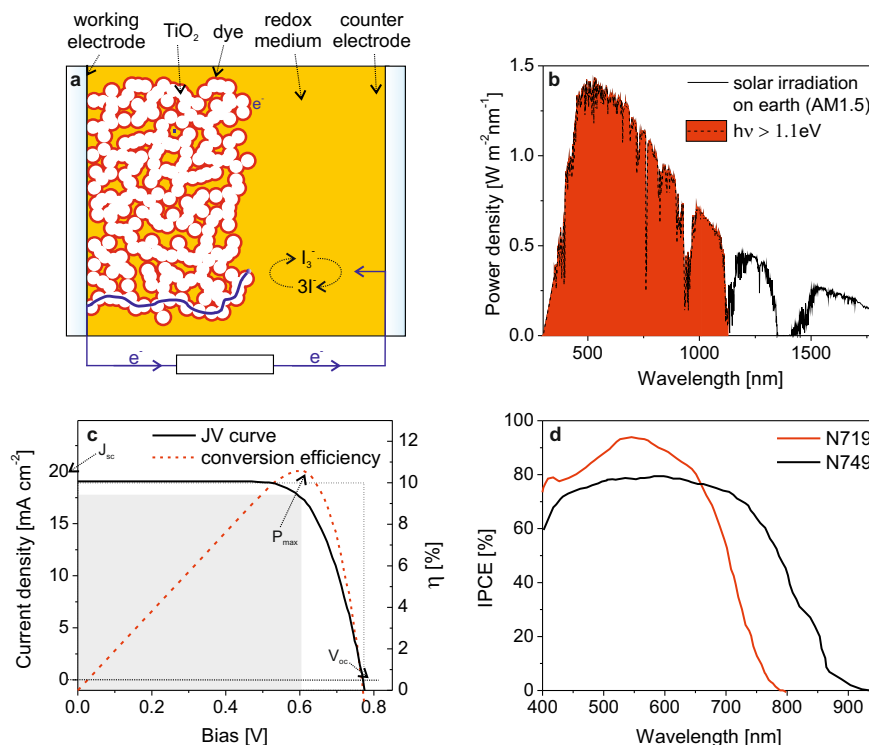
Figure 3.1: **Key device characteristics of dye-sensitised solar cells a)** Schematic of a conventional device architecture. Nanometre-sized TiO$_2$ particles form an electron conducting random network with high surface area. A monolayer of light-absorbing dye molecules is chemisorbed onto the TiO$_2$ and surrounded by an electrolyte. Upon photoexcitation of the dye, electrons are injected into the TiO$_2$, while the oxidised dye is regenerated by the electron-donating redox medium, which is subsequently reduced at the counter electrode. **b)** Power density of solar irradiation on earth as a function of photon wavelength (AM 1.5, reference [12]). The spectral window for an ideal single junction solar cell ($\Delta E = 1.1$ eV) is shown as a dashed line. **c)** Current–voltage ($J - V$) characteristics of a conventional DSC under illumination (dye N719). The generated power density of the device ($P = J \cdot V$) is shown in red. The device performance can be described by the key parameters J_{sc} (short circuit current), V_{oc} (open circuit potential) and P_{max} (maximum power point). **d)** Incident-photon-to-electron conversion efficiency (IPCE) as a function of wavelength for devices sensitised with the dye N719 (red) and N749 (black), respectively. *c) data reprinted with permission from [8]. Copyright 2003 Elsevier. d) N749 data reprinted with permission from [7]. Copyright 2001 American Chemical Society. N719 data reprinted with permission from [13]. Copyright 2007 Elsevier.*

The functioning of a DSC is largely determined by the energy level alignment between the individual components as well as the underlying kinetics of the charge separation and charge transfer processes. Figure 3.2 represents an energy level diagram of a conventional liquid electrolyte DSC with the underlying reaction kinetics. The fundamental processes include:

(1) Photo-excitation of the dye [14].

(2) Electron injection into the metal oxide [15, 16].

(3) Electron transport to the working electrode [17].

(4) Regeneration of the oxidised dye by electron transfer from donor species [18, 19].

(5) Hole transport to the electrode [20].

(6) Reduction of the oxidised donor [21].

and the competing charge recombination processes:

(7) Excited state decay of the dye [14].

(8) Regeneration of the oxidised dye by back transfer of into TiO_2 injected electrons [22].

(9) Recombination of injected electron with acceptor species in the redox medium [23, 24].

Dye-sensitised solar cells are a promising photovoltaic concept for a number of reasons. The spatial separation of light absorption and charge generation makes the devices very stable against photocorrosion. This is due to the band gap of the employed semiconductor material in the photoanode, being a measure of the chemical bond strength. Metal oxides like TiO_2 or Nb_2O_3 have an absorption edge towards the ultraviolet and are therefore stable against photodegradation in the spectral range of highest photon energy flux, i.e. the visible spectrum [26]. Unlike conventional p-n junction solar cells, where excitons are generated in the bulk and then need to diffuse to the p-n interface in order to be separated and extracted, exciton generation in DSCs takes place directly at the material's interface. As a consequence the demand on materials purity is much lower, which implies that processing under vacuum, ultra high temperature or cleanroom classification is generally not necessary [27]. Recent advances in the synthesis of organic dyes have eliminated the need for the rare ruthenium-based sensitisers, meaning that all device components are now abundant and promise significantly lower processing costs than existing technologies [10, 28]. The variety of colours and transparencies distinguishes DSCs from other photovoltaic concepts and makes them ideally suited for integrated architecture and building design [29, 30].
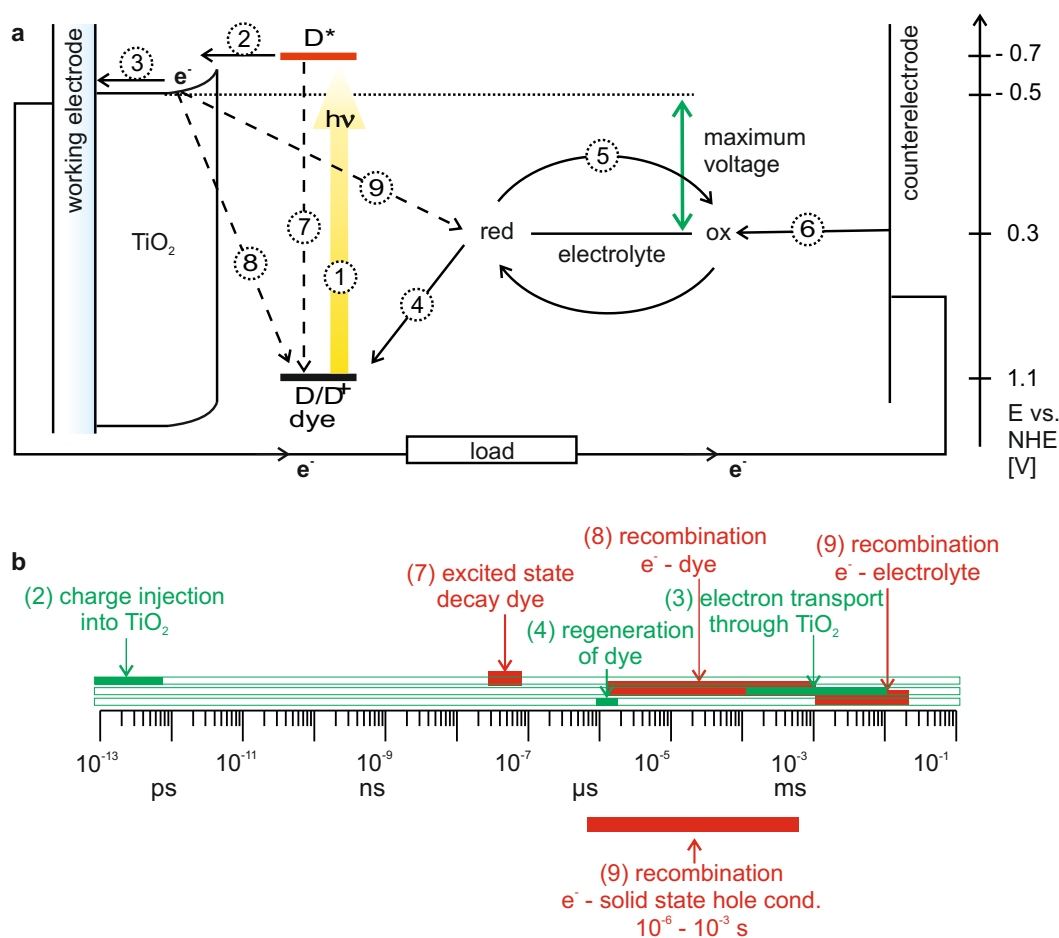
Figure 3.2: **Energy level diagram and reaction kinetics. a)** Energy level diagram of a conventional liquid electrolyte DSC. Fundamental processes include: (1) photo-excitation of dye, (2) electron injection into the metal oxide, (3) electron transport to the working electrode, (4) regeneration of the oxidised dye by electron transfer from surrounding donor species, (5) hole transport to the electrode, (6) reduction of the oxidised donor. Possible loss mechanisms are: (7) Excited state decay of the dye, (8) regeneration of the oxidised dye by back transfer of into TiO_2 injected electrons, (8) recombination of injected electron with acceptor species in the regenerating redox medium. The energy level E vs. NHE denotes the potential with respect to the reference of a normal hydrogen electrode (NHE). **b)** Overview of reaction kinetics for the processes described above. Parasitical recombination processes are marked in red. The time regimes above the scale correspond to a standard iodine-based liquid electrolyte cell. An alternative system is the solid state DSC, where dye regeneration occurs via an electron donating organic hole-transporter. This one-electron redox system exhibits different recombination kinetics, shown underneath the scale [19, 25].

Nevertheless, high performance DSCs with $\eta_{max} = 12.3\,\%$ lag behind other technologies and fall short of their theoretically attainable efficiency [10, 31]. When consolidating efficiency parameters and experimental results of Figures 3.1 and 3.2 several key points for further efficiency enhancement are evident:

1. **Loss in potential**: The established high performance black dye N749 has an absorption onset at ~ 920 nm, corresponding to an optical bandgap of around 1.35 eV. However, devices only deliver $V_{oc} = 0.74$ V (in the case of N719: $E_{gap} = 1.48$ eV; $V_{oc} = 0.80$ V). As schematically illustrated in Figure 3.2a, photoelectrochemical cells rely on the progression of charge carrier generation followed by several charge carrier transfer processes. In order to make these energetically more favourable than parasitical recombination processes, a certain loss in potential is required. The dye regeneration via the redox reaction of iodine ($3I^-/I_3^-$) consumes ~ 0.6 V, due to the fact that the reaction is a two-step process [32, 33]. The oxidation of the electrolyte ($2I^- \rightarrow I_2^-$) requires an overpotential of $0.2 - 0.3$ eV, followed by the dismutation of $2I_2^- \rightarrow I_3^- + I^-$, with a further demand of ~ 0.3 eV. Alternative routes that employ a one-electron regeneration process may only require an overall loss in potential of 0.4 eV instead of up to 0.75 eV, which would make power conversion efficiency of 20 % viable [31]. Yet, changing from a two-electron to a one-electron regeneration process has far-reaching consequences on the kinetic balance of the system as recombination of injected electrons with oxidised acceptor species becomes more likely.

2. **Loss in absorption/photocurrent**: As shown in Figure 3.1d, the IPCE can reach values up to 80-90 % in high efficiency devices but only in a limited spectral range. The IPCE then drops drastically in regions of poor dye extinction, i.e. in the tail of the absorption spectra of the dye [34]. The development of dyes that are more panchromatic and of higher exctinction coefficient is therefore essential [35]. Another effective parameter is the photonic design of the photoanode architecture. The addition of a layer of scattering particles is widely used to increase the IPCE, particularly in the red/infrared region of the spectrum due to the greatly enhanced photon path length [9, 34]. Further control of the light-matter interaction can be achieved by integration of one-dimensional (1D) or three-dimensional (3D) photonic crystals [36, 37].

3. **Loss in fill factor**: The origin for the deviation of the $J - V$ curve from an ideal diode characteristic are numerous. Ohmic resistance arises from the diffusion impedance of the electrolyte ($0.7 - 2\,\Omega/cm^2$, [20]), the charge transfer resistance of platinum-based counterelectrode $< 1\,\Omega/cm^2$ and the sheet resistance of the transparent conducting electrode (TCE) [19]. This will not affect the open circuit voltage but seriously deteriorates the diode characteristics, as the overall fall of potential is now divided between the diode and an ohmic resistor, which are connected in series [32]. Another impairing influence for the fill factor arises from the recombination of electrons in the substrate with vacancies in the donor species, particular for alternative redox couples with one-electron

transfer. This parallel (or shunt) resistance can somewhat be suppressed by coating the TCE with a compact metal oxide layer [38]. Furthermore, the extraction efficiency of injected electrons is voltage-dependent and near-unity IPCE values measured at J_{sc} may not necessarily lead to similarly efficient extraction under working conditions. At the maximum power point, the electron density in the TiO_2 is typically doubled compared to short circuit conditions, leading to an increase in the recombination rate [39]. Poorly working devices with an extremely low FF are often the consequence of an s-shaped $J - V$-curve under illumination. This may be caused by photo-injected electrons that cannot escape the metal oxide network due to insufficient percolation paths to the TCE or a degraded counter electrode [39].

The focus of this dissertation was to employ the structure control offered by soft matter self-assembly to explore the structure-function interplay of DSC photoanodes. Two different strategies were followed:

1. Increase in photocurrent, photovoltage and fill factor by the design of novel electrode structures with improved charge transport properties. See Section 3.1.

2. Increase IPCE in regions of low dye absorption by enhancing light-matter interaction through the integration of photonic crystal elements. See Section 3.2 for the design of alternative device architectures with photonic properties.

3.1 Novel electrode structures for enhanced charge carrier transport

Several requirements for the morphology of the electron-conducting photoanode are apparent when studying the operating principle of DSCs. As photons are only absorbed at the n-dye-p interface, the photoanode needs to exhibit an extremely large surface to multiply the available area for dye anchoring. Even state-of-the-art dyes with high extinction coefficients require a photosensitive interfacial area that is a hundred- to thousand-fold increased compared to a flat film. Upon excitation and electron injection, the oxidised dye has to be promptly reduced by a surrounding regenerating redox mediator. The pores of the electron-conducting network therefore need to be large enough to allow ion diffusion for a solution-based electrolyte or pore infiltration with a solid state hole conductor. Furthermore the porous network has to offer direct percolation paths for the extraction of charges. Thus, an idealised photoanode morphology should be mesoporous (i.e. exhibit porosity on the 10 nm length scale), bicontinuous and offer adequate charge carrier transport.

The efficiency leap in the seminal work of O'Regan and Grätzel in 1991 was mainly due to a novel photoanode structure which sufficiently fulfilled these requirements - a mesoporous network generated by the random sintering of 20 nm-sized TiO_2 particles. Although random in pore size and morphological order, this electrode structure is still the gold standard in today's devices and a fundamental component in all record-breaking DSCs [9, 10]. Two main drawbacks arise from the random sintering of nanoparticles to form a mesoporous network, namely poor charge transport [40] and a lack of control over the pore size distribution [41].

The electron mobility typically decreases by several orders of magnitudes from a value of $\mu \sim 10\,cm^2/Vs$ for single crystal anatase [42] to around $\mu \sim 10^{-1} - 10^{-5}\,cm^2/Vs$ in nanoparticle films [40, 43, 44]. In comparison to a single-crystal model system where only optical phonon scattering and lattice defects limit the mean free path of propagating electrons [45], a number of causes slow down electron diffusion in random networks, as illustrated in Figure 3.3a. Charge traps are located at the grain boundaries between the crystalline nanoparticles as well as at the particles' surfaces and in the bulk. These lead to the formation of an exponentially decreasing tail of sub-band gap states below the conduction band edge [46, 47]. Furthermore electrostatic interactions with surrounding ions in the redox medium influence the electron diffusion and lead to trapping and an ambipolar diffusion process [46, 48]. It is therefore widely agreed that electron transport in such mesoporous networks is consistent with a multiple trapping model, where generated electrons mostly populate localised states below the conduction band and only diffuse towards the electrode in iterative cycles of thermal detrapping and trapping [39, 46, 47, 49]. This is illustrated in Figure 3.3b.

Accordingly, the effective electron diffusion coefficient $D_{el,eff}$ in TiO_2 can be correlated with the concentration of electrons that are localised in sub-band gap traps ($\rho_{el,t}$) and delocalised in the conduction band ($\rho_{el,c}$).

$$D_{el,eff} = \left(1 + \frac{\partial \rho_{el,t}}{\partial \rho_{el,c}}\right)^{-1} D_{el,0}, \tag{3.4}$$

where $D_{el,0}$ is the diffusion coefficient of electrons in the conduction band (i.e. in a trap-free system) [47].

While experimental evidence for a multiple trapping-governed electron transport process is convincing [48, 49], the exact origin of the multitude of transport-limiting traps is still under debate [25]. In particular the decisive role of traps on the particle surface [50, 51] and at the interparticle's grain boundaries [52] has been experimentally shown. Furthermore the geometry plays a decisive role as the random dense packing of nanoparticles leads to a greatly enhanced number of dead-ends, i.e. particles with only one neighbour, for porosities above 50 %, resulting in a percolation threshold at 76 % porosity [53]. The development of network
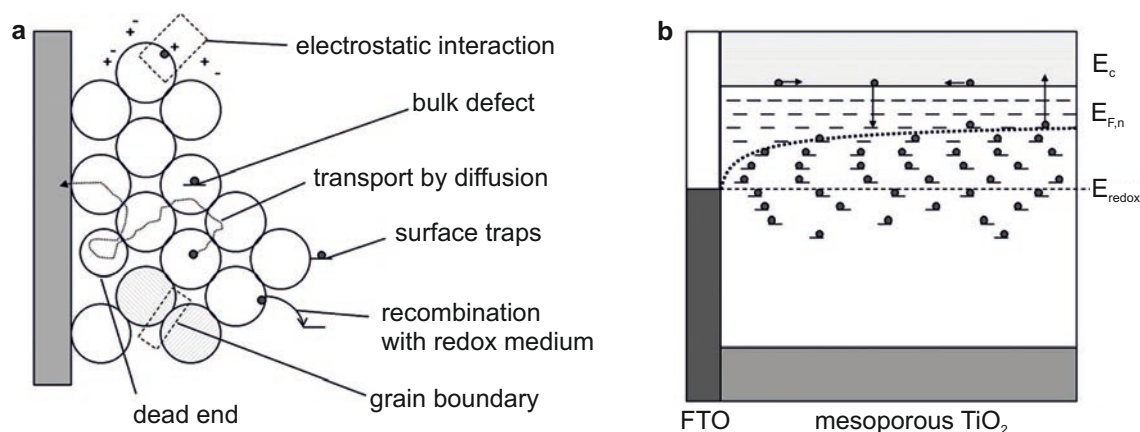
Figure 3.3: **Electron transport in mesoporous TiO$_2$. a)** Simplified drawing to illustrate electron transport across a random network of nanocrystalline particles. Diffusion of electrons to the working electrode is limited by traps located at the particle grain boundaries, their interfaces and in the bulk of the particles, as well as by dead ends in the percolation path. Furthermore electrostatic interactions with surrounding ions in the redox medium influence the diffusion process, leading to ambipolar diffusion and trapping. **b)** Schematic diagram of electron transport to the electrode under short-circuit conditions as proposed by a multiple trapping model. More than 90 % of the generated electrons are trapped in localised sub-band gap states below the conduction band edge [39]. Transport in the conduction band only takes place in iterative cycles of thermal detrapping and trapping. *a) - b) Adapted with permission from [19]. Copyright 2010 American Chemical Society.*

structures with well defined bicontinuous geometries, large and oriented nanocrystals and stoichiometrically annealed surfaces should therefore result in significantly improved electron mobilities.

Historically, the poor electronic properties of a random nanoparticle network were not a major limiting factor due to the slow recombination kinetics for the iodine-based redox couple [33]. Yet, one of the main recent trends is to reduce the loss-in potential and improve device efficiency by moving from a two-electron to a one-electron regeneration process. Examples include the use of an electrolyte with a cobalt-based redox couple [10] or an organic solid state hole transporting material [54, 55] with reported V_{oc} up to 0.97 V and 0.99 V, respectively. These systems furthermore eliminate the corrosion problems of the iodine-based electrolyte, which limits the lifetimes of the cells [28]. However, due to faster recombination kinetics in a one-electron redox system, the poor electron transport properties of nanoparticle-based films deteriorate photocurrent, fill factor and photovoltage through low charge collection efficiencies, faster interfacial recombination and high internal resistance [25, 56]. A further drawback of the standard nanoparticle network for new generation DSCs is the lack of control over the pore size distribution [41]. Cobalt complexes are bulky and therefore need well-defined

percolation paths with sufficiently large pores to avoid mass transport limitations to the counterelectrode [10, 56]. For solid state DSCs, a heterogeneous pore size distribution may reduce pore filling when infiltrating the viscous materials [57, 58]. As a consequence both device systems are somewhat limited in the maximum film thickness, which particularly affects the IPCE in the tail of the absorption spectrum [5].

Several concepts for nanostructured photoanodes of next generation DSCs are presented in Figure 3.4. A cross-sectional and close-up view of a standard nanoparticle network is shown in Figure 3.4a,b. Crystalline TiO_2 nanorods or nanotubes have attracted much interest as alternative morphology. These should exhibit greatly enhanced charge carrier transport properties as the percolation path is in principal 1D and therefore much more direct [59] (Figure 3.4c-e). Hydrothermal growth allows the formation of µm long single crystal rutile nanorods [60, 61]. Advances in the electrochemical anodisation of titanium have led to the fabrication of up to $\sim 20\,\mu$m long TiO_2 nanotubes [62]. Highest electron mobilities are expected in systems that exhibit the growth of single-crystalline wires [61, 63] or quasi-single crystalline growth through the oriented attachment of crystalline fragments [52, 59, 64]. On the other hand, these 1D arrays suffer from a greatly reduced surface area per unit volume due to the conformal alignment and lack of nanoporosity associated with the roughness of nanometre-sized crystals.

Efforts are therefore drawn towards the fabrication of hierarchical structures that are typically tree-like, i.e. they consist of a highly conductive one-dimensional backbone that branches out into a network of feeding pathways. This can be realised by pulsed laser ablation [65] (Figure 3.4g) or hydrothermal growth [66]. While it seems rational that these nanostructures exhibit greatly improved electronic properties, there is still a lack of experimental evidence for this assumption. Single crystal TiO_2 nanorods can only synthesised rutile, which is a somewhat less ideal n-type semiconductor for DSCs. Thus, the electron transport rates found in single crystal rutile nanorods are similar to random anatase nanoparticle networks [67]. Nanotube arrays made from electrochemical anodisation are polycrystalline and show comparable electron transport properties to random nanoparticle networks of similar crystallite size distribution [68, 69]. This is in contrast to a reported increase in electron transport properties by orders of magnitude when one-dimensional growth is governed by the oriented attachment of nanocrystals to form a random network of fibrils [59].

An alternative approach to control structure formation of the photoanode is to use a sacrificial template. The potential of block copolymers (BCPs) ,which can self-assemble into highly ordered, bicontinuous arrangements and allow morphology replication by inorganic materials, is discussed in Chapter 1.2. An example of a freestanding TiO_2 gyroid network is shown in Figure 3.4g, which was fabricated by electrochemical deposition of TiO_2 into one selectively degraded phase of the BCP film [70]. In contrast to 1D networks, the use of BCPs as sacrificial

templates or structure-directing agents allows the fine control over the morphology formation in 3D and therefore a much wider parameter space for probing the structure-function interplay in dye-sensitised solar cells [71].
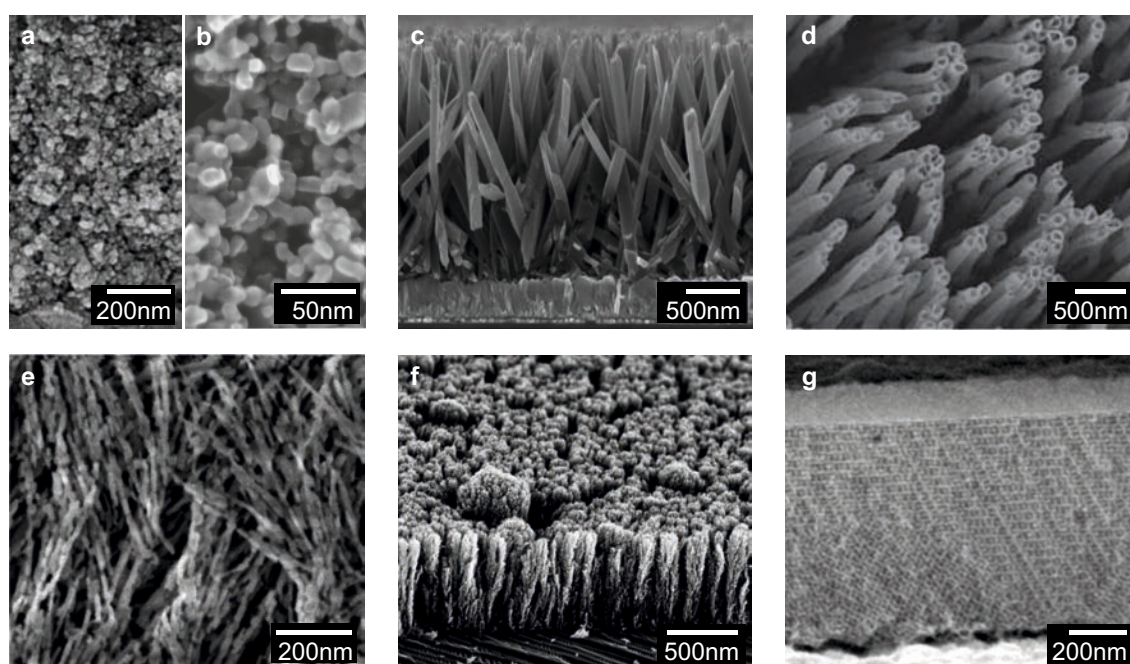
Figure 3.4: **Scanning electron microscopy of novel electrode structures for DSCs. a)** Cross-sectional and **b)** close-up view of a conventional TiO_2 electrode, generated by the random sintering of ~ 20 nm-sized nanoparticles. **c)** Cross-sectional image of single-crystalline TiO_2 nanorods fabricated by hydrothermal growth in solution. **d)** Top view of ~ 20 µm long TiO_2 nanotubes, grown by electrochemical anodisation of titanium. **e)** Micrograph of a 3D fibrous network of crystalline TiO_2 nanowires synthesised by hydrothermal growth (top view). **f)** Cross-sectional image of an array of hierarchical, tree-like TiO_2 nanostructures that were generated by pulsed lased deposition. **g)** Cross-sectional view of TiO_2 resembling the bicontinuous gyroid morphology generated by electrochemical deposition of TiO_2 into a sacrificial block copolymer template. *a) Adapted with permission from [57]. Copyright 2006 Elsevier. **b)** Adapted with permission from [1]. Copyright 2000 John Wiley & Sons. **c)** Adapted with permission from [61]. Copyright 2009 American Chemical Society. **d)** Adapted by permission from Macmillan Publishers Ltd: Nature Materials [62], copyright 2009. **e)** Adapted with permission from [59]. Copyright 2010 American Chemical Society. **f)** Adapted with permission from [65]. Copyright 2010 American Chemical Society. **f)** Adapted with permission from [70]. Copyright 2009 American Chemical Society.*

3.2 Photonic device architectures for enhanced light absorption

Light harvesting in a DSC is fundamentally related to the absorption spectrum of the light-sensitive component. Following the Beer-Lambert law, the absorbance A of light in a photoactive medium is defined as

$$A(\lambda) = -\log_{10}\left(\frac{I}{I_0}\right) = \varepsilon(\lambda)cl, \qquad (3.5)$$

with I and I_0 the intensity for incident and transmitted light, ε the molar extinction coefficient of the dye, c the molar concentration and l the photon path length.

As the film thickness of the photoanode is somewhat restricted due to mass transport limitations and recombination dynamics, the only parameter that can increase light harvesting in a DSC seems to be the development of dyes that absorb with a high extinction coefficient across the targeted spectral range. In fact, recent record efficiencies stem from the development of organic porphyrin-based dyes with a donor-π-bridge-acceptor structure [10, 72]. Yet, the absorption in high efficiency devices is not only determined by the intrinsic properties of the sensitiser but also influenced by the photonic design of the electrode structure. The photon path length l can greatly exceed the film thickness through the incorporation of optical elements into the device structure. This is particularly important for the spectral regions with low extinction (typically in the red/infrared [5]) where the necessary film thickness would otherwise exceed rational device principles.

The incorporation of larger TiO_2 particles to increase the photon path length by multiple scattering has been theoretically described as particularly beneficial with a wavelength-dependent optimum scatterer size of $d_{iam} \sim 0.68 \cdot \lambda$ [73, 74]. Nowadays, scattering particles of $\sim 400\,nm$ diameter are a common element in record efficiency cells [9, 10, 13]. Various configurations have been developed, where the scattering particles are positioned either within or on top of the working electrode [34, 75]. Recently, much progress has been made in the fabrication of mesoporous scattering particles of controlled size that can contribute to light absorption and electron generation due to their increased surface area [76, 77, 78]. While the implementation of scattering particles has proven highly beneficial for enhanced light absorption, the diffusive scattering over a broad spectral range has the detrimental effect of turning the cells opaque. This deprives the DSC of its variability in colour and thus, its potential for integrated architecture [29, 30].

An alternative concept that allows more detailed control over the optical action spectrum is the integration of photonic crystal (PC) elements into DSCs. These enable to enhance light harvesting in specific parts of the spectrum while preserving cell transparency in others [36, 79].

Early experimental work on the integration of PC elements into the device architecture of DSCs was focussed on the use of 3D PCs in the form of TiO_2 inverse opal structures [80, 81]. These were deposited onto FTO substrates and subsequently covered with a mesoporous TiO_2 layer of high surface area. PC fabrication limitations only allowed to deposit the mesoporous layer on top of the inverse opal structure, which required illumination from the counterelectrode to enable the penetration of incident light into the device structure. Nevertheless double layer devices showed a clear enhancement of the IPCE in the spectral vicinity of the photonic band gap. This was initially attributed to slow photon propagation $v_g = \hbar \partial \omega / \partial k$ in the region of flat photon dispersion relation $E(k)$ [80, 82]. While this mechanism is in principle possible, it would only be effective for a narrow range of photon frequencies at the edge of the photonic band gap [83]. Further experimental investigations indicated that the absorption enhancement was mainly caused by incoherent scattering at disordered regions of the PC [81, 84]. Moreover, Bragg diffraction in the periodic lattice was identified as the third possible origin for the observed enhancement [85].

Mihi and Míguez later introduced a concept for the optimised coupling of a PC layer to a DSC [36], which is illustrated in Figure 3.5. According to their model, resonant cavities are formed between the PC top layer and the high refractive index TCE. The resonant modes are determined by the penetration depth of the incoming light into the PC and the thickness of the mesoporous film sandwiched between the PC and the substrate. These cavities give rise to the localisation of photons in the device, thus an enhanced absorption probability throughout the photonic band gap of the PC. The calculated optical response of the individual components with similar surface area is shown in Figure 3.5b for a sensitised 3D PC (black line) and mesoporous layer (dotted line). The expected absorption peak at the edge of the photonic band gap, caused by slow photon propagation in the 3D PC, can be clearly identified. However, the overall absorption of the 3D PC suffers from the impeded propagation of photons into the structure for frequencies within the photonic band gap. In contrast, a combined device architecture where a mesoporous layer is sandwiched between the TCE and the 3D PC is predicted to exhibit significant absorption enhancement in a wide spectral range, as shown in Figure 3.5c. Within the spectral region of the photonic band gap, the optical response oscillates between two situations, indicated as λ_1 and λ_2. Photons are either localised in the device due to the formation of a resonant cavity (λ_1: low reflection, high absorption, low group velocity) or simply reflected off the 3D PC (λ_2: high reflection, low absorption, high group velocity). In both cases, the result is an increased absorption in comparison to a reference DSC without an optical element due to the prolonged photon dwell time in the device.

While this device architecture is highly promising, the modelled effects strongly depend on the correct layer configuration and high structural order. Experimental realisation proved dif-

Figure 3.5: **Integration of a 3D photonic crystal into the DSC device architecture. a)** Schematic of a double layer photoanode, where a mesoporous TiO$_2$ layer of high surface area is sandwiched between the FTO substrate and a highly ordered inverse opal layer, representing a 3D PC. **b)** Reflectance, absorptance and inverse group velocity (c/v_g) within the 3D PC (solid line) and in a conventional mesoporous film (dotted lines). **c)** Model calculation of the optical response of a double layer DSC electrode. Depending on the penetration depth into the 3D PC and the thickness of the mesoporous film, photons are either localised in the device due to the formation of a resonance cavity (λ_1: low reflection, high absorption, low group velocity) or simply reflected off the 3D PC (λ_2: high reflection, low absorption, high group velocity). Both cases lead to an absorption enhancement in comparison to a reference DSC without optical element, due to the prolonged photon dwell time in the device. **b) - c)** *Adapted with permission from [36]. Copyright 2005 American Chemical Society.*

ficult, mainly because of fabrication problems associated with the growth of a 3D inverse opal structure of high optical quality onto a previously deposited mesoporous TiO$_2$. After evaporation induced self-assembly, the colloidal array had to be infiltrated with a high refractive index material, typically TiO$_2$. This clogged the underlying mesoscopic pores and therefore inhibited sensitisation and electrolyte infiltration of the double layer device. The correct double layer configuration was finally experimentally achieved by protecting the mesoporous underlayer with a copolymer [86]. Yet, the lack of intimate physical contact between the two layers prevented the harvesting of PC-induced resonance effects.

An alternative to a 3D PC is the integration of a 1D PC into the device architecture, illustrated in Figure 3.6a. The 1D PC element is typically realised by a mesoporous Bragg reflector, which is fabricated via the cyclic deposition of nanoparticle-based TiO$_2$ and SiO$_2$ into a multilayer to achieve porosity and refractive index contrast in the stack [87]. The effect of the 1D PC on the light harvesting of the DSC has been experimentally and theoretically investigated [88, 79]. The optical response of a double layer structure subject to illumination from the

front side (white) or PC side (red) is shown in Figure 3.5e. Reference points are denoted at characteristic wavelengths $\lambda_1 = 775\,\text{nm}$ (band-pass), $\lambda_2 = 575\,\text{nm}$ (maximum reflectance) and $\lambda_3 = 512\,\text{nm}$ (dip in reflection peak). The spatial distribution of the electric field $|E|^2$ under front side illumination, modelled by scalar wave approximation, is presented in Figure 3.5f. Similar to the case of a 3D PC, the concentration of the electric field throughout the photonic band gap of the 1D PC is evident. While λ_1 represents a reference region with almost no Bragg scattering by the PC top layer, λ_3 shows the effect of the formation of a resonance mode with an increase of $|E|^2_{\text{max}}$ by a factor of > 2.5. The overall benefit for the integration of a 1D PC in high performance DSCs was recently experimentally demonstrated [89, 90].
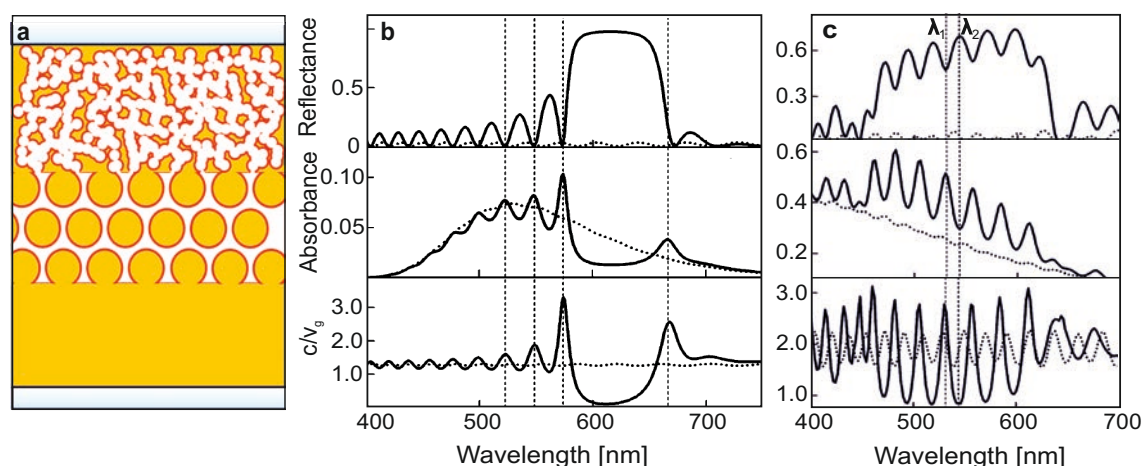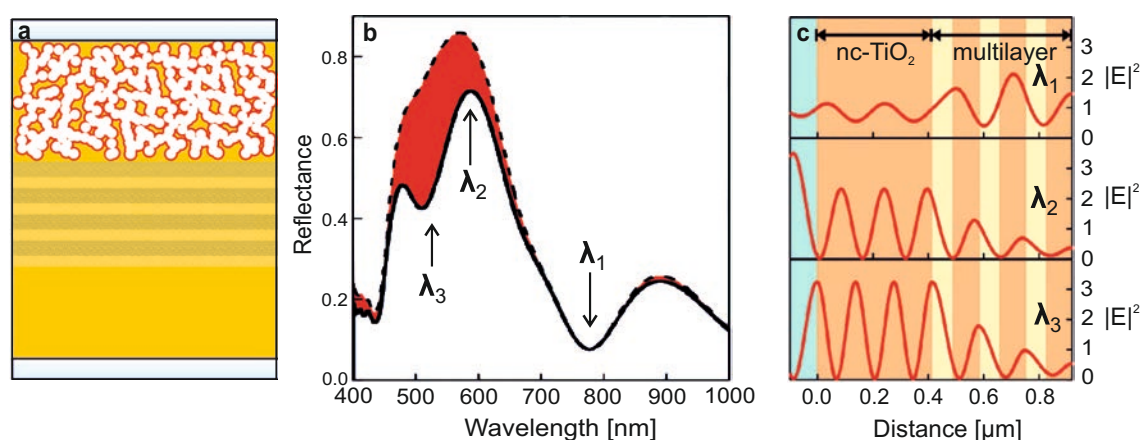

Figure 3.6: **Integration of a 1D photonic crystal into the DSC device architecture.** **a)** Schematic of a double layer device architecture with a mesoporous Bragg reflector acting as 1D PC. **b)** Comparison of optical response for a double layer DSC with illumination from the front side (white) and PC-side (red). **c)** Modelling of the electric field, based on scalar wave approximation, reveals the spatial distribution of $|E|^2$ in the double layer electrode depending on the wavelength of incoming photons, where $\lambda_1 = 775\,\text{nm}$ (band-pass), $\lambda_2 = 575\,\text{nm}$ (maximum reflectance) and $\lambda_3 = 512\,\text{nm}$ (dip in reflection peak). **b) - c)** *Adapted with permission from [88]. Copyright 2009 American Chemical Society.*

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Experimental and analytical techniques

4.1 Materials fabrication

4.1.1 Poly(isoprene-*block*-ethylene oxide) copolymers

Poly(isoprene-*block*-ethylene oxide) (PI-*b*-PO) exhibits several intrinsic characteristics which make the block copolymer (BCP) system excellently suited as a structure-directing agent for the co-assembly of inorganic nanostructures. Polar hydrolysis products of titanium or silicon-based precursors preferentially reside in the hydrophilic PEO block due to the formation of hydrogen bonds with the ethylene oxide [1]. The Flory-Huggins interaction parameter of the PI-PEO couple is particularly high compared to other systems [2]. The low glass transition temperature of 213 K for both blocks allows high chain mobilities at ambient temperatures [3, 4]. Anionic polymerisation enables the synthesis of molecules with a high degree of polymerisation and low polydispersities [5]. The self-assembly behaviour of PI-*b*-PEO has been widely studied intensively and its phase diagram is now well understood, covering the full range of PI/PEO volume ratios [6]. Besides several PI-*b*-PEO diblock copolymers, a triblock terpolymer PI-*b*-PS-*b*-PEO with an intermediate PS (polystyrene) block was also used in the course of this thesis. See Table 4.1 for an overview of the employed BCPs.

All BCPs employed in this study were synthesised and characterised by Morgan Stefik and Juho Song in the group of Professor Ulrich Wiesner at Cornell University, USA. See reference [5] for experimental details. The polymers were characterised by ^{1}H NMR spectroscopy and their polydispersity was determined using gel permeation chromatography (GPC). The characteristic properties of polymers used in this study are shown in Table 4.1.

Table 4.1: **Characteristic properties of employed BCPs.**

M_n PI-b-PEO [kg/mol]	N_{TOT}	M_n PEO [kg/mol]	N_{PEO}	f_{PEO} [%]	PDI $(= \frac{M_w}{M_n})$
12.5	204	2.6	58	20.4	1.10
34.4	606	9.8	245	28.4	1.05
35.7	609	8.2	205	23.0	1.03
91.6	1579	28.6	651	31.2	1.09

M_n PI-b-PS-b-PEO [kg/mol]	M_n PI [kg/mol]	M_n PS [kg/mol]	M_n PEO [kg/mol]	f_{PEO} [%]	PDI
53.4	14.6	29.0	9.8	19.4	1.05

4.1.2   Sol-gel chemistry

Hydrolytic sol-gel chemistry is a solution-based technique that leads to the formation of an oxide, like SiO_2, TiO_2 or Nb_2O_5, via a two-step chemical reaction. This involves the hydrolysis of the precursor material (typically a metal alkoxide or metal salt):

$$X - (OR)_v + H_2O \rightarrow \text{OH-X-OR}_{v-1} + ROH, \tag{4.1}$$
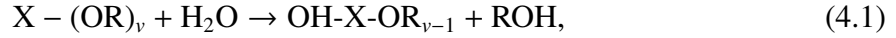
where X represents the core chemical element of the precursor material, v its valency and R is the organic substituent. The fully hydrolysed precursor $X\text{-}(OH)_v$ in a colloidal suspension (sol) then undergoes condensation reactions to form an oxide network (gel) via one of the two chemical pathways:

$$\text{X-OH}_v + \text{X-OH}_v \rightarrow OH_{v-1} - XOX - OH_{v-1} + H_2O \tag{4.2}$$

$$\text{X-OR}_v + \text{X-OH}_v \rightarrow OH_{v-1}XOX - OR_{v-1} + ROH \tag{4.3}$$
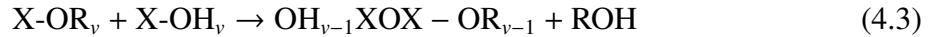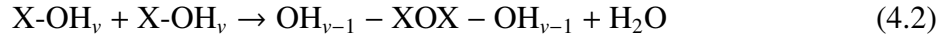
et sequens

Depending on the reaction kinetics, condensation may also take place between partially hydrolysed species, resulting in a multitude of different reaction sequences [7]. Sol-gel chemistry is an effective chemical route for the BCP-directed assembly of inorganic material if the reaction kinetics can be sufficiently controlled. This includes limitations in spatial dimensions of the guest material to allow incorporation into one of the BCP phases [8]. Furthermore, the gelation process needs to be slow in comparison with the time scale for microphase separation to prevent quenching of the BCP-driven structure formation process before reaching thermodynamic equilibrium [9]. Another challenge is the sol-gel accompanied release of wa-

ter and alcohol, as this may impede the symmetric evaporation of solvents from hydrophilic and hydrophobic components. A major advantage of the sol-gel route is the possibility to fully condense the inorganic material into a homogeneous and continuous network, e.g. through temperature annealing after microphase separation, which distinguishes the technique from co-assembly of chemically inert nanoparticles.

Hydrolytic sol-gel chemistry of TiO$_2$

In contrast to silica sol-gel chemistry, where the hydrolysis of a silicon alkoxide typically needs the catalysis by an electrophile, the hydrolysis and subsequent condensation of metal alkoxides occurs spontaneously and is difficult to control [7]. Several strategies have been introduced to overcome the problem of uncontrolled condensation and macroscopic phase separation, including the utilisation of pH variation, stabilising ligands, nonaqueous media and preformed nanoclusters [10]. Yet, the kinetic control is still restricted, preventing a comparable structure control and polymorphism as reported in neat BCP or BCP/silica systems [10, 11]. In this work the titanium alkoxides titanium isopropoxide (OR $\stackrel{\scriptstyle\wedge}{=}$ OCH(CH$_3$)$_2$) and titanium ethoxide (OR $\stackrel{\scriptstyle\wedge}{=}$ OCH$_2$CH$_3$) were used as titanium source. Control of reaction kinetics was attempted by manipulation of the pH, ratio of water molecules and detachment of hydrolysis and phase separation by the introduction of a solvent exchange.

Hydrolytic sol-gel chemistry of aluminosilicates

The co-assembly of organically modified aluminosilicates has been of interest in this work due to its abrasion resistance and low refractive index [12]. The sol-gel chemistry of aluminosilica involves the hydrolysis and condensation of a mixture of silicon and aluminium precursors, typically in a molar ratio of 9:1 (Si:Al). In the course of this study a sol-gel route was employed, where aluminum sec-butoxide serves as the aluminum source and 3-glycidyloxypropyltrimethoxysilane as the silicon source. The organic modification 3-glycidyl-oxypropyl plays an important role in the solubility and compatibilisation of the inorganic material during the subsequent co-assembly process [13]. Due to the reactivity of the aluminum sec-butoxide, the mixture is typically hydrolysed in a two-step process, where the first 15 % of the final amount of acidic water is added at 0 °C. The mixture of aluminium and silicon in the aluminosilica material then occurs via the hydrolysed precursors. According to ^{27}Al solid state nuclear magnetic resonance spectroscopy, the aluminium is typically found in tetrahedral and octahedral coordination, i.e. evenly distributed in the silicon-framework and in aluminium microdomains, respectively [14].

4.1.3 Thin film deposition

The fabrication of BCP-derived material architectures in thin films is inherently linked to solution-based processing. Polymers and inorganic material are typically mixed in a solvent system which is compatible with all components. Self-organisation into a phase separated film then occurs during the evaporation of the solvent. The evaporation rate of the solvent system therefore defines the available time-scale for structure formation [15].

Spin coating

Spin coating deposits a solute material onto a substrate by angular rotation. Typically an excess volume of solution is placed onto a substrate, which is held on a vacuum stage. The stage is then accelerated up to a rotational speed between 500 and 10,000 revolutions per minute. During the spinning process the droplet develops in a three step process. In a first phase most solution is centrifuged off the substrate to form a homogeneous film of thickness h_0 and a concentration c_0. Outflow of solution dominates the mass loss of the sample in the second phase until a critical film thickness h_c is reached. In the final phase the evaporation of solvents becomes the dominant mechanism of mass loss, leading to a dry film of defined thickness, typically in the range of 10 nm to several μm [16, 17]. A schematic of the spin coating procedure is shown in Figure 4.1a. The resulting final film thickness h_∞ can be calculated as a function of rotational speed ω, viscosity η and initial concentration c_0, which has been verified experimentally for model systems [17, 18].

$$h_\infty \sim \omega^{-1/2}\eta^{1/3}c_0. \tag{4.4}$$
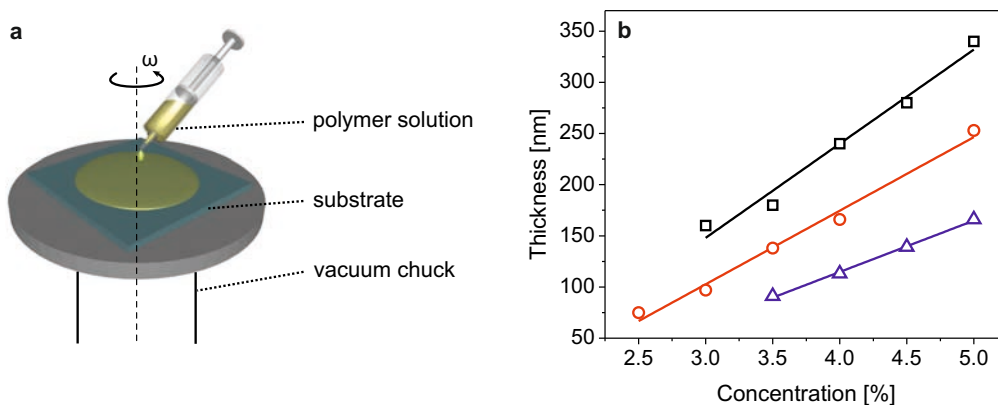
Figure 4.1: **Spin coating and film thickness calibration. a)** Schematic of the spin coating process, where a substrate is held on a vacuum stage and covered by excess volume of solution before the stage is accelerated to a rotational speed between 500 and 10,000 revolutions per minute for film formation. **b)** Exemplary relationship between final film thickness and solute concentration for different solvent systems. *a): Adapted with permission from [19]. Copyright Mathias Kolle.*

The linear dependence of the final film thickness on the initial concentration of the solution is in good agreement with results in this work, presented in Figure 4.1b. The adjustment of concentration was therefore used as the main parameter for film thickness control. Spin coating was carried out on a WS-400B-6NPP-Lite processor (Laurell Technologies).

Blade coating

Blade coating (or doctor blading) is an alternative technique for thin film deposition on the lab-scale with accessible film thicknesses ranging from several hundred nm to µm. Here, a drop of solution is placed in front of a sharp blade that is then drawn linearly across the substrate to form a thin wet layer, which subsequently dries into a solid film. The thickness of the film can be controlled by the vertical distance between the substrate and the blade, the concentration of the solution and the drying kinetics. Another important parameter is the shape of the evolving meniscus, which depends on the surface energy of the substrate, surface tension of the solution, its viscosity and the shear field that is a function of the drawing speed [20]. The employed set-up, used in the course of this work, is shown in Figure 4.2. A commercially available instrument (RK Print Coat Instruments, K Paint Applicator) was extended by a solvent-fed chamber and a programmable heating element (Omron E5CS). The enclosed atmosphere allowed adjustment of solvent partial pressure and enabled in conjunction with the thermal stage fine control of crucial parameters for structure formation, such as temperature and solvent drying kinetics. Neither spin coating nor blade coating are attractive film deposition techniques from an industrial point of view. Yet on the lab-scale, they offer repeatable and finely controllable deposition conditions. The further understanding of processing parameters may then be transferrable to roll-to-roll processing techniques such as slot-die coating or meniscus coating [20, 21].
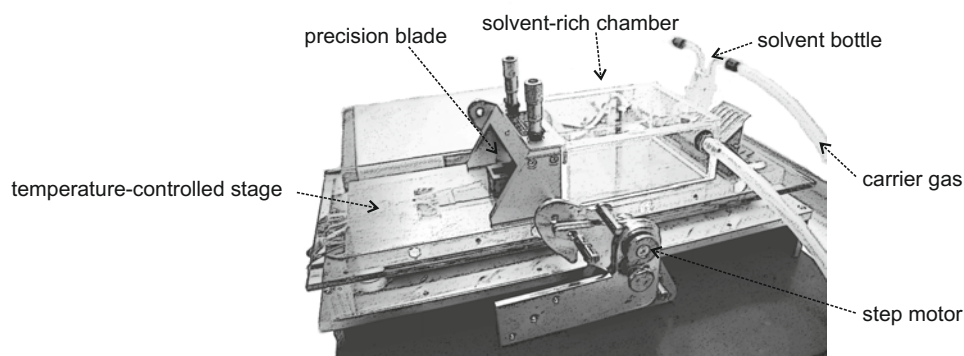

Figure 4.2: **Blade coating in controlled environment.** A commercial blade coating set-up was modified by the integration of a programmable heating element and an enclosed chamber, which is fed by solvent-rich atmosphere through a saturated carrier gas.

4.2 Materials characterisation

A variety of characterisation techniques is necessary to understand and develop self-assembly driven material formation and functioning. Figure 4.3 shows an overview of the employed techniques in the course of this work and their accessible length scales. Their main operation principles are briefly explained in the following.
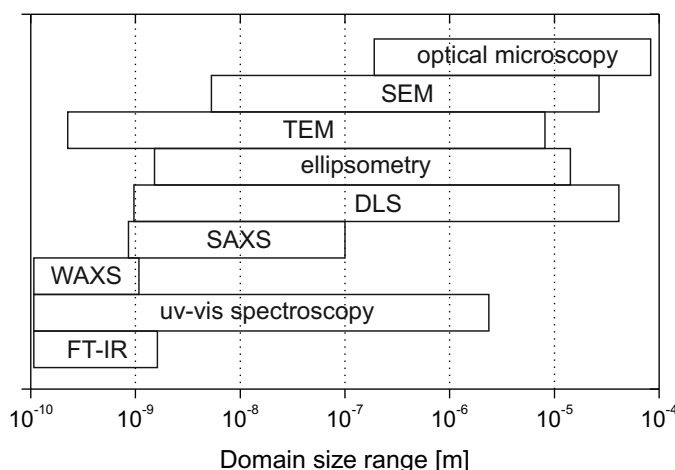
Figure 4.3: **Overview of the employed characterisation techniques and their accessible length scales.** Abbreviations from top to bottom: SEM - scanning electron microscopy; TEM - transmission electron microscopy; DLS - dynamic light scattering; SAXS - small angle X-ray scattering; WAXS - wide angle X-ray scattering; FT-IR - Fourier transform infrared spectroscopy. [22]

4.2.1 Imaging techniques

Various aspects of this work were concerned with structure formation on the sub-100 nanometre scale. The resolution of conventional visible-light microscopes is restricted to the spatial limit s to which a beam of light can be focused, i.e. $s = \lambda/2(n \sin \theta)$, where $n \sin \theta$ is the numerical aperture $NA < 1.4$. In order to resolve smaller feature sizes a reduction of the employed wavelength is needed. Electron microscopes use a beam of electrons which is collimated and focused with electromagnetic lenses to illuminate the sample. Typical de Broglie wavelengths are in the range of $10^{-13} - 10^{-11}$ m. The study of electron-sample interactions therefore allows imaging with resolution down to the nanometre-length scale.

Possible interactions of an electron beam with a specimen are schematically shown in Figure 4.4. The variety of detectable signals opens up a multitude of ways to employ electron microscopy.
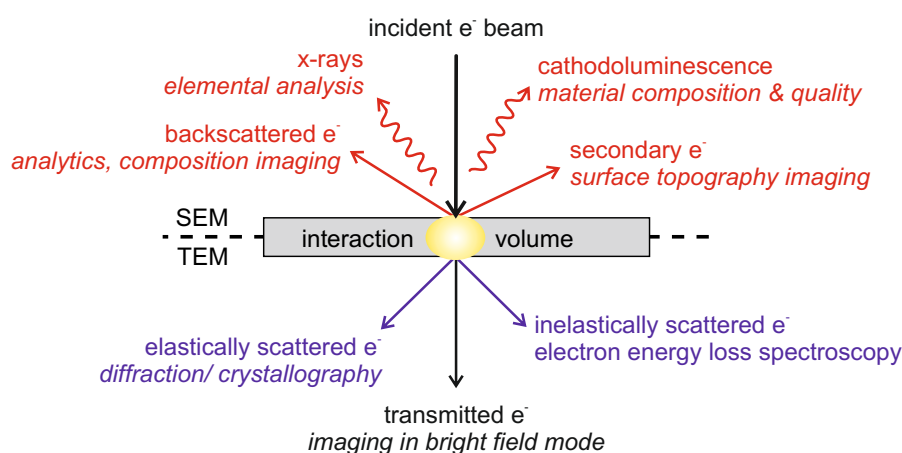
Figure 4.4: **Overview of electron-matter interaction and corresponding use in electron microscopy.** [23]

Scanning electron microscopy

In scanning electron microscopy (SEM) the electron beam is focused to a very small spot size and scanned over the surface of a sample. A number of different operational modes allow to gain insight information of the samples topography and material composition with up to 5 nm resolution in commercial instruments. The most common operational mode is the detection of secondary electrons, which can produce high resolution images of the samples surface. Secondary electrons are generated by inelastic scattering of primary electrons from atoms of the sample material. Due to their low energy (< 50eV), only secondary electrons that are generated close to the surface (< 10 nm) contribute to the signal, thereby providing high topographical contrast. In the most commonly used detection technique "In-Lens", secondary electrons which are generated directly in or near the spot centre are absorbed, re-accelerated and focused through an electromagnetic field to the "In-Lens" detector. A combination of scintillator and photomultipliers generate a signal that is translated into a pixel intensity. Imaging is achieved by scanning the electron beam over the sample

Further signal processing includes the detection of X-rays, backscattered electrons and cathodoluminescence. The detection of characteristic X-rays from the excitation of inner shell electrons is used in energy dispersive X-ray spectroscopy (EDX) to spatially resolve and carry out elemental analysis of the specimen. The detection of backscattered electrons offers further information on the elemental composition as the intensity of elastically scattered electrons is strongly dependent on the atomic number of the specimen. Spatially-resolved detection of cathodoluminescence corresponds to the collection of a sample's photoemission in the visible spectrum caused by the electron beam interaction. Energy decay after the excitation of outer shell electrons can take place via phonon or photon emission. The detection of intensity and

spectrum of photoemission therefore delivers information on the composition, growth and quality of semiconductors and other materials.

In the course of this work SEM was carried out on a LEO Ultra 55 with a field emission source of typically 3 kV electron acceleration voltage [24]. The instrument was mainly used for imaging of the samples topography via the "In-Lens" detection system. Occasionally EDX was employed for elemental characterisation of the specimen. In order to prevent charging effects a conductive platinum layer ($\sim$ 2 nm) was deposited onto the sample with a sputter coater (Emitech K575X, 8 s, 75 mA). Typical SEM parameters were: working distance $3 - 5$ mm, extractor voltage 5.9 V, extractor current 162.8 μA, filament heating current 2.36 A, gun vacuum 4.1×10^{-10} mbar and system vacuum 5.8×10^{-6} mbar.

Transmission electron microscopy

Transmission electron microscopy (TEM) is another technique that was employed for material characterisation. While sample preparation proves considerably more difficult and time-consuming, the achievable image resolution is superior to SEM, typically with resolution below 1 nm in commercial instruments.

In the bright field imaging mode, only transmitted and weakly scattered electrons are collected due to the positioning of the objective aperture and focusing of the lens optics. Dark areas on the screen then correspond to strongly scattering regions in the sample. The resulting image of the sample can therefore reveal information on morphological features, structural composition and crystallinity. In diffraction mode the lens system is adjusted as such that the backfocal plane is focused. Electrons that leave the sample at identical angles undergo coherent scattering. The resulting Bragg reflections reveal information on the crystal structure, unit cell size, crystal orientation and the degree of polycrystallinity of the sample [23].

Cryo-ultramicrotomy allows the preparation of sufficiently thin hybrid or organic sample sections. This involves embedding of the sample in a viscous water-soluble compound, cooling to -50 °C and sectioning in $30 - 40$ nm slices using consecutively a glass and diamond knife on a piezoelectric-actuated motion stage. Alternatively ultrathin hybrid films can be floated onto a TEM grid using a sacrificial water-soluble underlayer ,e.g. poly (4-styrene sulfonic acid, to aid lift-off from the substrate [25].

Two different instruments were used in this work. During a research stay at Cornell University a FEI Tecnai T12 Spirit TEM (acceleration voltage 120 keV) was used under the supervision of Dr. Morgan Stefik. In Cambridge TEM imaging was carried out with Giorgio Divitini on a FEI Tecnai F20-G2 FEGTEM with a 200 kV field emission gun.

4.2.2   Scattering techniques

While real space imaging offers a direct route for the sampling of material arrangement, scattering techniques only allow structure determination in the reciprocal space. Results then have to be related to the real space by Fourier transformation. Scattering techniques are often complimentary to imaging as the obtainable results are statistically more reliable, since all scattering events in the beam passage contribute to the measured signal.

An ordered morphology, may it be an atomic crystal or a phase separated BCP structure, can be represented by a periodic lattice of scattering objects. Diffracted wavefronts undergo constructive interference if the Bragg condition is satisfied (see Figure 4.5a) [26]:

$$n\lambda = 2d\sin\theta, \tag{4.5}$$

where $n = 1, 2, 3...$ is the order of peak, λ is the wavelength of the incident beam, d is the spacing of lattice planes in real space, and θ is the angle between the incident beam and the lattice plane. Periodicity in the sampling structure can therefore be investigated by variation of wavelength (Laue method) or scattering angles (Scherrer method, angular dependent scattering) in the appropriate range.

The construction of a reciprocal lattice proves useful to understand when the condition for constructive interference is met. The array of periodic scattering objects can be described with $\mathbf{R} = n_1\mathbf{a}_1 + n_2\mathbf{a}_2 + n_3\mathbf{a}_3$, where n_i are integers and $\mathbf{a}_i$ are the primitive vectors that span the so-called Bravais lattice. For any translation of $\mathbf{R}(n_1, n_2, n_3)$ the lattice is therefore invariant. Incoming waves are generally described with $\Psi_k(\mathbf{r}) = \Psi_0\exp^{i\mathbf{kr}}$. Accordingly, the set of wavevectors $\mathbf{k}$ which result in plane waves with the periodicity of the Bravais lattice is defined by the condition:

$$\Psi_0\exp^{i\mathbf{kr}} = \Psi_0\exp^{i\mathbf{k}(\mathbf{r}+\mathbf{R})} = \Psi_0\left(\exp^{i\mathbf{kr}}\cdot\exp^{i\mathbf{kR}}\right). \tag{4.6}$$

Therefore,

$$\exp^{i\mathbf{kR}} = 1 \tag{4.7}$$

has to be fulfilled for all $\mathbf{R}$, leading to the definition of the reciprocal lattice vector in $\mathbf{k}$-space for which $\exp^{i\mathbf{kR}} = \exp^{i\mathbf{GR}} = 1$, i.e. $\mathbf{G} = h\mathbf{b}_1 + k\mathbf{b}_2 + l\mathbf{b}_3$. Considering a set-up shown in Figure 4.5b, constructive interference of the diffracted beam is obtained for $\exp^{i(\mathbf{k}_{out}-\mathbf{k}_{in})} = 1$. This determined the so-called Laue condition:

$$\mathbf{q} = \frac{4\pi\sin\theta}{\lambda} = \mathbf{k}_{out} - \mathbf{k}_{in} = \mathbf{G}(h, k, l). \tag{4.8}$$

Thus, for any scattering vector $\mathbf{q} = \mathbf{k}_{out} - \mathbf{k}_{in}$ that can be expressed with $\mathbf{G}(h, k, l)$, the Bragg

condition is met for integer values of h, k, l. The three indices h, k, l therefore define symmetry planes in the crystal lattice that result in characteristic reflection peaks. The related notation in real space $[hkl]$ refers to the direction $h\mathbf{a}_1 + k\mathbf{a}_2 + l\mathbf{a}_3$ of the normal vector for this characteristic set of crystal planes.

The above description does not consider the spatial dimensions of the scattering objects and the finite size of the crystal, which both affect the measured intensity $I(\mathbf{q})$. The spatial dimensions of the scattering object is generally described by a form factor $F(\mathbf{q})$ of the crystal's unit cell, while the finite size is accounted for by the convolution of the reciprocal lattice with a step function $\sigma(\mathbf{r})$ and the corresponding Fourier transform $\mathcal{F}[\sigma(\mathbf{r})] = \sum(\mathbf{q})$. The measured scattering intensity $I(\mathbf{q})$ therefore follows

$$I(\mathbf{q}) \propto |F(q)|^2 \cdot |Z(\mathbf{q}) * \sum(\mathbf{q})|^2, \tag{4.9}$$

where $Z(\mathbf{q}$ defines the reciprocal lattice. This means that, in addition to the periodic arrangement, one can also obtain information on the overall size of the crystal and spatial dimensions of the lattice points from scattering experiments. See reference [27] for details.

The appropriate angular window for a fixed wavelength (typically $\lambda_{\text{CuK}\alpha} = 1.54\,\text{Å}$) then depends on the length scale of interest. For probing the atomic lattice of a solid state material, where d_{hkl} is comparable to the wavelength, wide-angle X-ray scattering with $2\theta \sim 10° - 80°$ allows to resolve the corresponding diffraction peaks. For feature sizes that are large compared to the wavelength of the beam, small angle X-ray scattering with $2\theta \sim 0.1° - 5°$ covers the correct angular range.

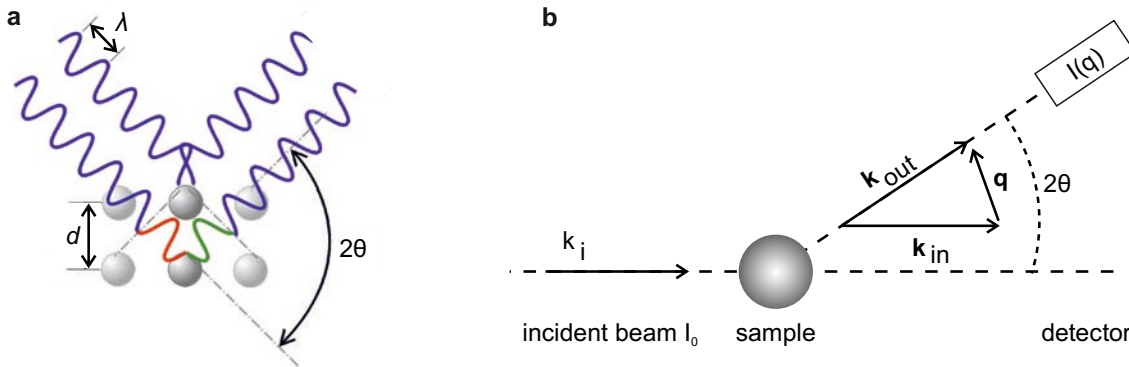Figure 4.5: **Principles of x-ray scattering techniques. a)** Elastically scattered incident waves undergo constructive interference if the difference in path length $2d\sin\theta$ is an integer multiple of the wavelength. **b)** Schematic of a scattering experiment. *a): Adapted with permission from [28].*

Wide angle x-ray scattering

Wide angle x-ray scattering (WAXS) was used in the course of this study to determine the crystallite size, crystal anisotropy and crystal phase mixing for materials such as $CaCO_3$, Fe_2O_3, SnO, TiO_2, ZnO, WO_3 and others. Characterisation was carried out *ex situ* as well as *in situ* during the temperature treatment

All experiments were carried out in a $\theta - 2\theta$ configuration, i.e. the sample was kept fixed while source and detector were rotated by $\theta°$ with respect to the sample plane. *In situ* WAXS was carried out on a Bruker "D8 Advance" X-ray diffractometer with integrated temperature stage. The actual temperature on the sample spot was calibrated via the lattice expansion of silicon and rutile TiO_2. Unit cell parameters were calculated using the software "UnitCell" [29]. The temperature offset between thermocouple and sample spot was identified by comparing the lattice expansion with reference data [30, 31, 32]. *Ex situ* WAXS was carried out on a Bruker "D8" diffractometer with position sensitive detector ("LynxEye").

Small angle x-ray scattering

Small angle X-ray scattering (SAXS) is capable to detect elastic scattering events at lower scattering angles ($\sim 0.1° - 10°$) and allows therefore to obtain structural information on the mesoscopic length scale ($1 - 100\,\mathrm{nm}$). In a typical set-up a beam of monochromatic X-ray radiation is focused on a bulk sample. The scattered X-rays form a pattern, which is collected by a two-dimensional X-ray detector, situated at a long distance from the sample in order to achieve high spectral resolution at low scattering angles. In order to identify the material's spatial arrangement from the scattering pattern, the observed peak spacings have to be compared to characteristic sequences for model lattices of candidate morphologies. The corresponding sequence of diffraction peaks for model diblock copolymer morphologies can be found in Table 4.2. A typical diffraction pattern of a block copolymer / inorganic hybrid is shown in Figure 4.6, which is consistent with a hexagonal arrangement of cylinders.

Block copolymer phase morphologies are just one example for material structures that can be characterised by SAXS. In general, any one- to three-dimensional structural pattern can be resolved by sufficient electron contrast between the building blocks [33]. In contrast to typical diffraction patterns from WAXS of crystalline solids, peaks are typically broadened. This is a consequence of the long-range imperfection of self-assembled periodic mesostructures, giving rise to fluctuations in size and spacing of the scattering bodies [27].

A variety of SAXS instruments were used in the course of this work. Laboratory set-ups were employed in Cambridge (Bruker "Nanostar", Department of Materials Science) and at Cornell University (Rigaku "RU300" rotating anode, Department of Physics). For high flux

experiments synchrotron radiation was utilised at the Cornell High Energy Synchrotron Source (CHESS, G1 beamline) and at the Diamond Light Source UK (I22 beamline). While SAXS experiments in Cambridge and at the Diamond light source were carried out by the author, characterisation at Cornell University was performed by Hiroaki Sai.

Table 4.2: Bragg spacings for model diblock copolymer morphologies [34].

Structure	q_{hkl}/q_{100}				
Lamellar	1	2	3	4	5
Hexagonal-packed cyl.	1	$\sqrt{3}$	$\sqrt{4}$	$\sqrt{7}$	$\sqrt{9}$
Gyroid	1	$\sqrt{4/3}$	$\sqrt{7/3}$	$\sqrt{8/3}$	$\sqrt{10/3}$
Body-centered cubic	1	$\sqrt{2}$	$\sqrt{3}$	$\sqrt{4}$	$\sqrt{5}$
Close-packed spherical	1	$\sqrt{4/3}$	$\sqrt{8/3}$	$\sqrt{11/3}$	$\sqrt{12/3}$
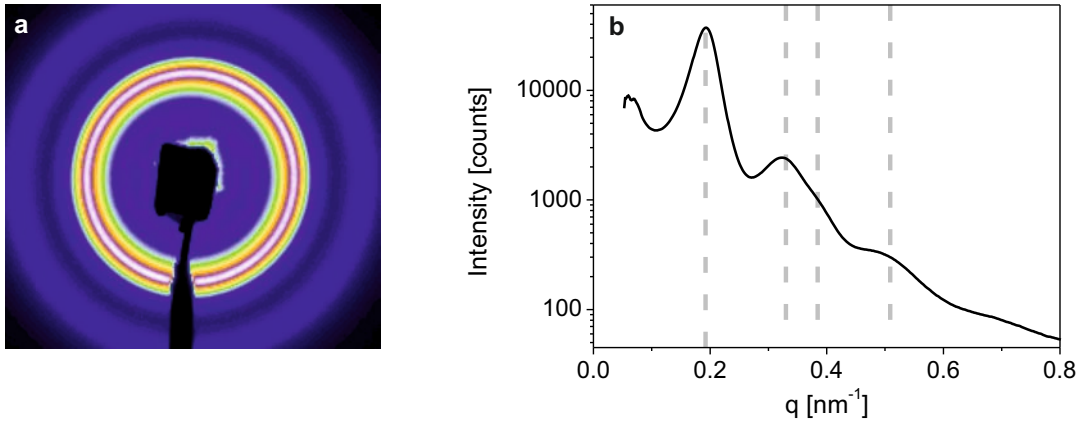
Figure 4.6: **SAXS diffraction pattern of a BCP / inorganic hybrid. a)** Example of a 2D SAXS image of a phase separated PI-*b*-PEO)/TiO$_2$ sample prepared in this study. **b)** Radially integrated SAXS data with expected peak positions $q_{hkl}/q_{100} = 1$, $\sqrt{3}$, $\sqrt{4}$, $\sqrt{7}$ for an array of hexagonally packed cylinders.

Dynamic light scattering

In dynamic light scattering experiments (DLS), also known as photon correlation spectroscopy or quasi-elastic light scattering, temporal fluctuations in the speckle pattern of objects in solution are employed to yield their characteristic properties, such the particle size distribution, the Zeta potential or the molecular weight distribution of macromolecules.

The speed at which particles diffuse due to Brownian motion is measured by the intensity fluctuations of their speckle pattern. Comparing the intensity signal (I(t)) with the signal

obtained at later times ($I(t+\tau)$, $I(t+2\tau)$, $I(t+3\tau)$) provides the contribution of slowly (large) and fast (small) diffusing objects in the sample volume. The correlation function $G(\tau)$ of the scattered intensity is therefore defined as

$$G(\tau) = \frac{\langle I(t)\,I(t+\tau)\rangle}{\langle I(\tau)\rangle}, \tag{4.10}$$

with τ expressing the time difference of the correlation. For a large number of monodisperse particles, the correlation function is a single exponential decay function with the time delay τ:

$$g_1(\tau) = A[1 + B\exp(-2\Gamma\tau)], \tag{4.11}$$

where A is the baseline of the correlation function and B is the intercept. The decay rate Γ is defined as

$$\Gamma = Dq^2, \tag{4.12}$$

where D is the translational diffusion coefficient given by the Stokes‑Einstein equation and

$$q = \frac{4\pi n}{\lambda_0}\sin\left(\frac{\theta}{2}\right), \tag{4.13}$$

where n is the refractive index of the dispersant, λ_0 is the wavelength of the laser and θ is the scattering angle. For polydisperse samples, Equation 4.10 can be written as

$$G(\tau) = A[1 + Bg_1(\tau)^2], \tag{4.14}$$

where $g_1(\tau)$ is the sum of all exponential functions that are contained in the correlation function. A comprehensive derivation of the DLS signal can be found in reference [35]. In Figure 4.7 a typical autocorrelation function $g_1(\tau)$ is plotted for a single exponential function of a single speckle.

The particle size distribution can then be obtained from the correlation function through a variety of algorithms. Usually a sum of multiple exponential curves is fitted to obtain the distribution of particle sizes, e.g. NNLS (non-negative least squares) or CONTIN. The obtained size distribution is by intensity. Using Mie and Rayleigh theory the sample intensity distribution can then be converted into a volume distribution. However, due to the fact that the intensity of light from elastic Rayleigh scattering scales as $I\alpha\,d^6$, conversion into volume fractions results in relatively high standard deviations, when particle diameters are much smaller than the laser wavelength [36].
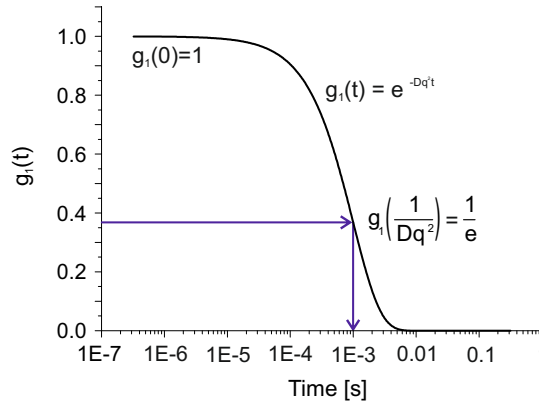
Figure 4.7: **Ideal autocorrelation function** $g_1(\tau)$**, where a single exponential function can be used to fit the speckle intensity with time.**

The Einstein-Stokes equation 4.15 describes the relation between the observed translational diffusion coefficient D and the hydrodynamic diameter of the particle $d_{\text{iam, hyd}}$:

$$d_{\text{iam, hyd}} = \frac{kT}{6\pi\eta D} \tag{4.15}$$

where T is the temperature, k is the Boltzmann's constant, η is the fluid viscosity, and D is the translational diffusion coefficient. Other shapes may also be modelled [37].

Dynamic light scattering was employed in this study to measure particle size distributions of hydrolysed sol, synthesised nanocrystals or colloidal suspension between 2 nm and 1 μm. Experiments were carried out on a Malvern Zetasizer ZS instrument in backscattering mode (collection angle 173 °) and adjustable penetration depth according to the scattering properties of the solution [38].

4.2.3   Spectroscopy techniques

Ellipsometry

Ellipsometry is a non-destructive technique to determine the refractive index, absorbance, thickness or optical anisotropy of a thin film. The technique bears its name from the underlying principle: the determination of a change in polarisation of initially elliptically polarised light upon reflection off a sample. The change in polarisation is represented by the so-called ellipsometric angles Ψ and Δ, which correspond to the amplitude ratio and phase difference upon reflection. These parameters can subsequently be related to the optical properties of the investigated film. The electric field components parallel (E_{p}) and perpendicular (E_{s}) to the plane of incidence are treated separately and can be described by the Fresnel reflection coefficients $r_{\text{p}} = |r_{\text{p}}| \exp^{i\delta_{\text{p}}}$ and $r_{\text{s}} = |r_{\text{s}}| \exp^{i\delta_{\text{s}}}$. For an experimental set-up shown in Figure 4.8,

the detected and incident field components E_{out} and E_{in} can be described in form of so-called Jones matrices [39]:

$$\begin{pmatrix} E_{\text{p, out}} \\ E_{\text{s, out}} \end{pmatrix} = \begin{pmatrix} r_{\text{pp}} & r_{\text{sp}} \\ r_{\text{ps}} & r_{\text{ss}} \end{pmatrix} \cdot \begin{pmatrix} E_{\text{p, in}} \\ E_{\text{s, in}} \end{pmatrix}. \tag{4.16}$$

In a polariser - compensator - sample - analyser configuration, the Jones reflection matrix R is:

$$\underbrace{R(\theta_a) \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} R(-\theta_a)}_{\text{analyser (a)}} \quad \underbrace{\begin{pmatrix} r_p & 0 \\ 0 & r_s \end{pmatrix}}_{\text{sample (s)}} \quad \underbrace{R(\theta_c) \begin{pmatrix} 1 & 0 \\ 0 & i \end{pmatrix} R(-\theta_c)}_{\text{compensator (c)}} \quad \underbrace{R(\theta_p) \begin{pmatrix} 1 & 0 \\ 0 & 0 \end{pmatrix} R(-\theta_p)}_{\text{polariser (p)}}, \tag{4.17}$$

where θ_a, θ_c and θ_p are the angles of analyser, compensator and polariser with respect to the plane of incidence, and $R(\pm\theta_{a,c,p})$ are the rotation matrices:

$$R(\pm\theta_{a,c,p}) = \begin{pmatrix} \cos\theta_{a,c,p} & \pm\sin\theta_{a,c,p} \\ \mp\sin\theta_{a,c,p} & \cos\theta_{a,c,p} \end{pmatrix}. \tag{4.18}$$

The ellipsometric angles Ψ and Δ then follow with

$$\tan\Psi = \frac{|r_p|}{|r_s|} \tag{4.19}$$
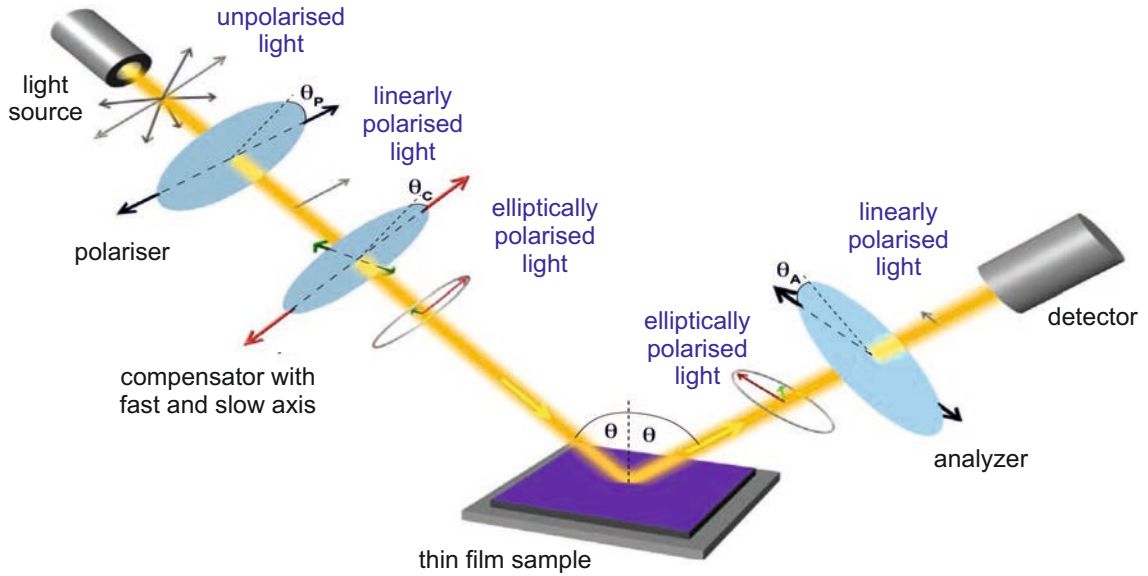
$$\Delta = \delta_p - \delta_s. \tag{4.20}$$

Figure 4.8: **Experimental set-up for ellipsometric thin film characterisation.** This configuration is known as p-c-s-a: polariser - compensator - sample - analyser. *Adapted with permission from [25]. Copyright 2011 Springer Science+Business Media.*

Ellipsometry of optical films is an indirect technique, i.e. access to the optical constants is only possible by regression analysis with a model that includes known parameters and reasonable estimates of the fitting variables. The quality of the iteratively obtained best fit can be evaluated by a mean free error value (MSE), which is a measure of the difference between the measured and modelled optical response.

In this work two different techniques were used, imaging ellipsometry and spectroscopic ellipsometry. Imaging ellipsometry was carried out on a commercial instrument (Nanofilm "ep3se"). The built-in imaging set-up, consisting of a 5x magnifying lens and a spatially resolving CCD camera, allows to choose an area of interest. The polarisation change by the sample is then determined by nulling ellipsometry. This technique involves the rotation of polariser and analyser to find the minimum detection signal at a fixed angle of the compensator. The "nulling condition" therefore corresponds to a position, where the light reflected off the sample is linearly polarised and subsequently blocked off by the analyser, set at $90°$ with respect to the axis of linear polarisation. In order to improve the fitting quality, measurements are repeated for a range of angles of incidence θ. While imaging ellipsometry operated with nulling condition allows to determine the optical constants with high accuracy, this is limited to a fixed wavelength of incident light. In order to obtain spectroscopic values for refractive index and absorption, a spectroscopic ellipsometer was used (J.A. Wollam "alpha-SE", spectral range $380 - 900 \, \text{nm}$). This instrument does not operate using a nulling principle (which would be too time consuming) but only has a rotating compensator positioned behind the sample. The element turns in discrete steps and records at every position the intensity of all wavelength channels [40].

Microspectroscopy

Microspectroscopy is essentially the quantitative study of light-matter interactions with the spatial resolution of a visible light microscope. This is realised by coupling a spectrometer to the microscope's beam path, as illustrated in Figure 4.9. The microspectroscopy set-up used in this study, consisted of an Olympus BX-51 microscope and an Ocean Optics QE 65000 spectrometer. By default the build-in halogen lamp of the microscope with a spectral range of $\sim 380 - 860 \, \text{nm}$ was employed as light source but alternative sources of wider spectral distribution (e.g. a combined deuterium tungsten halogen with a spectral range of $\sim 215 - 2000 \, \text{nm}$, Ocean Optics "DH-2000") or a narrow line-width laser can be coupled in. A computer-controlled x-y-translational stage (Prior Scientific "ProScan II") allows the movement of the sample with sub-μm accuracy. The use of magnifying lenses imply a certain angular spread in the wave vector distribution, which is determined by the numerical aperture

of the lens. In order to keep the wave vector dispersion to a minimum, most experiments were carried out with a 5x magnifying objective (NA = 0.15, Olympus "UIS2 MPlanFLN"). With fixed magnification, the spot size of detection depends on the core dimensions of the optical fibre, acting as a pinhole in the conjugate to the focal plane. Using fibre diameters between 50 μm and 1000 μm, the collection spot size therefore be varied between 15 μm and 300 μm.
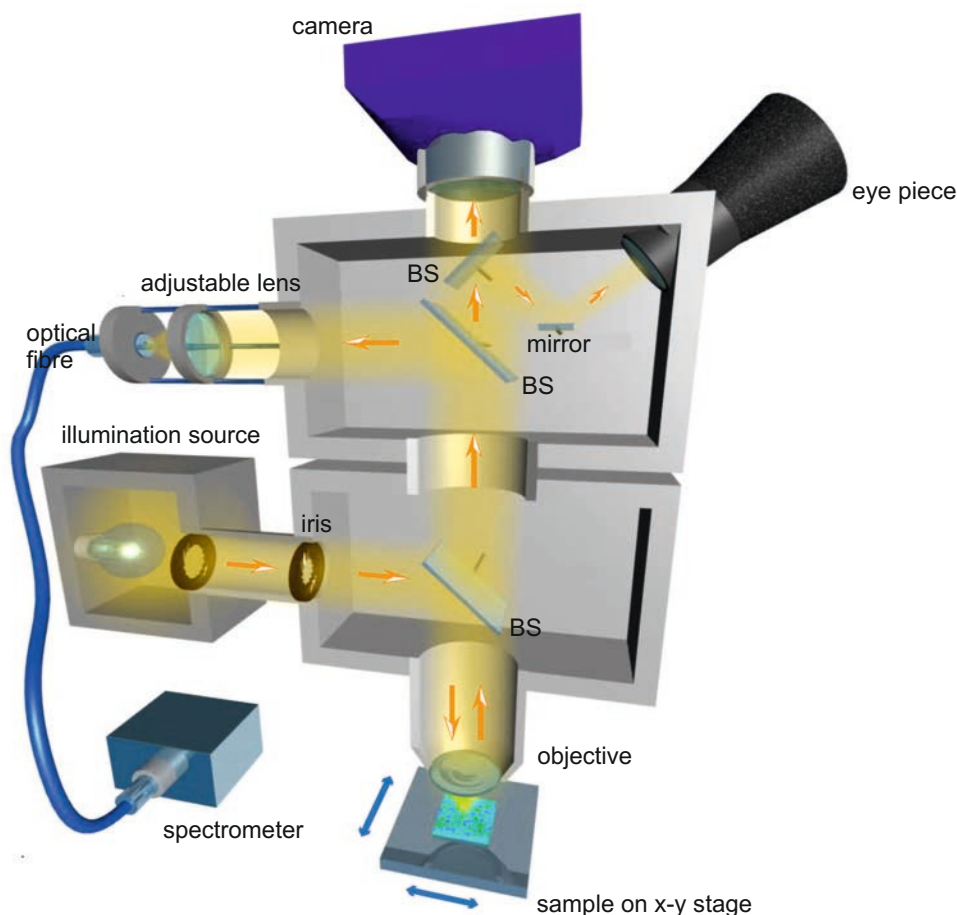
Figure 4.9: **Microspectroscopy set-up.** The conventional set-up of a light microscope is extended by the addition of a spectroscopy compartment, which is connected via a beamsplitter (BS) to the instrument's main beam path. Sampling of the spectrometer is carried out via an optical fibre that is mounted in the conjugate of the focal plane and acts as a pinhole. *Adapted with permission from [25]. Copyright 2011 Springer Science+Business Media.*

Fourier transform infrared spectroscopy

Fourier transform infrared spectroscopy (FT-IR) is a technique to investigate the molecular fingerprint of a sample by measuring its absorption in the infrared frequency range. Sampling is typically carried out in a range of $\lambda \sim 0.78 - 1000$ μm, which corresponds to a wavenumber of $\tilde{\nu} = 1/\lambda \sim 13000 - 10$ cm^{-1}. FT-IR therefore allows to quantify transitions between quantised

vibrational energy states. In a non-linear molecule the number of possible vibrational modes is $3N - 6$, where N is the number of atoms in the molecule. Six degrees of freedom are determined by the collective translational and rotational motion of the molecule. The energy difference between the ground state and the first excited state of most vibrational modes is typically in the mid-infrared ($\sim 4000 - 400\,\mathrm{cm^{-1}}$). Many vibrational modes only have large displacements for a specific hot spot, while the rest of the molecule has no or little influence. These modes allow the determination of specific functional groups and enable the classification of the molecule [41].

FTIR instruments are typically based on a Michelson-interferometer, which encodes an interference pattern by the addition of a modulated optical path difference of one-half to the IR-beam. The measurement of absorption via an interferogram allows to sample a multitude of frequencies simultaneously. Transformation into a frequency spectrum is then accomplished via Fourier transformation [42].

In this work FTIR was carried out on a commercially available instrument (Thermo Scientific "Nicolet iS10"). This allowed to monitor the decomposition of marker molecules under photocatalytic decomposition. The investigated molecule, stearic acid, showed three characteristic features in the observed range that enabled the quantitative determination in the sample volume: the asymmetric in-plane CH stretching mode of the CH_3 group ($\tilde{\nu} \sim 2958\,\mathrm{cm^{-1}}$) as well as the symmetric ($\tilde{\nu} \sim 2923\,\mathrm{cm^{-1}}$) and asymmetric ($\tilde{\nu} \sim 2853\,\mathrm{cm^{-1}}$) CH stretching modes of the CH_2 group.

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Block copolymer-induced structure control for inorganic nanomaterials

5.1 Introduction

The conditions for structure-control in a co-assembly approach using block-copolymers (BCPs) as structure-directing host and an inorganic sol as guest material have been discussed in Section 1.2.3. Four requirements have to be fulfilled in order to reach equilibrium morphologies: (1) the guest material needs to exhibit selective interaction with one block of the polymer, (2) the inorganic material has to disperse into small units in comparison to the length scale of the polymer chain, (3) the kinetics of the gelation process need to be slow in comparison to the time duration of the polymer phase separation, and (4) a common solvent system has to dissolve all components and enable even and sufficiently slow evaporation of the volatile species.

Condition one can easily be met. Most polymer structure-directing agents (SDAs) have a hydrophilic poly(ethylene oxide) (PEO) block, which interacts with a polar inorganic guest by forming hydrogen bonds [1, 2]. Various strategies can be employed to tune the reactivity of the inorganic sol-gel transformation in order to meet condition number two. Typically, hydrolysed sols is stabilised in form of < 4 nm sized colloids to allow complexation with the PEO chain. In contrast, condition number three and four still pose a major challenge for structure control of certain materials, which shall be discussed in the following.

The SDA driven co-assembly of silica has led to remarkable results over the years, indicating that all four conditions can be fulfilled in this materials system for the assembly of bulk materials. For PI-*b*-PEO in combination with a silica-type sol, all equilibrium morphologies of a diblock copolymer phase diagram have been reported, including inorganic-rich spheres,

hexagonally arranged cylinders, gyroids, lamellae and the corresponding inverse arrangements of hydrophobic and hydrophilic components [3, 4]. For the most widely studied materials couple of PEO-*b*-PPO-*b*-PEO (Pluronic) in conjunction with sol-gel-derived silica, equilibrium morphologies have been realised where the inorganic materials resides in the majority component of lamellae, hexagonal cylinders, gyroids and spherical arrangements [5, 6].

The general applicability of the SDA approach is mostly limited by two aspects. For many applications, such as in batteries, supercapacitors, dye-sensitised solar cells, fuel cells and electrochromic devices, the morphology has to be fabricated in a thin film, where the evaporation kinetics of the solvent greatly complicates the equilibration of the phase morphology [7]. Further challenges emerge when extending the SDA approach from silica to other materials, such as transition metal oxides. For TiO_2, high chemical reactivity and multiple stable coordination states of the titanium precursor greatly limit the control over the kinetics of the sol-gel reaction. As an example, the hydrolysis of titanium alkoxide $Ti(OR)_4$ is 10^5 times faster than that of the silica counterpart $Si(OR)_4$ [8]. Routes to decelerate the gelation of the inorganic sol include the addition of stabilising ligands, reacting under acidic conditions or non-hydrolytic synthesis. Usually a significant amount of aqueous HCl is added in order to obtain a stable sol for BCP-directed material assembly [5]. This, however, results in an oversupply of water (typically four times as much as needed for hydrolysis), which consequently resides in the hydrophilic block and impedes the simultaneous evaporation of volatile components from both blocks in a non-aqueous solvent mixture.

Table 5.1 presents an overview of commonly employed SDAs. The widely-used BCP Pluronic exhibits a much lower Flory-Huggins interaction parameter χ in comparison to the PHB-*b*-PEO and the PI-*b*-PEO systems. This means that polymer phase separation occurs on significantly slower time scales, which is the reason why most successful material routes towards equilibrium morphologies involve daylong preparation under controlled humidity and temperature. As an example, high order in Pluronic-directed thin films with gyroid morphology was achieved by aging of the precursor solution for 10 days, followed by annealing of the coated film for 12 hours after deposition [9]. In contrast, morphologies in PI-*b*-PEO-directed approaches typically form within minutes [10].

A high χ interaction parameter enhances phase separation with long range order and allows faster processing as well as lower sensitivity to the preparation conditions. This comes, however, at the expense of higher dissimilarity in the solubility of the components. When using the BCP Pluronic, water and ethanol are good solvents for both polymer blocks and the inorganic material. In contrast, PHB and PI are not water-soluble, and overall solubility in aqueous solutions can only be achieved by limiting the volume fraction of these hydrophobic components [15]. Non-hydrolytic sol-gel chemistry and the use of polar solvents may in principle be one

Table 5.1: Comparison of structure-directing agents for ordered mesoporous silicates [11].

	PEO-b-PPO-b-PEO (Pluronic)	PHB-b-PEO (KLE)	PI-b-PEO
Flory Huggins χ at 50 °C	0.085	~ 0.33	0.33
M_n (kg/mol)	2 – 13	8 – 10	10 – 84
wt% PEO	30 – 70 %	37 – 57 %	8 – 38 %
Solubility in water / alhohol	yes	limited	limited
Hybrid morphologies	CM, iHEX, G, L	CM	(i)CM, (i)HEX, PN, G, L
Pore size range (nm)	5 – 10 nm	12 – 13	11 – 50
References	[5, 6, 12, 13, 14]	[15]	[4, 16, 17]

i: inverse; CM: close-packed micelles; HEX: hexagonally arranged cylinders
G: gyroid; L: lamellae; PN: plumbers nightmare

route to overcome these solubility issues but control over the non-hydrolytic reaction pathways proves difficult, especially for TiO_2 [18, 19].

This chapter presents strategies to overcome the outlined limitations in order to fully exploit the potential of the PI-b-PEO SDA system for morphology control in the bulk and in thin films.

5.2   Experimental

Three different BCPs were used as structure-directing agents: I) PI-b-PEO with $M_{n,tot}$ = 34.4 kg/mol and 28.4 vol% PEO, II) PI-b-PEO with $M_{n,tot}$ = 91.6 kg/mol and 31.2 vol% PEO and III) PI-b-PS-b-PEO with $M_{n,tot}$ = 53.4 kg/mol and 29.4 vol% PEO. See Table 4.1 for details. The polymer was weighed and subsequently dissolved in a solvent system of choice, such as tetrahydrofuran (THF, 99.97 %), an azeotrope solvent mixture of 72.84 wt% toluene (99.8 %) and 27.16 wt% 1-butanol (99 %) or anisole (anhydrous, 99.7 %).

Preparation of TiO_2 morphologies in the bulk and in thin films

Titanium containing sol was synthesised by quickly adding 0.69 ml of HCl (37 %) into 1 ml of titanium ethoxide (purum) under vigorous stirring at ambient conditions. Depending on the inorganic to organic weight ratio, the adequate amount of sol was subsequently mixed with PI-b-PEO copolymer in 7 ml THF (99.97 %). For a weight ratio of 1:1 between the resulting TiO_2 after fabrication and the polymer in initial solution, 0.44 ml sol was added to 0.1 g BCP. After solvent evaporation in a Petri dish at 50 °C, the hybrid material was redissolved in an azeotrope solvent mixture of toluene (apolar, 99.8 %) and 1-butanol (polar, 99 %) and then either processed by solvent casting in a covered Petri dish at 50 °C to obtain bulk material or

spin coated for thin film processing. The dry hybrid material was subsequently annealed by slow ramping to 130 °C (180 min linear ramp, 30 min dwell). Where indicated, calcination was carried out at 500 °C (90 min ramp, 2 hour dwell).

Preparation of silica-type thin films

Aluminosilicate sol was prepared as follows: 2.8 g (3-glycidyloxypropyl)trimethoxysilane ($\geq$ 98 %) and 0.32 g aluminum-tri-sec-butoxide (97 %) were mixed with 20 mg KCl (99.9995 %) and promptly placed into an ice bath. In a first hydrolysis step, 0.135 ml of 10 mM HCl was added dropwise in 5 s intervals at 0 °C and stirred for 15 min. After warming the solution to room temperature, 0.85 ml aqueous HCl (10 mM) was further added dropwise. The sol was then stirred for 20 min before adding to the polymer solution in a mixing ratio, which was defined by the weight of the resulting aluminosilicate compared to the weight of polymer in the initial solution. After subsequent stirring for another 60 min, the solution was processed by spin coating or evaporation-controlled blade coating. Ensuing solvent evaporation, the hybrid films were annealed on a hotplate by slowly increasing the temperature to 200 °C (180 min linear ramp, 30 min dwell). In a final step, the organic component of the hybrid films was removed by reactive ion etching in oxygen plasma (30 min, 100 W, 0.33 mbar, STS Instruments, 320PC RIE).

5.3 Results and discussion

5.3.1 Block copolymer induced structure control in hybrid bulk assemblies

As outlined in the introductory section, the use of hydrolytic sol-gel chemistry poses an inherent challenge to the use of PI-*b*-PEO with a majority block of the hydrophobic PI. A typical approach for the synthesis of anatase TiO_2 therefore consists of separately preparing a hydrolytic sol containing the titanium precursor and a solution of the BCP in THF. The two solutions are subsequently mixed before the solvents are evaporated. The resulting morphology of a self-assembled hybrid material is shown in the transmission electron microscopy (TEM) images in Figure 5.1a. For all bulk samples shown in this section, specimens were prepared by ultra-microtomy to allow imaging in transmission mode.

The one-pot procedure, where the mixed solution is slowly allowed to evaporate in a Petri dish at 50 °C under a glass dome, results in a micellar arrangement. This is somewhat similar to reported morphologies for the PEO-*b*-PHB SDA system [15]. The reason for micellar

arrangement may be multifold. For a mixture of 5 wt% water and 95 wt% THF, the solvents should form an azeotrope with a common boiling point of 66 °C [20]. The low solubility of the PI polymer block in a water-rich solvent mixture at the later stages of solvent evaporation may therefore not be the origin for the micellisation of the system. Another reason may be associated with the fast evaporation of THF, one of the rare solvents that dissolves all components. This can result in quenching of the phase morphology by the TiO_2 condensation reaction before the equilibrium morphology is reached. In order to overcome micellisation, an additional step in the fabrication procedure was introduced in form of a solvent exchange. The initial mixture was slowly dried in a Petri dish and subsequently redissolved in a blend of 1-butanol and toluene, which was mixed in a volume ratio that allowed the formation of an azeotrope [21]. The azeotrope exhibits a boiling point of 105 °C and should enable good solubility of hydrophilic and hydrophobic components. The resulting morphology after the subsequent second evaporation process is shown in the TEM image in Figure 5.1c. Here, the TiO_2 is arranged in an inverse hexagonal matrix, which is surrounded by PI cylinders. This observation is consistent with small angle X-ray scattering (SAXS) results of the specimen, shown in Figure 5.1b. While the scattering pattern of the as-made sample is reminiscent of a micellar arrangement of pores, the reflection peaks of the redissolved sample align well with a morphology of hexagonally arranged cylinders. This is a convincing indication that the approach resulted in a better solubility of the hybrid material, leading in combination with the slower evaporation of the solvents to a close resemblance of the phase separated hybrid material to a BCP morphology near thermodynamic equilibrium.
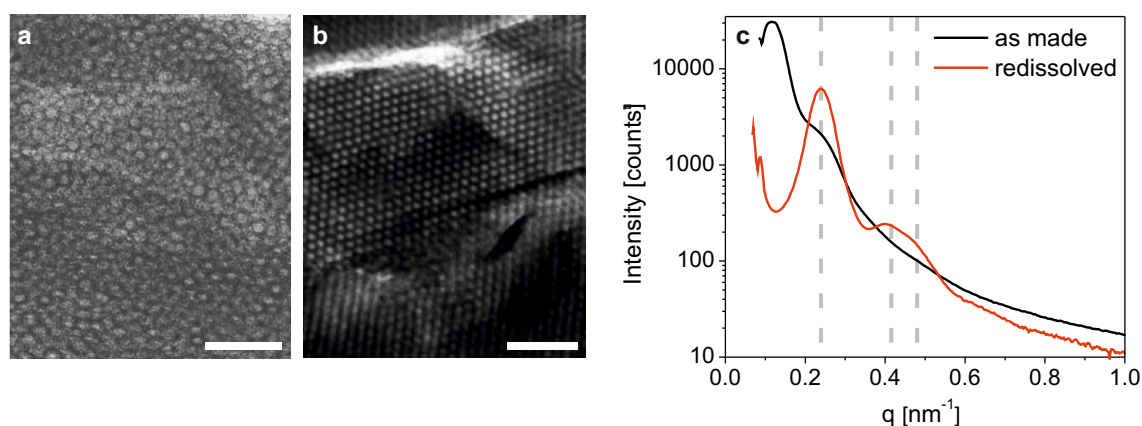
Figure 5.1: **Bulk co-assembly of PI-*b*-PEO & TiO_2: effect of annealing conditions.** TEM images of samples that were made **a)** without and **b)** with the described redissolving step under otherwise identical experimental conditions. Scale bars represent 500 nm. **c)** Radially integrated SAXS patterns of both samples, where $q = 4\pi \sin\theta/\lambda$ (see Chapter 4). The vertical lines correspond to a hexagonal arrangement of cylinders, which are observed for the redissolved sample.

The versatility of this approach is demonstrated in Figure 5.2, where the mixing ratio of TiO_2 and polymer in the initial solution was varied to access a range of morphologies. According to the TEM images, a 1:3 ratio, defined by the mass of the resulting TiO_2 after calcination to the mass of polymer in solution, resulted in the formation of TiO_2-rich cylinders surrounded by a PEO matrix. The vol% of the PI block used in this study was 77 %, which means that the incorporated TiO_2 must have swollen the PEO-rich phase by up to 8 vol% to drive the hydrophilic block into a hexagonal arrangement of cylinders [22]. The observed morphology is consistent with SAXS scattering data, plotted in Figure 5.2d. The position of the reflection peaks predicted for a hexagonal morphology are indicated as grey lines. When increasing the inorganic weight fraction to 1:2, the morphology observed in TEM resembled a lamellar arrangement of the hydrophilic and hydrophobic components, shown in Figure 5.2b. Consistently, the SAXS reflection peaks align with the expected peak positions for the lamellar phase. Further increase of the TiO_2 weight fraction to 3:2 resulted in an inverse hexagonal structure, where the TiO_2 resides in the majority matrix, being surrounded by PI cylinders. Different projections of the cylinders can be seen in the image plane, which clearly distinguishes this morphology from an ordered micellar array. This is supported by the corresponding SAXS data shown in Figure 5.2f, where the radially integrated scattering pattern aligns well with the expected peak positions of a hexagonal morphology.

The results presented in Figures 5.1 and 5.2 illustrate the potential of introducing a redissolution procedure after partial evaporation of the primary solvent system. Yet, the success of this approach largely depends on the appropriate timing for evaporation and redissolution. If the condensation reaction has already completed during the first evaporation step, the material will no longer redissolve. On the other hand, interrupting the primary evaporation process too early may cause a deterioration of the structure formation process by residual water. In experimental practise, the appropriate timing proved relatively robust. The primary evaporation process was stopped when a sudden increase in viscosity inhibited further flow of residual solvent in the Petri dish. Subsequent work on understanding solubility parameters and the kinetics of the sol-gel reaction enabled Stefik *et al.* to introduce a one-pot approach based on the toluene/1-butanol azeotrope solvent system and hydrolysis under less acidic conditions [11]. Shifting from a conventional oversupply of 4 mol H_2O per mol of titanium alkoxide to a molar ratio of 1 in conjunction with the appropriate timing allowed to suppress the discussed micellisation issues and led to equilibrated morphologies without the need of a redissolving step. Yet, high TiO_2 loadings, such as an inorganic to organic ratio of 3:1 led to the precipitation of the inorganic material. In contrast, the presented two step procedure enables highly inorganic mixtures up to a ratio of 5:1. This is an indication that during the primary evaporation cycle the TiO_2 has already partially condensed on the local scale (typically 1-4 nm [23]), lim-
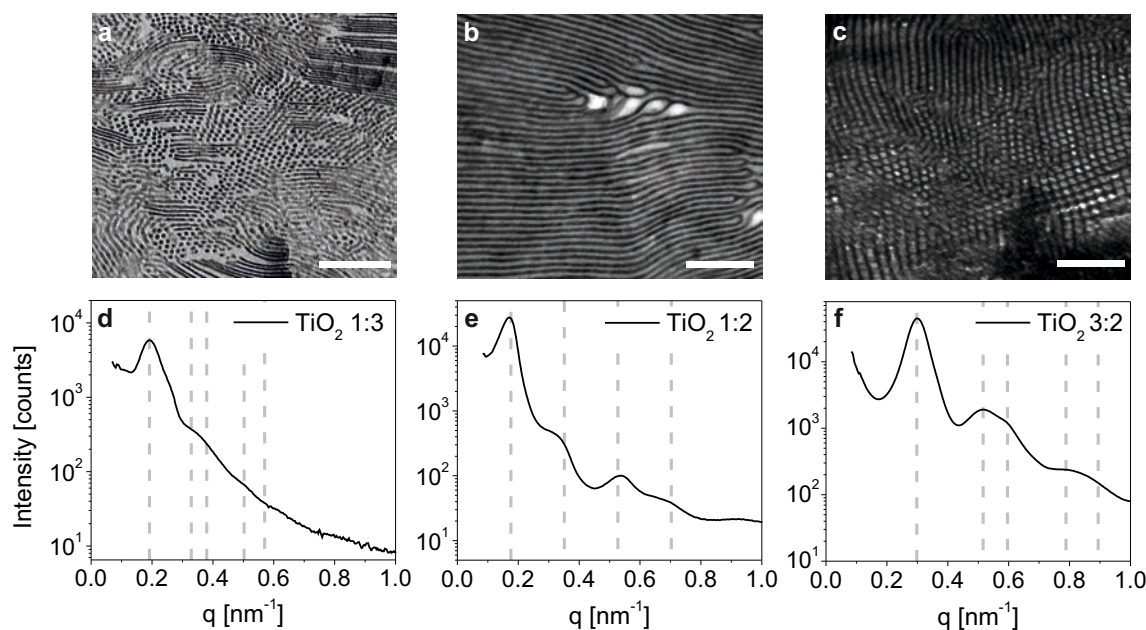
Figure 5.2: **Bulk co-assembly of PI-*b*-PEO & TiO$_2$: effect of mixing ratio. a**) - **c**) Transmission electron micrographs of hybrid PI-*b*-PEO/TiO$_2$ samples. Samples were derived from inorganic to organic mixing ratios of **a**) 1:3, **b**) 1:2 and **c**) 3:2, which led to a variation of the morphological arrangement from TiO$_2$-rich cylinders in an organic matrix (1:3), to TiO$_2$ lamellae (1:2) and for a high TiO$_2$ loading (3:2), to organic cylinders in TiO$_2$-rich inverse hexagonal matrix. Scale bars represent 500 nm. **d**) - **f**) Corresponding radially integrated plots from SAXS of the samples. Expected peak positions for a **d**), **f**) hexagonal arrangement of cylinders, and **e**) lamellae are indicated as grey lines, calculated from the position of the first reflection peak.

iting the amount of water produced during the second evaporation. In addition, a redissolving step decouples material synthesis from film processing. It is therefore possible to redissolve the material in a well defined manner up to high concentrations ($< 20\,$wt%), which greatly enhances control over thin film processing.

5.3.2   Inorganic thin films with controlled pore size and porosity

The morphology of a thin film that was processed via redissolution and spin-coated from an azeotrope solution is shown in Figure 5.3a. After deposition, the film was lifted onto a TEM grid for imaging. The observed morphology is consistent with a hexagonal arrangement of micellar pores. Corresponding characterisation of the specimen by SAXS is presented in Figure 5.3b in form of a radially integrated plot of the scattering pattern. Bulk processing of the identical solution by solvent casting resulted in an inverse hexagonal TiO$_2$ matrix, surrounding PI cylinders (Figure 5.1b). In contrast no long-range order can be observed in the hybrid film. The greatly increased evaporation kinetics during spin coating has presumably prevented the

hybrid film from reaching thermodynamic equilibrium.

It is important to note that this micellar assembly represents a 3D bicontinuous network of TiO$_2$ with pores on the 10-nm length scale, a morphology that offers isotropy and structural integrity. Both characteristics are not inherent to most BCP morphologies at thermodynamic equilibrium. An inverse hexagonal arrangement of cylinders is not isotropic and needs to be aligned for pore access. Other BCP morphologies, such as hexagonal inorganic cylinders, do not offer structural integrity as the features tend to cluster upon removal of the surrounding matrix [24]. As the micellar film morphologies proved reproducible and yielded promising results when used in dye-sensitised solar cells and optical coatings, this film formation strategy was further explored. Though micellar, the pores showed close-packing in a hexagonal arrangement and exhibited well defined optical interfaces. These characteristics are a direct consequence of the dissolution procedure. In contrast, when processing the films directly from the initial THF-based solution, the films were rough and of greatly varying thickness. This can be attributed to the volatility of THF, preventing the formation of a well-defined film during spin coating, see Section 4.1.3.

Control over pore dimensions, porosity and well-defined percolation paths are beneficial for many applications of mesoporous films. In the widely established nanoparticle-route, pores are generated by the random dense packing of nanometre-sized particles and subsequent sintering. The pore geometry is therefore defined by the remaining interstitial space between close-packed particles, which results in a highly heterogeneous size and shape distribution [25]. Pore generation in a SDA approach to mesoporous thin films is fundamentally different.
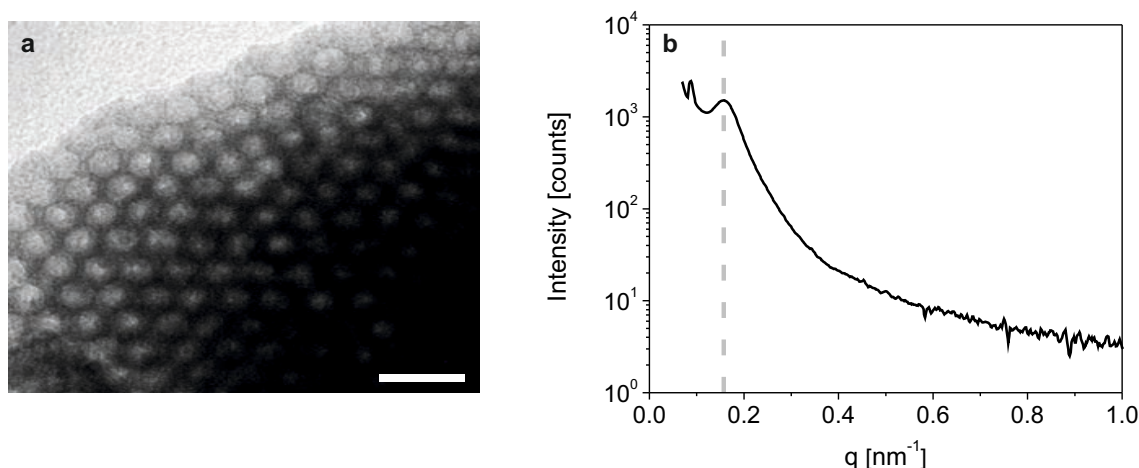

Figure 5.3: **Thin film co-assembly of PI-*b*-PEO & TiO$_2$. a)** TEM image of the ordered, hexagonally arranged micellar hybrid film produced by spin-coating the redissolved material. **b)** Corresponding radially integrated SAXS pattern of the specimen, where only the first order reflection peak was observed.

The volume occupied by the sacrificial polymer block that incorporates no inorganic material will result in empty space upon calcination. Hence, the molecular weight of this block should be the main parameter to define the pore size distribution. In Figure 5.4a and d SEM top views of mesoporous silica-type films are presented, which were generated by SDAs of different molecular weights but identical mixing ratio of inorganic material and polymer (1:1 in weight). Both films exhibit a highly porous mesostructure, resembling an inverse opal morphology as known for larger length scales from colloidal templating (see Chapter 1.2.4). SEM images of porous inorganic films after the polymer has been removed by oxygen plasma etching or calcination are highly reminiscent of the hybrid morphology shown in Figure 5.4a. These findings are similar when using either TiO_2 or aluinosilicate as the inorganic sol. The accessibility and continuity of the pores over several micellar planes is clearly discernible. No solid overlayer has formed that could impede the infiltration of the network.

Figure 5.4a-c illustrates the pore size analysis procedure for a mesoporous film stemming from a PI-*b*-PEO BCP of $M_{n, tot} = 34.4$ kg/mol (71.6 vol% PI). From the raw SEM top view micrograph a binary image was obtained by applying an intensity threshold. For comparison,
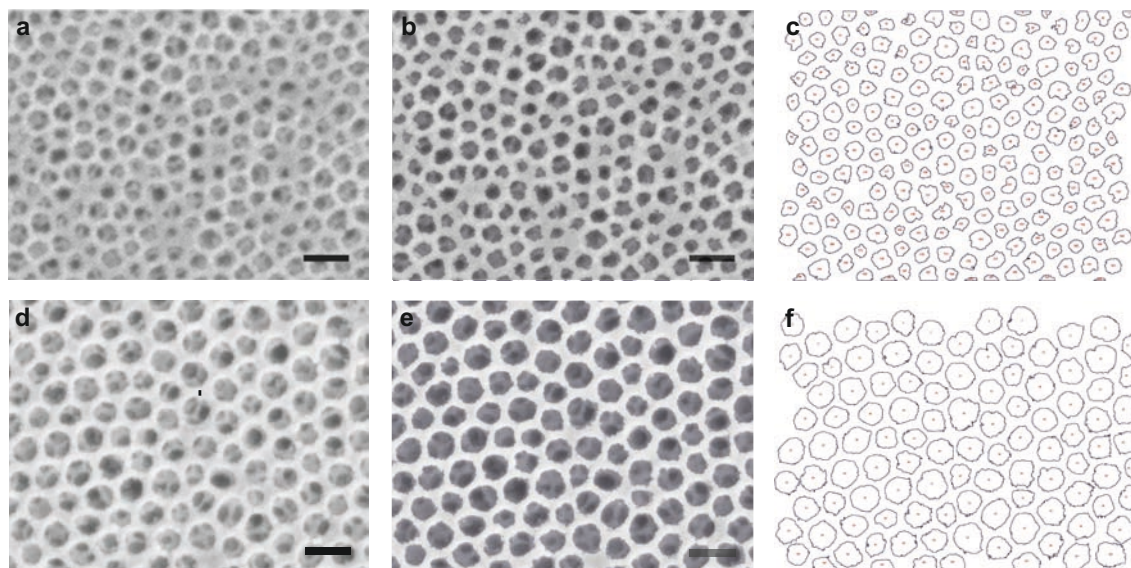
Figure 5.4: **Pore size analysis in thin films.** Pore size analysis for mesoporous silica-based films derived from the co-assembly of aluminosilicate sol and PI-*b*-PEO BCP. **a)** SEM top view micrograph of a mesoporous film that served for image analysis ($M_{n, tot} = 34.4$ kg/mol). **b)** Superposition of original SEM image and an abstracted binary image, which was derived by applying an intensity threshold. **c)** Arithmetic pore identification by the "ImageJ" led to a pore size distribution of 33 ± 6 nm [26]. For comparison, manual analysis yielded an average pore size of 34 ± 4 nm. **d)** - **f)** Image analysis for a mesoporous film derived from a BCP of $M_n = 91.6$ kg/mol led to pore size distribution of 52 ± 6 nm. This compares to a manual measurement of 52 ± 4 nm. The ratio of inorganic material to polymer was in both samples 1:1. Scale bars represent 100 nm.

the raw and binary image are superimposed in Figure 5.4b. The binary image was subsequently analysed with the image analysis software "ImageJ" [26], which yielded a pore size distribution of 33 ± 6 nm. Based on the raw image, the pore size distribution was also determined manually, rendering 34 ± 4 nm. In Figure 5.4d-e a similar pore size analysis is presented for an increased molecular weight of the pore forming PI block ($M_{n, tot} = 91.6$ kg/mol, 68.8 vol% PI). Here, a mean pore diameter of 53 ± 6 nm resulted from image analysis and a distribution of 52 ± 4 nm was measured manually. An increase of $\sim 55 - 60\%$ is in good agreement with scaling laws of polymer chain statistics [27]. The radius of gyration for an unperturbed polymer chain scales with $\sqrt{N}$ (where N is the degree of polymerisation), i.e. by a factor of 1.59, when increasing the molecular weight of the PI block from 24.8 kg/mol to 62.7 kg/mol.

In addition to the control over the resulting pore size distribution, control over the porosity is another important parameter for many applications of mesoporous thin films. Subject to structural integrity, the mixing ratio in the initial solution between inorganic sol and sacrificial SDA should determine the resulting porosity after calcination. The variation in porosity of an inorganic film can be characterised by optical means, as this parameter is reflected in the effective refractive index of the films. The experimentally found dependence of refractive index on the polymer weight fraction can be seen in Figure 5.5a. Samples series of different molecular weight polymers are plotted separately and show a similar dependence. Following the Bruggeman effective medium approximation (see Chapter 2.5), a quasi-linear relationship between the polymer weight fraction, the resulting pore volume and hence the corresponding refractive index is expected. In fact, the measured refractive index scales quasi-linearly for low polymer weight content. When increasing the organic fraction to ≥ 50 wt%, the experimentally observed value deviates from the expected scaling. This is probably related to a progressive shrinkage of the film for an increasing polymer weight fraction. An organic weight content of 50 % effectively corresponds to a polymer volume content of ~ 67 %. It is therefore reasonable to assume that such high polymer volume fractions lead to a certain densification of the inorganic network after removal of the SDA. Nevertheless, the porosity could steadily be increased by extending the polymer weight fraction to 66 %. The measured refractive index was $n = 1.135 \pm 0.007$ ($\lambda = 632$ nm), which corresponds to a relative pore volume of ~ 71 %.

These results imply that the presented route allows to tune the porosity over a wide range, i.e. from ~ 30 % to over 70 %. This is in line with studies of Garcia *et al.* who reported that the hydrophilic PEO block can accommodate large amounts of guest material (up to 20 times its volume) via hydrogen bonds [4]. Similar porosity tuning was achieved for mesoporous TiO_2, which will be presented in Chapter 8.
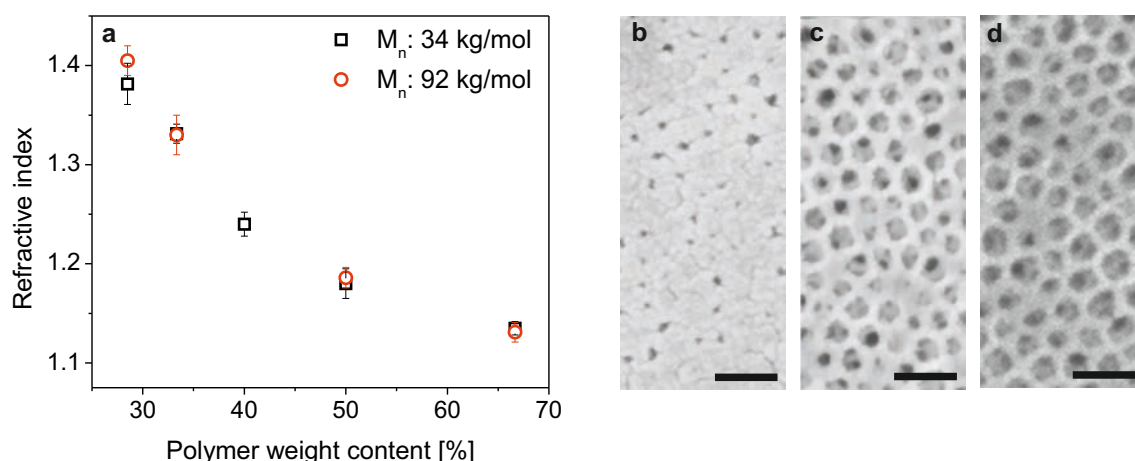
Figure 5.5: **Porosity tuning of mesoporous films.** **a)** Dependence of refractive index of the resulting inorganic film on the polymer weight content in the initial hybrid solution. Results for two polymers of different molecular weight are shown. The polymer weight fraction was determined as percentage with respect to the total weight of polymer SDA and resulting silica-type material. The refractive index values are shown for $\lambda = 632\,nm$. **b)** - **d)** Scanning electron microscopy top view of mesoporous silica-type films, stemming from a solution of PI-*b*-PEO BCP (M_n = 34.4 kg/mol) and aluminosilicate sol. The polymer weight fraction was **b)** 33 %, **c)** 40 % and **d)** 50 %. Scale bars represent 100 nm.

5.3.3   Highly ordered network morphologies in silica-based thin films

The presented route to mesoporous films via dense packing of sacrificial micelles is robust in terms of processing conditions and offers fine control over porosity and pore size. However, some applications rely on a specific space symmetry of the materials configuration, which can only be achieved by BCP microphase separation close to thermodynamic equilibrium. One example are optical metamaterials, described in Chapter 2.5. Overcoming micellisation and kinetic trapping in thin films would enable to access the same range of BCP equilibrium morphologies as reported in this chapter for bulk materials. Materials arrangement of particular interest are continuous multiple network structures, such as the double gyroid. These phases do not have the discussed drawbacks of other BCP equilibrium morphologies, such as domain alignment, pore accessibility and structural collapse [28]. Extending from an AB diblock copolymer to an ABC terblock copolymer greatly increases the gyroid composition window in the phase diagram, from $2 - 6\,\%$ in an AB to $4 - 14\,\%$ in ABC systems [29, 30]. Furthermore, a ternary system offers several configurations of the gyroid morphology. One example is the double gyroid, with an ABCBA core-shell structure (space group: $Ia\bar{3}d$, Q^{230}), another one the chiral alternating gyroid, where two individual networks A and C are embedded in a matrix of B (space group: $Il4_132$, Q^{214}).

An ABC terblock copolymer in form of a PI-*b*-PS-*b*-PEO chain structure has already been

used as a SDA for transition metal oxides, in particular TiO_2 and Nb_2O_5 [31]. After removal of the polymer, porous inorganic morphologies were observed in the bulk material which closely resembled the corresponding equilibrium morphologies of the BCP melt, i.e. chiral network structures, such as the non-centrosymmetric alternating gyroid Q^{214} as well as centrosymmetric network morphologies.

The aim of the present study was the extension of these results to thin films. For this purpose, the previously described evaporation-controlled blade coating technique was developed, see Section 4.1.3. Basically, a commercially available set-up was modified by the integration of a programmable heating element and an enclosed chamber with solvent-rich atmosphere, fed by a saturated carrier gas. As a result, the evaporation kinetics of the solvent were greatly reduced due to the increased partial pressure in the saturated environment. Controlling the substrate temperature during deposition allowed to further promote phase separation by increasing the chain mobilities. Based on results from solvent-casting of thick films, a temperature of 50 °C was found to optimise the competing kinetics of polymer phase separation and gelation of the inorganic material [11, 31].

In the experiments the same PI-*b*-PS-*b*-PEO terblock copolymer was used as in reference [31]. The mixing ratio between sol and polymer was adjusted to result in the phase space of the alternating gyroid structure in the ternary diagram [30]. The aluminosilicate should therefore reside in the hydrophilic minority component C, leading to an inorganic single gyroid network upon removal of the SDA. Figure 5.6 shows an overview of cross-sectional SEM images for different silica-type thin film morphologies after exposure to an oxygen plasma. When blade coated in an unsaturated solvent atmosphere from a toluene/1-butanol azeotrope solution, the films exhibited a random network structure that showed the expected porosity but did not resemble the expected equilibrium morphology (Figure 5.6a). The use of an enclosed chamber with saturated solvent atmosphere during the coating process significantly slowed down the drying process from less than a minute to over 15 min for a μm-thick film. The increased drying time resulted in a more equilibrated structure with indications of the expected network morphology, as discernible in Figure 5.6c.

A change of the solvent from the toluene/1-butanol azeotrope system to anisole further improved structure control and resulted in a morphology that closely resembled an alternating gyroid formed by the silica-type material (Figure 5.6d). Anisole has a boiling point of 154 °C, further extending the drying time during which microphase separation can take place. As a result, films consistently exhibited high structural order throughout the film. Yet, at the bottom interface a lamellar arrangement was observed, which can be attributed to a preferential interaction of the polar PEO/inorganic phase with the substrate [32, 33]. Dipcoating in a solution of octadecyltrichlorosilane in cyclohexane greatly reduced the surface polarity due to

the formation of a silane monolayer on the substrate. Films prepared on silanised substrates showed no discontinuity of the network structure at the substrate interface, as evidenced in Figure 5.6f. The long-range order of the obtained network structures is depicted in Figure 5.6g.

Further characterisation, e.g. by grazing incidence SAXS, is required to confirm possible non-centrosymmetric configurations of the structural unit cell. In principle, such network structures should be ideally suited for applications in optical films, where linear dichroism and gyrotropic light propagation have been observed for chiral alternating gyroid templates upon infiltration of the network with gold and subsequent removal of the polymer [34]. Shifting
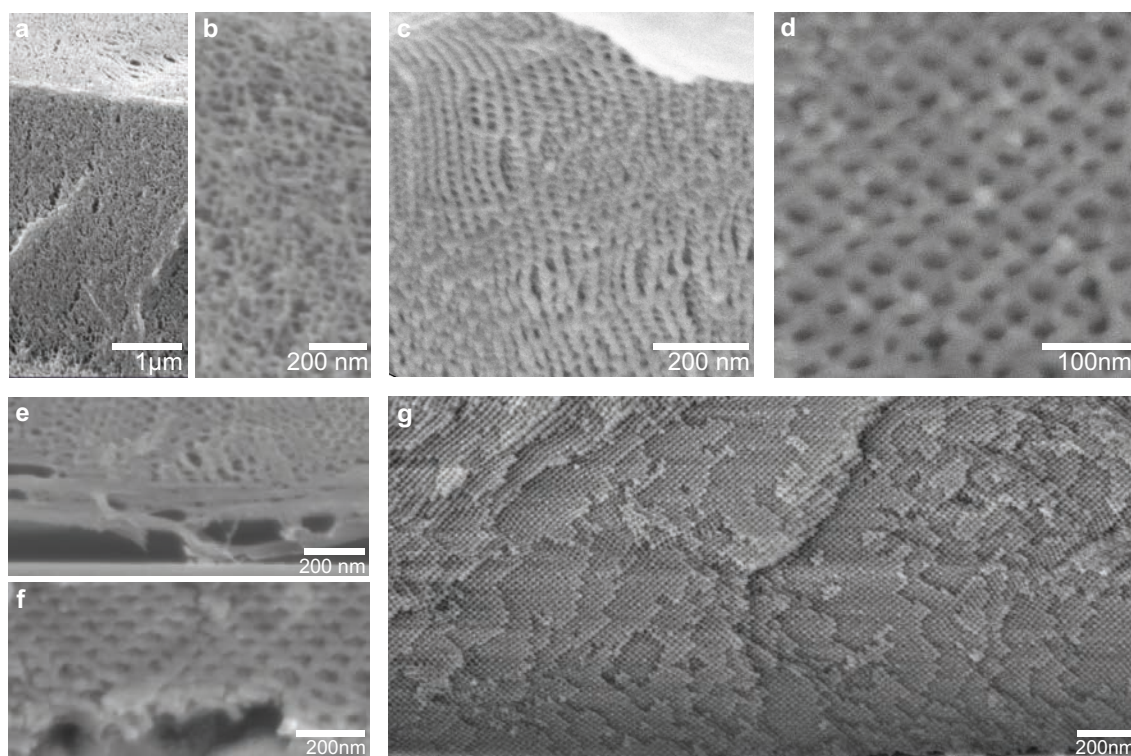
Figure 5.6: **Assembly of silica-type thin films into highly ordered network morphologies.** The PEO/aluminosilicate content was adjusted to a volume fraction of 30 % which should result in an alternating gyroid morphology under equilibrium conditions [31]. After deposition and annealing, films were exposed to an oxygen plasma to remove the SDA. All cross-sectional imaging was carried out by SEM. **a)** - **b)** Mesoporous film prepared from a toluene/1-butanol azeotrope solution in unsaturated atmosphere. **c)** Film prepared in saturated solvent atmosphere under otherwise identical conditions. **d)** - **g)** Resulting morphologies obtained by the use of anisole and deposition in a saturated atmosphere. **d)** Close-up view of the resulting network morphology. **e)** Preferential interaction of the polar PEO/inorganic phase with the substrate led to the formation of lamellae at the substrate interface. **f)** After silanisation of the substrate, the bottom interface shows no indication of preferential interaction. **g)** Zoomed-out view of highly ordered network morphology in thin a film.

from the previously reported organic to an inorganic template may greatly improve the long-term stability, in terms of temperature and abrasion resistance as well preventing oxidation of the plasmonic metals, such as silver.

Silica-type networks offer high temperature stability. Crystallisation accompanied by structural collapse only occurs well above $1000\,°C$. The presented mesoporous films are therefore ideal candidates for the crystallisation of infiltrated functional materials at high temperatures [35, 36]. The "hard" scaffold may subsequently be removed by wet etching with hydrogen fluoride to reveal a free-standing film of the infiltrated material after crystallisation at temperatures that would otherwise lead to structural collapse [37].

Reduction of the aluminosilicate film in magnesium vapour may lead to the formation of silicon domains in a free-standing network [38]. This would make the materials system ideally suited as anodes in lithium-ion batteries [39]. Insertion of lithium ions typically poses a major challenge for the anode due to the imposed volume change for every charging and discharging cycle [40]. The length scale of the SDA-directed structure, the dispersion of aluminium-rich and silicon-rich domains and the structural integrity of a gyroid network upon volume contraction make this route ideally suited to improve anode stability and capacity.

5.4   Conclusions

Several strategies are presented in this chapter that are geared towards controlling structure formation of inorganic materials by BCP co-assembly with PI-*b*-PEO. The use of solvent exchange enabled to overcome kinetic barriers for structure formation of sol-gel-derived TiO_2. The resulting hybrid material arrangement of hydrophobic PI and hydrophilic PEO/TiO_2 beared close resemblance with typical BCP morphologies in the melt at thermodynamic equilibrium. By the variation of the mixing ratio between the inorganic guest and the polymer host in solution, different morphologies were obtained, such as hexagonal TiO_2-rich cylinders in an organic matrix, TiO_2 lamellae or a TiO_2 inverse hexagonal matrix.

In thin films, processing via redissolution of the hybrid material led to the formation of ordered micelles in a close-packed lattice. Tuning of the BCP's molecular weight and mixing ratio between inorganic sol and organic SDA allowed fine tuning of the porosity and refractive index of the resulting mesoporous films after removal of the polymer host. While the micellar assembly does not form at thermodynamic equilibrium, it represents a very promising route to mesoporous films. A hexagonal arrangement of pores offers morphological isotropy and structural integrity and allows full accessibility of the porous network. Processing is greatly simplified and highly robust with respect to the various parameters. In addition, the proposed redissolving step decouples material synthesis from film processing and therefore allows pre-

cise control of the resulting film thickness.

Thin film deposition by evaporation-controlled blade coating prevented micellisation and enabled the realisation of highly ordered and free standing network structures in silica-type films. The high porosity, accessibility and fine structural order of the network makes the films an excellent candidate for a variety of applications, such as optical films, high temperature scaffolds and lithium-ion batteries.

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Chapter 6

Crystal growth in block copolymer-derived mesoporous TiO₂

6.1   Introduction

The interest in nanocrystalline, mesoporous TiO$_2$ has intensified in recent years for a variety of "green" applications such as dye-sensitised solar cells (DSCs) [3], photocatalysis [4], electrochemical capacitors [5], sensors [6] and electrochromic devices [7]. Typically, a mesoporous film is obtained by the sintering of $10-20$ nm sized TiO$_2$ nanoparticles that are predominatly of the anatase crystal structure [8]. The resulting network of randomly packed nanocrystals and intermediate pores expands the surface area of the film by a multitude (up to 1000 fold [3]), but this comes at the expense of greatly deteriorated electronic properties. While the electron mobility in single crystalline anatase TiO$_2$ is usually on the order of $\mu \sim 10 \, \text{cm}^2/\text{Vs}$ [9, 10], this value decreases by orders of magnitude to around $\mu \sim 10^{-1} - 10^{-5} \, \text{cm}^2/\text{Vs}$ in nanoparticle films [11, 12, 13]. The reasons for the diminished electron transport in nanoparticle films are numerous. The high density of traps, predominantly located at grain boundaries and at the particles' surfaces, cause generated electrons to mostly populate localised states below the conduction band and only diffuse towards the electrode in iterative cycles of thermal detrapping and trapping [14, 15] (see Chapter 3.1 for further details). While low electron mobility was previously not a major limiting factor, new technologies, such as solid state dye-sensitised

solar cells (ss-DSCs), are suffering from poor charge carrier transport, which appears to limit charge collection and thereby power conversion efficiency [16].

Novel electrode architectures have evolved in recent years with the aim to improve the electronic properties of the TiO$_2$ photoelectrode (see Chapter 3.1). Furthermore, the poor morphological control in nanoparticle networks [8] may impede mass transport of bulky molecules, such as reactants and certain redox couples, which limits the performance of photocatalytic devices and DSCs [17, 18]. In other device types, such as ss-DSCs, the smallest pores represent a barrier for effective infiltration of the porous film by other functional materials [19].

The use of block copolymers (BCPs) to guide the morphological arrangement of mesoporous TiO$_2$ is a promising concept for improved structure control [20, 21, 22]. This has also led to remarkable results in DSC systems, at least for film thicknesses below 1 μm [23, 24]. Yet, BCP-templated or co-assembled morphologies typically suffer from poor crystallinity and electronic properties that are correlated to the limited structural stability at high crystallisation temperatures. In order to prevent the collapse of the morphology, calcination is usually carried out at temperatures around 400 °C, which results in poor overall crystallinity in comparison to sintered nanoparticle films [25, 26]. Transformation into a fully crystalline material at high calcination temperatures often leads to the collapse of the structure [26]. This can be attributed to the fact that nanocrystals grow at elevated crystallisation temperatures to diameters of $10 - 20$ nm. This exceeds by far the length scale of the widely used PEO-*b*-PPO-*b*-PEO (Pluronic) structure-directing agent (SDA) and therefore causes the micro-morphology to break down during crystallisation. Alternative concepts include backfilling the mesopores with carbon or silica [27] or elaborate annealing and crystallisation protocols [21] to enhance temperature stability. The addition of preformed nanocrystals in order to decrease the crystallisation temperature of amorphous TiO$_2$ is another promising concept, but it remains a challenge to simultaneously achieve high crystallinity and structural integrity [28]. Furthermore phase impurities have been reported in this materials system with finite amounts of TiO$_2$ (B) and traces of rutile, both of which are not favourable for solar cell operation [29, 30].

Recently, BCP systems of higher molecular weight were introduced, such as PHB-*b*-PEO. The increased pore walls, compared to Pluronic-derived materials, allow crystallisation at up to 700 °C for periods of 10 min [22, 26]. The introduction of this new SDA therefore enabled the increase of anatase phase fraction within the mesoporous morphology from previously reported 40 % to 100 %. On the other hand, pore size ($\sim$ 8 nm) and porosity ($\sim$ 30 %) are still limited. This is a consequence of the relatively low molecular weight and the low volume fraction of the pore forming PHB block ($M_{\text{n, tot}}$ $\sim$ $8 - 10$ kg/mol; vol%$_{\text{PHB}}$ $\sim$ $43 - 63$ %). Recent studies on the use of PI-*b*-PEO as SDA for the co-assembly of inorganic materials have pointed out several intrinsic advantages of this particular BCP system [31, 32, 33]. The

well-established polymerisation procedure enables synthesis of large molecular weight BCPs (up to $M_{n, tot} \sim 100$ kg/mol) with a high fraction of the pore forming PI-block (typically around $75 - 90\%$) and a relatively narrow size distribution ($D \sim 1.02 - 1.05$) [34, 35]. In principle, this should allow the development of mesoporous architectures that enable extended crystallite growth and exhibit pores large enough for infiltration and mass transport through the inorganic network.

In this chapter, the evolution of crystal growth in highly ordered mesoporous TiO_2 films is investigated. The kinetics of the crystallisation process was resolved *in situ* by wide angle X-ray scattering (WAXS), from the sol-gel-derived amorphous TiO_2 to highly crystalline anatase. Furthermore, impedance spectroscopy and the implementation of porous TiO_2 films in liquid electrolyte and ss-DSCs were employed to correlate the evolution of crystallinity with electron transport properties and photovoltaic performance of devices.

6.2 Experimental

Material fabrication

A titanium containing sol was prepared by the rapid addition of 0.69 ml HCl (37%) to 1 ml titanium ethoxide (purum) under vigorous stirring. A solution of 0.1 g poly(isoprene-*block*-ethylene oxide) copolymer (PI-*b*-PEO) (M_n = 35.7 g/mol, 23 wt% PEO) in 7 ml of tetrahydrofuran (THF) was prepared alongside. After 90 min of stirring, 0.87 ml of the resulting sol was added to the polymer solution, before the volatile components were evaporated at 50 °C in a Petri dish. Shortly after, the dry material was redissolved in an azeotrope solvent mixture of 72.8 wt% toluene (99.8%) and 27.2 wt% 1-butanol (99%). Films were then deposited by spin-coating of the 20 wt% solution (5 s, 1500 rpm) onto pre-cleaned silicon substrates or fluorine doped SnO_2 (FTO) coated glass sheets (Nippon Sheet Glass, TEC15). The dry hybrid material was subsequently annealed by slow ramping to 130 °C (180 min linear ramp, 30 min dwell) and then calcined under conditions as explained in the text. *In situ* WAXS during the crystallisation process was carried out on a Bruker D8 Advance diffractometer with integrated furnace. A calibrated tube furnace (TSH12, Elite furnaces) was otherwise used for high temperature treatment.

Material characterisation

WAXS experiments were carried out *in situ* during heating on a Bruker D8 Advance diffractometer over an angular range of $22° - 32°$ with a step size of $0.0143°$ and a total scan time of 5 min. A heating rate of 10 °C/min was used unless otherwise stated. Samples were measured

during crystallisation in air for up to seven hours, representing 84 consecutive X-ray scans. The obtained raw data was corrected for the CuK$_{\alpha 2}$ radiation by the Bruker software 'EVA'. To obtain the peak broadening caused by the finite size of the anatase crystallites, a Voigt function was fitted to the peaks. The Lorentzian and the Gaussian parts of the Voigt function were determined using the approximation of Olivero and Longbothum [36]. The peak width was then corrected for machine broadening by subtracting (by deconvolution) the broadening of a monocrystalline silicon reference sample. The Debye-Scherrer equation was subsequently employed to obtain a mean crystallite diameter of the peak broadening [37]. As in similar studies, the dimensionless number $K = 0.89$ was used as Debye-Scherrer constant [25].

Small-angle X-ray scattering (SAXS) of CuK$_{\alpha}$ radiation was carried out in transmission geometry at a sample-detector distance of 1.05 m (Bruker AXS Nanostar). An acquisition time of 7500 s was used. The scattered intensity was collected with a two-dimensional Hi-Star gas-filled wire detector (1024 x 1024 channels) and background subtracted. In each case, the scattering patterns were found to be isotropic. Radial scattering intensity profiles were obtained by averaging over the azimuthal angle (from 0 to 360°) with 0.005° increments.

In order to quantify the accessible surface area for dye sensitisation, dye desorption studies were carried out according to studies by to Neale *et al.* [38]. The absorbance of the resulting light pink solutions was measured with an uv-vis spectrophotometer (HP 8453, wavelength range 190 − 1100 nm, 1 nm slit width, 0.03 % stray light). The relative amount of dye adsorbed was determined by comparing the peak height of the respective solution with the reference obtained from desorption of the film annealed at 400 °C.

For liquid electrolyte DSC assembly, the samples were sensitised with N719 as described above. Platinisation of the counter electrode was carried out by coating the FTO films with a solution of hexachloroplatinic (IV) acid in anhydrous isopropanol solution (50 mM) followed by heating to 450 °C for 15 min. The sensitised TiO$_2$ electrodes were washed in acetonitrile, dried and assembled in a sandwich type cell configuration with the platinised counter electrodes. A "hot-melt" 50 μm thick surlyn spacer (Dupont) was used to bond the working and counter electrode. A drop of iodine-based liquid electrolyte named "Robust" [39] was subsequently dispensed into a hole in the counter electrode. The cell was filled via vacuum backfilling and sealed with polyimide tape (Dupont). Liquid electrolyte DSCs (active area 0.13 cm^2) were measured under AM 1.5 simulated sunlight generated by a 300 W solar simulator (Oriel). The intensity was calibrated with a silicon photo diode (Fraunhofer ISE) and adjusted by a mismatch factor. The currentvoltage measurements were recorded by a Keithley 237 sourcemeter. The incident photon-to-electron conversion efficiency was determined by illumination with a spectrally resolved halogen lamp, which was calibrated by a silicon diode.

Nitrogen physisorption was carried out by Dr. Dominik Eder on a Micromeritics TriStar

3000 (saturation pressure of 745 mmHg). Fabrication and characterisation of ss-DSCs were accomplished by Priti Tiwana and Pablo Docampo at the University of Oxford. Impedance spectroscopy was performed by Dr. Burak Ülgüt on a Gamry Reference 600 potentiostat with the EIS300 software package, following a procedure described in reference [40]. See reference [1] for further experimental details.

6.3   Results and discussion

The co-assembly of TiO_2 into ordered domains on the nanometre scale by the microphase separation of the BCP PI-*b*-PEO is discussed in Chapter 5. The present chapter aims to shed light on the transformation of the initial hybrid film of interdigitated BCP and inorganic material into a crystalline network of mesoporous TiO_2. Typically the inorganic material results from sol-gel chemistry, i.e. it is added to the polymer solution in form of a hydrolysed sol, which then complexes with the polar PEO block of the polymer by hydrogen bonding [41, 42]. This means that the TiO_2 is initially amorphous and needs thermal activation to nucleate and grow into an anatase network, while the sacrificial organic material is simultaneously oxidised [43]. The temperature stability of the resulting mesoporous morphology is a decisive parameter to achieve highly crystalline networks with good charge carrier properties [26]. Figure 6.1 shows the thermal stability of mesoporous TiO_2 derived by PI-*b*-PEO BCP assembly. Structural order after annealing of the films and subsequent removal of the self-assembling BCP host during crystallisation was probed by SAXS, presented in Figure 6.1b. The position of the primary scattering peak after annealing at 370 °C refers to a characteristic length-scale (*d*-spacing) of 30 nm, shrinking to 27 nm after complete decomposition of the organic SDA. The first-order peak at $\sim 0.23\,\text{nm}^{-1}$ disappeared only at 740 °C, indicating a loss of structural order at this temperature. Electron microscopy confirmed these observations. Cross-sectional scanning electron microscope (SEM) images of the calcined films in Figure 6.1b and c show that the self-assembled morphology remained intact after crystallisation at temperatures of 430 °C (b) and 690 °C (c) for 400 min. The collapse of the pores observed at 740 °C is evidenced by the SEM cross-section in Figure 6.1d. Thus, the structure imposition of the BCP, organising the inorganic TiO_2 sol in a highly ordered network can be seen up to 690 °C.

   The overall crystallinity and crystallite size strongly influence charge transport properties of polycrystalline wide band-gap semiconductors and therefore play decisive roles in device applications. Time and temperature of crystal formation are important in controlling these parameters. Figure 6.2a shows wide-angle x-ray scattering (WAXS) patterns of TiO_2 films calcined for 400 min at temperatures between 400 °C and 700 °C. Up to crystallisation temperatures of 700 °C, all reflections can be indexed to anatase, confirming phase purity for these
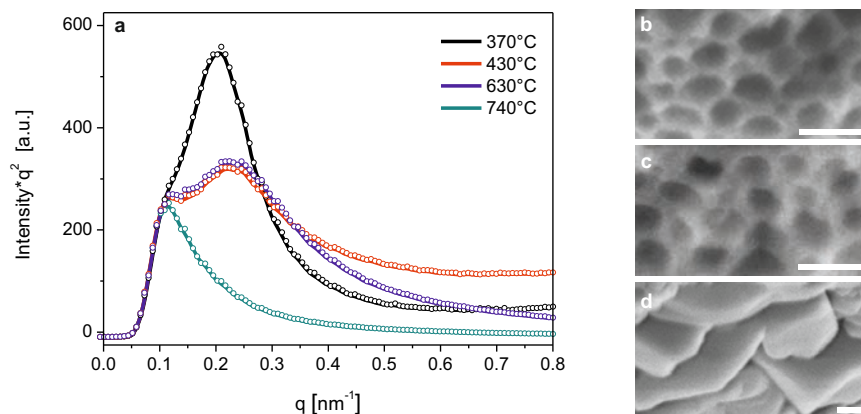
Figure 6.1: **Structural stability of BCP-derived morphology.** **a)** Radially integrated SAXS spectra for BCP-assembled TiO$_2$ heat-treated at different temperatures. The spectra are scaled in intensity to overlap in the $0-0.1$ nm^{-1} q-range. Cross-sectional SEM images of the nanostructured TiO$_2$ films calcined in air at temperatures of **b)** 430 °C and **c)** 690 °C for 400 min. **d)** Cross-sectional SEM image of a film crystallised at 740 °C which resulted in the transformation from anatase to rutile and a subsequent loss of the mesopores. Scale bars represent 100 nm.

calcination conditions [44]. The smaller angular range of Figure 6.2b shows the evolution of the width of the anatase (101) peak with temperature. Diffraction data after crystallisation at 740 °C is consistent with the coexistence of TiO$_2$ rutile, evidenced by the appearance of the rutile (110) peak at 27.3°. This is line with SAXS data shown in Figure 6.1a and suggests that the structural collapse at 740 °C is caused by the stresses involved with the lattice reconstruction from anatase to rutile. Debye Scherrer analysis of the full width at half maximum (FWHM) of the (101) peak was used to define the mean crystallite size of the polycrystalline assembly, shown in Figure 6.2c. The final crystallite size was found to be independent of the heating rate in the range of $1 - 10$ °C/min.

To investigate the time required for completion of the crystallisation process, the crystallite growth was monitored *in situ* during the calcination process by WAXS. The observed diffraction range for the scattering angle 2θ between 22° and 32° contains the anatase (101) peak, which was used for this analysis. A heterogeneous distribution of crystal sizes during the early stages of crystallisation was clearly observable by electron microscopy. This may be the reason for the poor fitting of the peak width at short crystallisation times. Following the development of the peak area with time and temperature is a more robust measure for the evolution of the crystallite size and was therefore used to follow the kinetics of the crystallisation process. A typical *in situ* scan of TiO$_2$ during calcination at 530 °C is shown in Figure 6.2d, indicating completion of the crystallisation process after about 100 min. The evolution of the overall crystallinity with time was determined by comparing the area of the anatase

peak with the final peak area after 400 min, which was defined as 100 % crystallinity. The result of this analysis is shown in Figure 6.2e, where the time required to reach values of the overall crystallinity of 50 %−98 % is plotted for a range of temperatures. While near-complete crystallinity (98 %) was obtained after $100 - 150$ min for temperatures between 530 °C and 690 °C, much longer times were needed for temperatures below 500 °C. In addition, the careful investigation of all WAXS samples in reflection (Figure 6.2a and b) and transmission (see supporting information in reference [1]) showed no sign of an amorphous hump. These results are in line with a study by Fattakhova *et al.* reporting the rapid disappearance of the amorphous signal for crystallisation temperatures between 550 °C and 650 °C [26]. It is therefore reasonable to conclude that the amorphous content in all investigated samples was very low when crystallised above 400 °C for several hours. The effect of the polymer template, spatially confining the crystallisation process, is clearly observable in Figure 6.2f. Here, the mean crystallite size was determined for a variation of the mixing ratio of inorganic and organic material in the synthesis. Lower inorganic loading hereby corresponds to thinner walls, leading to a decrease in crystallite size by ~ 30 %, as seen in Figure 6.2f. In the absence of the organic structure-directing agent, much larger crystals (> 23 nm) were observed.
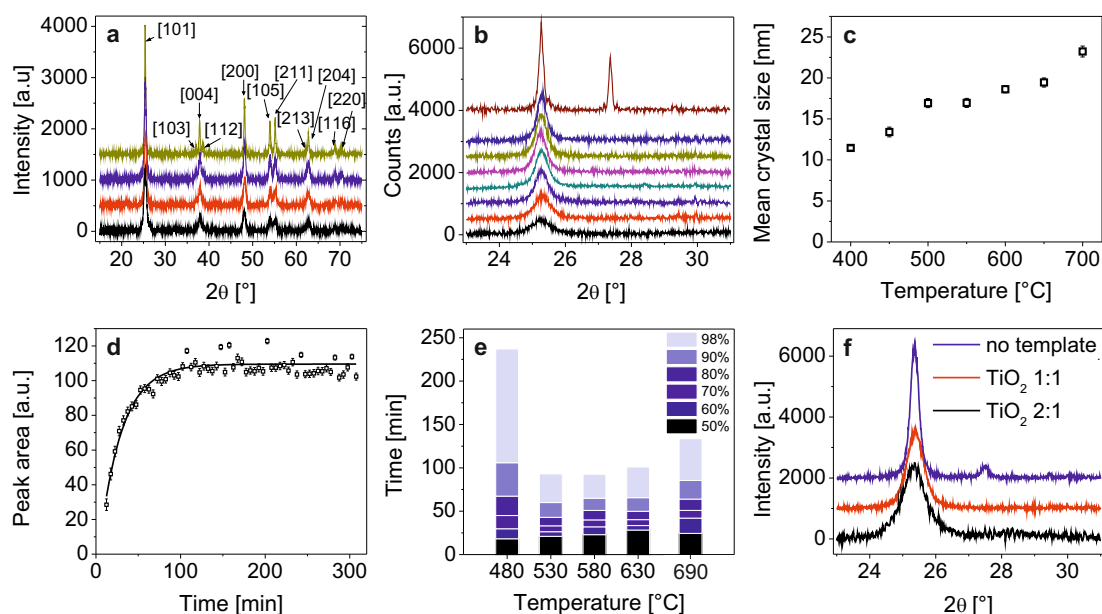
Figure 6.2: **Crystallisation of TiO$_2$ anatase crystals in BCP-derived confinement. a)** Wide angle x-ray diffraction scans of mesoporous films crystallised at 400 °C, 500 °C, 600 °C and 700 °C (bottom to top). **b)** Anatase (101) crystal peak as a function of crystallisation temperature after calcination for 400 min. From bottom to top: 400 °C to 700 °C in 50 °C increments (structurally intact) and 740 °C (collapsed structure). **c)** Debye-Scherrer mean crystallite sizes after crystallisation for 400 min as a function of temperature. **d)** Evolution of crystallinity by monitoring the peak area as a function of time at 530 °C. **e)** Corresponding evolution of overall crystallinity with time for a range of temperatures. **f)** Dependence of anatase (101) peak on BCP-dictated confinement. From bottom to top; black: mass ratio TiO$_2$:BCP 1:1 (mean crystallite size: 9.5 nm); red: 2:1 (14.7 nm); blue: sol only (23.6 nm).

High resolution transmission electron microscopy (HRTEM) images of samples calcined at 400 °C and 650 °C are shown in Figure 6.3a and b, respectively. After crystallisation at 400 °C for 400 min, the specimen exhibited a heterogeneous assembly of of 10±5 nm-sized crystallites. Increasing the temperature to 650 °C, led to larger and more irregularly shaped crystals of around 20 nm in size, which probably arose from the coalescence of smaller grains. These results are consistent with the x-ray diffraction data analysis. The schematics in Figure 6.3c and d illustrate crystal growth in BCP-derived confinement at low and high temperatures, respectively. After calcination at 400 °C, dimensions of the crystals are generally smaller than the average width of the TiO$_2$ walls in the network, which is around 15 nm. As the crystals are randomly orientated, growth occurs in this regime isotropically. At higher temperatures crystal growth within the spatial constraints can only proceed anisotropically. This is in line with the observed shape of the crystallites after calcination at 650 °C (see Figure 6.3b).

The aim of this study was to investigate the interplay between crystallisation of TiO$_2$ in BCP-derived confinement and the corresponding performance of the films in DSC devices.
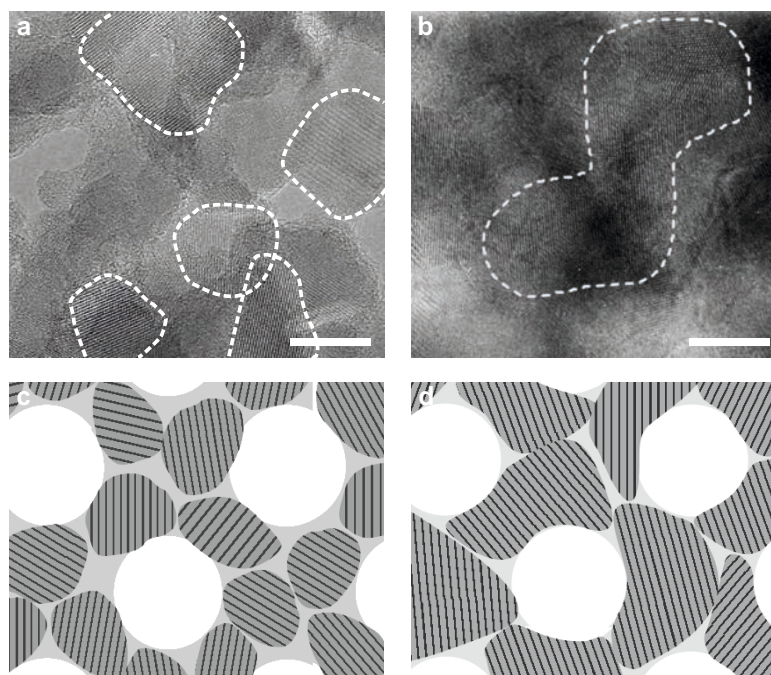
Figure 6.3: **Crystallite assembly within the mesoporous network.** High resolution transmission electron microscopy (HRTEM) images of samples crystallised at **a)** 400 °C and **b)** 650 °C. White dotted lines are superimposed on the images to visualise individual crystallites. **a)** Sample calcined at 400 °C: small, randomly oriented crystals significantly smaller than the length scale of the porous matrix are observed.**b)** Sample calcined at 650 °C: crystal size exceeds the length scale of the confinement. Anisotropic growth within the network is likely. Scale bars represent 5 nm. **c)** - **d)** Schematic illustrating crystallite size and orientation in BCP-derived networks at **c)** 400 °C and **d)** 650 °C.

The development of the accessible pores and surface area with temperature are therefore crucial parameters. Figure 6.4a shows nitrogen adsorption-desorption isotherms of films calcined at 400 °C and 650 °C, which were subsequently scraped off the substrate to reveal a powder that resembled the morphology of the film. Fitting of the Brunauer, Emmett & Teller (BET) model in the linear regime of the adsorption–desorption isotherm ($0.03 < p/p_0 < 0.25$) reveals a reduction in surface area of more than 60 %, from 42.0 m^2/g at 400 °C to 16.7 m^2/g for 650 °C [45]. A simple geometrical consideration, based on SEM image analysis, of a micellar structure with pores of 22 nm in diameter and a TiO$_2$ wall thickness of 15 nm, leads to a prediction of a surface area of around 20 m^2/g, similar to the value found for the sample calcined at 650 °C. The substantially increased specific surface area of samples calcined at 400 °C must therefore stem from an additional nanoporosity within the TiO$_2$ structure on smaller length scales than resolvable by SEM or SAXS. Figure 6.4b shows the pore distribution for both calcination temperatures as derived from the capillary condensation regime of the isotherm ($p/p_0 > 0.4$), following the Barrett, Joyner & Halenda method (BJH) [46]. The pore

size distribution is in line with the assumption that nanoporosity arises from the assembly of smaller crystallites within the matrix. This represents a significant contribution to the overall surface area for lower crystallisation temperatures. At higher temperatures the crystallites grow anisotropically within the confined structure and sinter together. At this stage only the flat walls of the BCP-defined mesostructure contribute to the exposed surface area, while the additional degree of nanoporosity within the walls is lost. Due to the limited sample quantity obtainable from thin films, these results should only be seen as a qualitative indication. Similar micellar bulk morphologies, characterised in larger quantities, typically yielded a surface area of $\sim 82\,\mathrm{m^2/g}$ when calcined at $400\,°\mathrm{C}$ and $\sim 64\,\mathrm{m^2/g}$ after crystallisation at $500\,°\mathrm{C}$. Moreover, the BJH model is disputed for severely underestimating the size of small to medium mesopores while delivering a rather broad size distribution of medium to large mesopores [47].

A more direct measure for surface accessibility is the amount of dye that is chemisorbed as a monolayer onto the TiO$_2$ surface [38]. This can be quantified by subsequent desorption of the dye. Measuring the absorbance of the desorbed solution thus allows to quantify the number of molecules chemisorbed per unit volume. The relative amounts normalised to the value at $400\,°\mathrm{C}$ are compared in Figure 6.4c for different crystallisation temperatures. The results suggest that the specific accessible surface area only varies weakly in the range between $400\,°\mathrm{C}$ and $550\,°\mathrm{C}$, but drops off for the highest calcination temperatures. This technique also takes into account steric hindrances for surface accessibility, which are associated to the spatial dimensions of the N719 dye molecule ($C_{58}H_{86}N_8O_8RuS_2$) compared to N$_2$.

Crystallinity and crystallite size distribution are important measures but it is ultimately their link to the electron conductivity, i.e. the resistivity of the mesoporous film, which de-
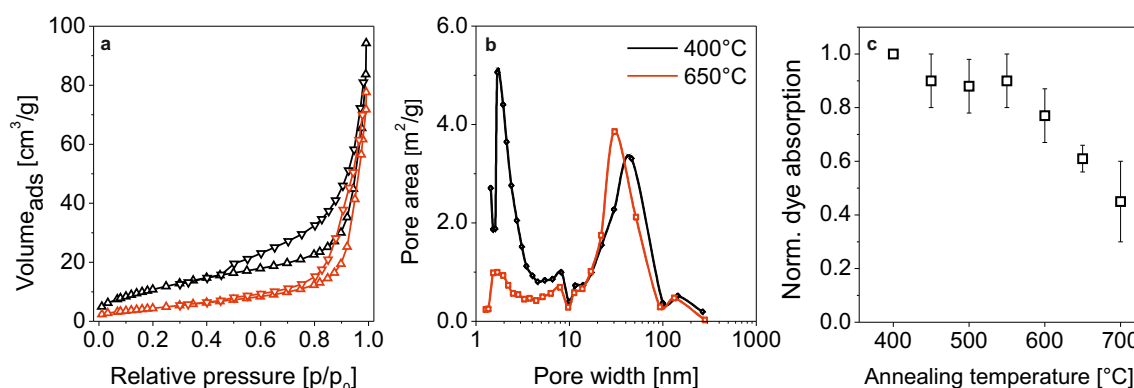
Figure 6.4: **Surface area vs. calcination temperature. a)** - **b)** Nitrogen physisorption of films calcined at $400\,°\mathrm{C}$ and $650\,°\mathrm{C}$. **a)** Adsorption-desorption isotherms for samples calcined at $400\,°\mathrm{C}$ and $650\,°\mathrm{C}$. **b)** Pore size distribution of mesoporous materials as derived by capillary condensation, following the BJH method [46]. **c)** Amount of dye adsorbed per unit area, relative the reference film calcined at $400\,°\mathrm{C}$.

termines its performance as a photoanode for DSCs. This was characterised by impedance spectroscopy measurements on complete, liquid electrolyte-based devices. The obtained data was subsequently fitted to a transmission line equivalent circuit model adapted from reference [40]. Increasing the calcination temperature from 400 °C to 650 °C reduced the resistivity by over a factor of 3. In contrast, the sheet resistance of the bare FTO substrate increased slightly over this temperature range. These observations are in line with a recent study by Janek and coworkers who compared the photoelectrochemical properties of sol-gel-derived and nanoparticle-based electrodes. They associated enhanced electronic connectivity to the superior performance of sol-gel-based materials [48]. The results of increasing conductivity and decreasing dye loading with temperature give rise to a dilemma for choosing the ideal TiO_2 sintering temperature. High temperature calcination leads to large crystallite sizes and therefore a coarser anatase network with a small number of grain boundaries per unit volume. Enhanced charge carrier transport comes at the expense of a reduced surface area, leading to a reduction in dye adsorption and therefore to a decrease in charge generation per unit volume.

This trade-off was further explored in liquid electrolyte and ss-DSCs. For liquid electrolyte DSCs, TiO_2 films were crystallised at temperatures ranging from 400 °C to 650 °C and subsequently assembled using the dye N719. In this study, 900 nm thick anatase films were used to avoid the formation of cracks that typically occurs for thicker films. While devices calcined at 400 °C and 500 °C had very similar incident photon-to-electron conversion efficiencies (IPCEs) with maxima of 22.0 % and 22.6 %, a calcination temperature of 650 °C resulted in a reduction of the $IPCE_{max}$ to 18.6 %. This decrease in IPCE most likely correlates with the reduced dye loading shown in Figure 6.4c. The corresponding current-voltage ($J - V$) curves are presented in Figure 6.5b. While all devices had comparable open-circuit voltages V_{oc}, their short-circuit current J_{sc} decreased with increasing anatase crystallisation temperature. The related power conversion efficiencies η were 2.3 %, 2.0 % and 1.5 % for 400 °C, 500 °C and 650 °C, respectively. The decrease in J_{sc} and η follows the trend in dye-adsorption and IPCE. While the values for the anatase calcination temperatures of 400 °C and 500 °C are comparable, reflecting the plateau in Figure 6.4c, the reduced values for the 650 °C data-set correlates with the drop-off in specific surface area for this temperature. This result is not surprising. In iodine-based liquid electrolyte cells, charge recombination is not believed to be a limiting factor as it occurs via a slow two-electron process [49]. Therefore, the increased TiO_2 conductivity does not outweigh the loss in specific surface area for this cell type. The situation is very different for ss-DSCs. To this end, Figure 6.5c shows the $J - V$ curves of ss-DSCs, employing the D102 dye and spiro-OMeTAD as hole-conducting medium. 400 nm-thick TiO_2 films were used. An overview of the characteristic photovoltaic device parameters is shown in Table 6.1. Increasing the sintering temperature from 350 °C to 650 °C resulted in a continuous
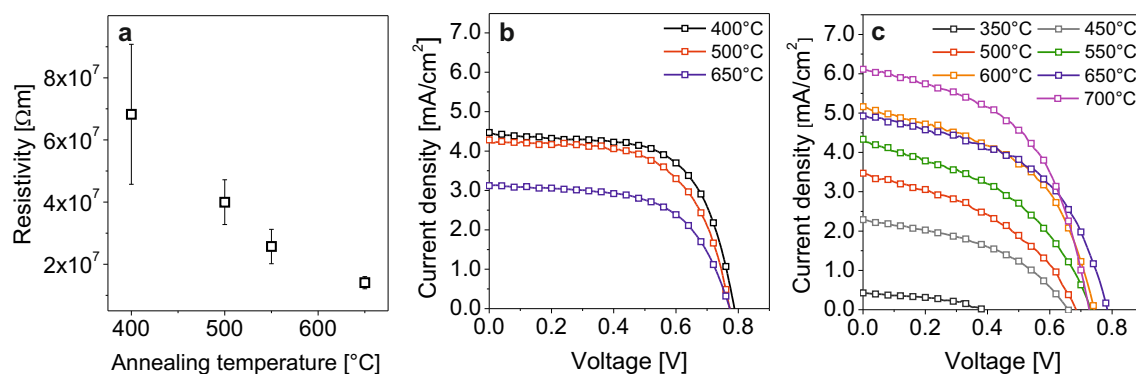
Figure 6.5: **Effects of crystallinity on device performance.** **a)** Resistivity determined by impedance spectroscopy of 900 nm thick films calcined at 400 °C, 500 °C and 650 °C. **b)** Current-voltage characteristics for liquid electrolyte DSC devices calcined at 400 °C, 500 °C and 650 °C (dye N719). **c)** ss-DSC performance of samples crystallised at 350 °C to 700 °C. Liquid and solid state devices were characterised under standardised AM 1.5 illumination of 100 W/cm^2.

increase in all relevant performance parameters (V_{oc}, J_{sc}, FF and η). The decrease in V_{oc} for samples crystallised at 700 °C might be partially due to the fact that the sheet resistance of the FTO doubled to 40 $\Omega/\square$ at these high temperatures. Nevertheless, the power conversion efficiency increased from 0.78 % for 450 °C to 2.48 % for samples crystallised at 700 °C. Since the specific surface area and dye loading are greatly reduced for the highest anatase crystallisation temperature, the results imply that the ss-DSCs strongly benefit from the increased TiO$_2$ conductivity. While earlier studies reported the relevance of crystallinity and crystal purity of mesoporous networks, it is important to note that the crystallite size is another important parameter to improve photoanode performance in devices, where the efficiency is limited by charge recombination [26]. This effect is expected to be even more pronounced in thicker devices (see Chapter 7). In contrast to conventional approaches, TiO$_2$ films were not post-treated with TiCl$_4$, which further underlines the quality of the anatase produced by this route [50].

Table 6.1: Photovoltaic device performance parameters

Calcination temperature	J [mA/cm^2]	V [V]	FF	η [%]
solid state DSC				
350 °C	0.4	0.40	0.07	0.1
450 °C	2.4	0.78	0.48	0.8
500 °C	3.6	0.73	0.47	1.3
550 °C	4.5	0.75	0.49	1.6
600 °C	5.2	0.77	0.52	2.1
650 °C	5.0	0.81	0.53	2.1
700 °C	6.1	0.74	0.55	2.5
liquid electrolyte DSC				
400 °C	4.4	0.79	0.65	2.3
500 °C	4.2	0.77	0.62	2.0
650 °C	3.1	0.77	0.58	1.5

6.4 Conclusions

The aim of this study was the exploration of the interplay of crystallisation temperature and time, anatase crystallite size and purity, mesoscopic pore structure, electric resistivity of the porous networks and performance when incorporated into a dye-sensitised solar cell. The self-assembling BCP PI-*b*-PEO is highly effective in controlling anatase crystallisation in mesoporous networks. It rapidly assembles the TiO$_2$ sol into an ordered spatial confinement that promotes crystallite growth within the matrix dictated by the polymer scaffold. Structural integrity can be maintained up to 700 °C, which results in the formation of relatively large crystallites.

When used in DSCs, the control over anatase crystal parameters afforded by this protocol presents an interesting dilemma: while anatase conductivity is markedly improved by high temperature crystallisation, this comes at the expense of specific surface area of the mesoporous scaffold. For liquid DSCs in which charge carrier recombination is not a limitation, the use of high temperature calcined anatase films therefore has a detrimental effect on device performance. In ss-DSCs, on the other hand, the reduced dye loading of the coarser TiO$_2$ network is outweighed by the improved anatase conductivity, leading to an increase in power conversion efficiency by a factor of 3 for cells employing anatase crystallised at 700 °C, compared to materials made by the previously established route.

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Chapter 7

Thin film processing of block copolymer structure-directed inorganic materials

7.1   Introduction

As outlined in the introductory chapters, mesoporosity, i.e. porosity on the sub-optical length scale, has become an essential feature in materials design for a wide range of applications, such as dye-sensitised solar cells (DSCs) [3], photocatalysis [4], electrochemical capacitors [5], chemical and biochemical sensors [6, 7] and electrochromic devices [8]. The high surface area, necessary in these interface sensitive applications, is usually generated by the random close packing of 10-20 nm sized particles, which are obtained by sol-gel chemistry and hydrothermal growth [9]. Although random in pore size and morphological order, these networks have been highly sought after due to the up to 1000-fold increase in surface area, which is a consequence of the sintering of nanometre-sized objects [3]. Nevertheless, a random network of nanoparticles (NPs) lacks detailed control over pore size distribution [9] and exhibits poor charge transport [10]. These characteristics, which are inherent to the electrode architecture, are detrimental for applications with a high demand on electron transport in the semiconductor or mass transport through the porous network [11]. Furthermore the infiltration of a random network of heterogeneously-sized pores is more difficult as the smallest pores act as a barrier and thereby limit effective pore filling over the entire film thickness [12].

One particular example is the solid state dye-sensitised solar cell (ss-DSC, see chapter 3).

Despite the fact that block copolymer (BCP)-assembled photoelectrode architectures exhibit a much higher control over the pore morphology and offer enhanced charge carrier transport, they still lag behind the maximum conversion efficiencies of NP films [13]. While BCP-derived photoelectrode have outperformed NP cells in thin layers (below 1 μm), this performance enhancement could not be extended to thick films [14, 15]. A fundamental problem is the large volume contraction of the host-guest assembly during the various processing steps. Film shrinkage is induced by the evaporation of residual solvent, the condensation of the inorganic network, the degradation of the polymer and the crystallisation of the TiO_2. As a consequence, layers exceeding several hundred nanometres in thickness are subject to crack formation and delamination [16], which limits the thickness of the photoanode and therefore light absorption [17].

Considerable progress has been made in recent years to overcome this issue. Carbone and coworkers proposed a sequential coating and step-by-step calcination to release stresses during the stack build-up [18]. Unfortunately the removal of the polymer during the cyclic calcination step caused a densification of the underlying layers with each subsequent coating. Grosso and coworkers improved this approach by altering the dip coating technique and protecting the pores after each deposition cycle with a sacrificial polymer to maintain the mesoporosity throughout the structure [19]. The group of Li reported the fabrication of several μm thick mesoporous films by the introduction of a synthesis procedure that is based on the deposition of an already gelled solution, followed by a post-deposition treatment in silicone oil [20]. Other approaches include the incorporation of NPs to prevent the formation of microcracks [21, 22] and multilayer deposition combined with a sequential rapid calcination process [23]. One appealing concept to reach thicker films is to decouple material manufacturing and film fabrication by synthesising and crystallising the mesoporous TiO_2 in the bulk. The as-made material is then processed into a paste and deposited onto a substrate following established routes for NP-based DSCs. Thick films for highly efficient liquid electrolyte DSCs have been reported [24], but the initial self-assembled morphology does not seem to be reflected in the final mesoporous film [25]. Most previous approaches to thick BCP-directed films have been applied to liquid electrolyte DSCs, where demands on a fully continuous and highly conducting TiO_2 network are somewhat less important, due to extremely long electron diffusion lengths. Apart from reference [25] the material routes for thick mesoporous films are based on the commercially available Pluronic BCP system (PEO-*b*-PPO-*b*-PEO). As a consequence of its small molecular weight, pore sizes are below 10 nm, and the limited wall thickness does not facilitate complete crystallisation while preserving the mesostructure. Limitations in pore diameter, crystallinity and crystal sizes make this system less ideal for ss-DSCs.

In this chapter, the shrinkage process of BCP-derived inorganic films is studied as a func-

tion of time and temperature. The *in situ* investigation permitted the identification of a suitable processing window for a simple and fast treatment protocol that promotes the formation of thick mesoporous films with sufficiently large and continuous pores. The resulting TiO_2 coatings were employed as photoanodes in solid state-DSCs and compared to the state-of-the-art nanoparticle film architectures in terms of device efficiency and electronic properties.

7.2 Experimental

Material fabrication

BCP-derived TiO_2 photoelectrodes were fabricated as follows: 0.4 g poly(isoprene-*block*-ethylene oxide) BCP (PI-*b*-PEO) (M_n = 34.4 kg/mol, 28 wt% PEO) was dissolved in an 8 ml azeotrope solvent mixture of toluene (72.84 wt%, 99.8 % purity) and 1-butanol (27.16 wt%, 99 % purity). A titanium-containing sol was prepared separately by the addition of 1.54 ml titanium(IV) isopropoxide (99.999 %) to 0.49 ml hydrochloric acid (37 %) under vigorous stirring. 5 min after addition of the titania precursor, the sol was added to the polymer solution and subsequently stirred for a further 30 min. Hybrid films were then deposited from solution by spin coating (1800 rpm, 20 s) or doctor blading onto silicon wafers or fluorine doped tin oxide (FTO) coated glass sheets (15 Ohm/□, Pilkington) that were previously coated with a compact layer of TiO_2. Subsequently the films were exposed to a temperature annealing protocol on a calibrated programmable hotplate (2000 W, Harry Gestigkeit GmbH). The procedure of film deposition and subsequent annealing was repeated several times (typically three to seven cycles) to achieve the required film thickness. Finally the stacks were calcined at 600 °C (three hours, heat ramp 5 °C/min, Cole Parmer, EW-33855-35) to remove the organic material and to crystallise the TiO_2.

Material characterisation

For thermogravimetric analysis (TGA), samples were characterised with a commercial set-up (TA Instruments Q500) in high resolution dynamic mode (ramp ~ 2 °C/min unless otherwise stated). An Ocean Optics DHL2000 light source with a combined deuterium halogen lamp served for spectroscopic measurements. A fibre-optic reflection probe (Ocean Optics, R400-7-SR) was utilised for sample illumination and signal collection. The reflected signal was detected with an Ocean Optics QE 65000 spectrometer. Optical film thicknesses during annealing processes were acquired from the spectra by least square fitting using a home-built algorithm developed by Prof. J.J. Baumberg, which was implemented by the "Igor Pro" scientific analysis software. Ellipsometric data were taken on a Nanofilm EP3se imaging ellipsome-

ter and analysed with the instrument software. Fabrication and characterisation of solid state DSCs was carried out by Pablo Docampo (University of Oxford). The particular TGA analysis presented in Figure 7.2 was done by Dr. Dominik Eder, while characterisation was otherwise performed by the author. See reference [1] for ss-DSC device fabrication and characterisation as well as further experimental details.

7.3 Results and discussion

As previously discussed, the manufacture of thick porous films derived from a sol-gel/BCP composite is problematic because of the considerable shrinkage during the condensation reaction, polymer removal and TiO_2 crystallisation, typically leading to crack formation and delamination. The necessity of a stepwise release of stresses in a layer-by-layer approach becomes clear when investigating the loss in film thickness of an initially 700 nm thick layer as a function of temperature. Figure 7.1a shows the shrinkage of films derived from a weight ratio of 1:1 between the resulting TiO_2 after fabrication and the mixed polymer in the initial solution (TiO_2 1:1) when exposed overnight to temperatures between 50 °C and 600 °C. Shrinkage levels off at around 400 °C, after evaporation of residual solvent, condensation of the TiO_2 network and complete oxidation of the polymer have led to a decrease in film thickness by 60 %. Film shrinkage is significant for all inorganic to organic mixing ratios employed in the course of this study, with 55 % thickness contraction for TiO_2 3:1 and 65 % for TiO_2 1:2, as demonstrated in Figure 7.1b.
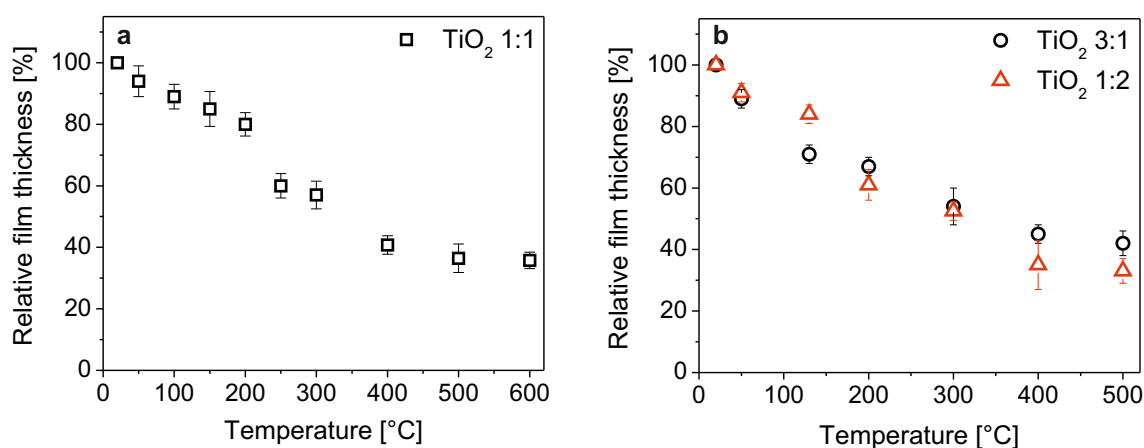

Figure 7.1: **Temperature dependent shrinkage in film thickness. a)** *Ex situ* development of the film thickness *h* as a function of annealing temperature, determined by ellipsometry and profilometry. The films were derived from an inorganic to organic weight ratio of 1:1 in solution (TiO_2 1:1) and annealed overnight at each temperature. **b)** Film thickness as a function of temperature for hybrid films for weight ratios of 3:1 (TiO_2 3:1) and 1:2 (TiO_2 1:2).

An important aspect of this work is revealed by thermogravimetric analysis (TGA), presented in Figure 7.2. Besides the hybrid samples, BCP and TiO_2 sol-gel material were also individually analysed by TGA. An expected development of the temperature dependent weight loss was subsequently calculated by linear combination of the inorganic and organic mass fraction in the hybrid materials. Compared to this anticipated development, samples with an inorganic mixing ratio of 3:1 (TiO_2 3:1) showed a retardation of the weight loss by 68 °C, whereas a mixing ratio of 1:2 (TiO_2 1:2) led to a delay of 75 °C. The greatly enhanced temperature resistivity of a hybrid sample compared to the purely inorganic and organic materials can most likely be attributed to the fact that the TiO_2 sol complexes with the PEO to form a hybrid matrix, which makes the organic component less susceptible to oxidation.

The resistance of the PI-*b*-PEO/TiO_2 hybrid system against high annealing temperatures is of central importance in this study. Earlier work has shown that a layer-by-layer approach can suppress crack formation due to the gradual release of stresses associated with the volume contraction. This is usually achieved by the calcination of the film after every layer deposition, which either leads to a densification of the film structure with subsequent coatings or requires an additional infiltration step to protect the pores [18, 19]. Both approaches may lead to a discontinuity of the porous network at the interfaces of each individual layer [26].

The aim of this study was therefore to anneal at temperatures that result in significant volume contraction but still allows pore protection by residual organic material. The appropriate annealing temperature is a trade-off between maximising stress release (by annealing at sufficiently high temperatures) and preserving most of the protective organic material (by
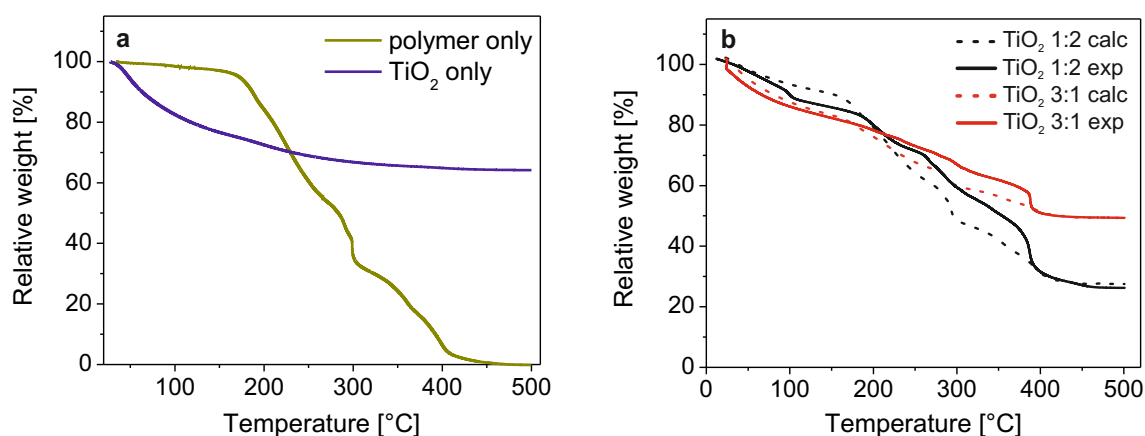

Figure 7.2: **Temperature dependent weight loss. a)** Weight loss of BCP (dark yellow) and TiO_2 sol (blue) during thermogravimetric analysis (TGA). **b)** Comparison of expected and measured weight loss by TGA. Dotted lines represent the weighed average derived from TGA results of purely organic and inorganic samples. Solid lines correspond to the measured results for inorganic to organic ratios of 1:2 (black) and 3:1 (red).

annealing at low enough temperatures). According to the data shown in Figures 7.1 and 7.2, a temperature of 300 °C is suitable to meet both requirements. Following the temperature-dependent weight loss of the pure TiO_2 sol it appears that the condensation of the hydrolysed $Ti(OH)_4$ to TiO_2 has completed at this temperature. Film shrinkage has already proceeded to 82 %, 70 % and 74 % of its overall loss in thickness for the different mixing ratios TiO_2 3:1, TiO_2 1:1 and TiO_2 1:2, respectively. Yet, according to the TGA results, a significant fraction of organic material is still present for finite annealing times at this temperature. The sacrificial material plays a crucial role for the formation of smooth and well-interconnected interfaces in a layer-by-layer stacking since the residual polymers protect the pores of the underlying film during the deposition of the subsequent layer. Furthermore, as the condensation of the inorganic network is more or less complete at 300 °C, partial dissolution of the underlying network is prevented when in contact with the solution during the cyclic film deposition process. Only in a final calcination and crystallisation step above 400 °C is the organic material fully removed to reveal the porous network. As will be shown in Chapter 8, subsequent layers in a multilayer stack are identical in their optical properties, i.e. of similar porosity and film thickness. This is convincing evidence that in contrast to earlier approaches, the pore size and pore shape stays constant throughout the layers [18, 27].

In order to resolve the kinetics of the shrinkage process, the annealing of the films was monitored *in situ* on a hotplate by collecting their reflection spectra. Figure 7.3 shows contour plots of time-resolved reflection spectra for annealing temperatures of 50 °C to 300 °C. The reflection intensity, normalised to that of a bare silicon wafer, is represented in a multi-colour scheme. The position of the interference fringes depends on the effective refractive index of the material n and the thickness of the film h (see Chapter 2). A shift of the reflectance maxima and minima to smaller wavelengths therefore corresponds to a reduction of the optical film thickness.

The optical film thickness $n \cdot h$ was subsequently obtained by least square fitting. The corresponding values at each temperature as a function of the annealing time are plotted in Figure 7.4a. Error bars include fitting uncertainties as well as the statistical standard deviation derived from three to five runs. For comparison, results were normalised to the initial film thickness of the samples at room temperature. Complementary *ex situ* measurements of the individual development of n with temperature are shown in Figure 7.4b. For this purpose, the samples were annealed overnight at the corresponding temperature and subsequently characterised by imaging ellipsometry. These results suggest that n is more or less unaffected by the annealing temperature with a maximum decrease of $\sim$ 6 % after annealing at 300 °C overnight. Hence, the development of the optically accessible parameter $n \cdot h$ is a good measure to reveal the development of the film thickness.
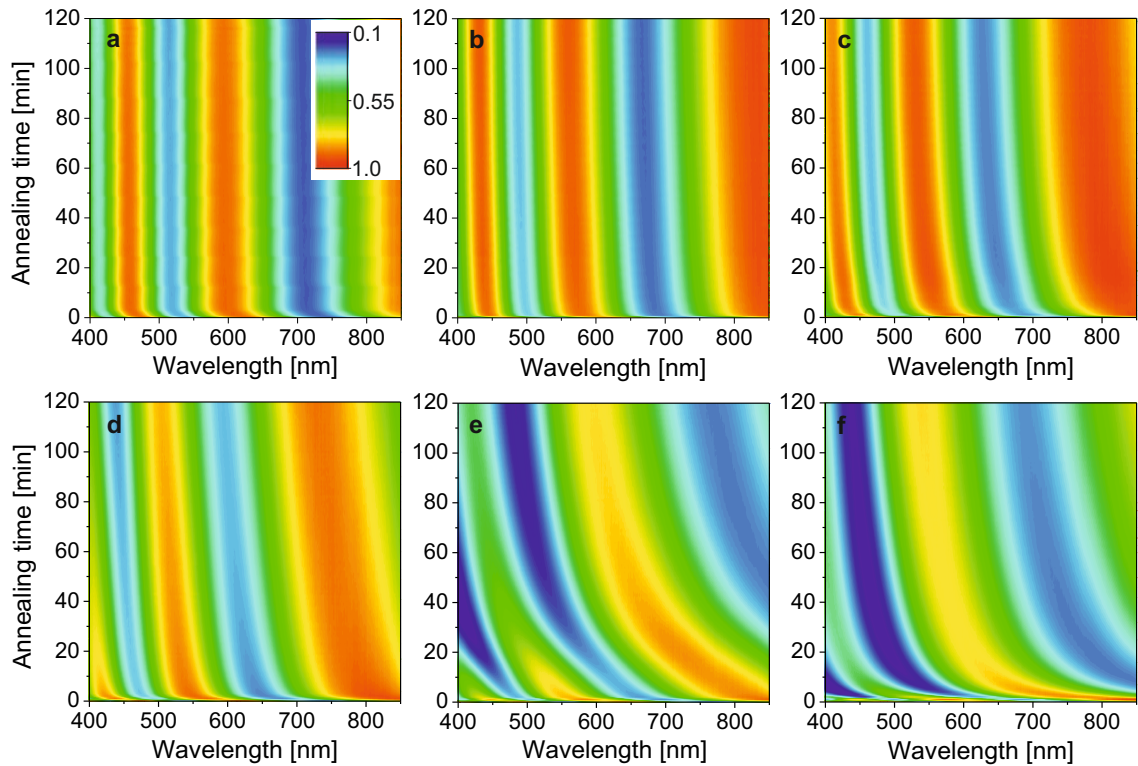
Figure 7.3: *In situ* **monitoring of film shrinkage at constant temperatures.** Reflectance spectra of ~ 700 nm thick hybrid films during annealing on a hotplate at **a)** 50 °C, **b)** 100 °C, **c)** 150 °C, **d)** 200 °C, **e)** 250 °C and **f)** 300 °C. The time-resolved reflection intensity is plotted in a multi color scheme shifting from blue to red for low to high intensities. The data is normalised to the reflectivity of a blank silicon wafer. A shrinkage in film thickness corresponds to a shift of the reflectance maxima and minima to smaller wavelengths.
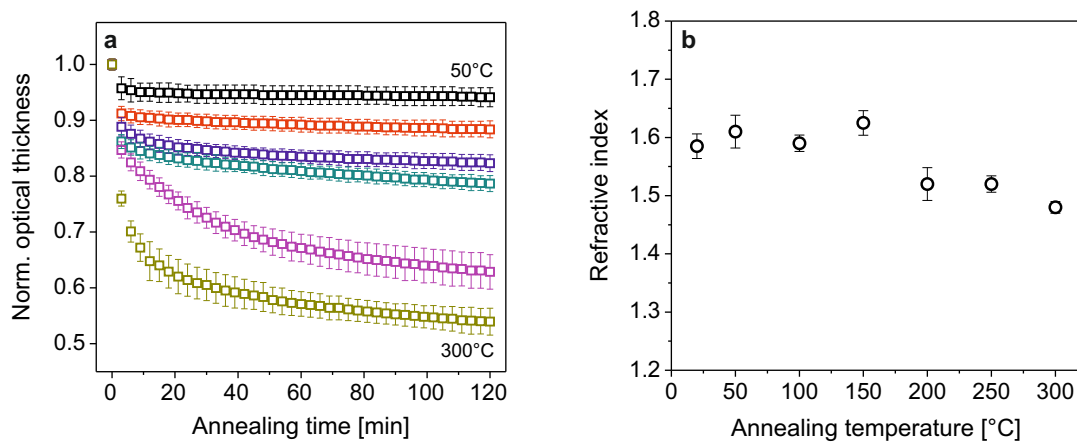

Figure 7.4: **Time-resolved development of optical film thickness at constant temperatures. a)** Development of the optical film thickness for different annealing temperatures (from top to bottom: 50 °C- 300 °C in 50 °C steps). Thickness values were derived from reflectance spectra by least square fitting. Error bars shown include fitting uncertainties as well as statistical standard deviation derived from three to five runs. **b)** Refractive index *n* as a function of annealing temperature determined by imaging ellipsometry. Samples were annealed overnight at each temperature.

Results from annealing at constant temperatures allowed the establishment of an annealing protocol, which enabled the gradual decrease of thickness with time and temperature, but limited the processing time to a minimum. This protocol consisted of an initial 10 min dwell time at 50 °C to evaporate the solvent and promote microphase separation, followed by a linear 45 min increase in temperature to 300 °C, where the films remained for 5 min before they were rapidly cooled down. The effect of such a 60 min annealing protocol on film thickness and weight is shown in Figure 7.5. In comparison to static annealing at a fixed temperature (Figure 7.4a), the temperature protocol has the beneficial effect of slowly and gradually reducing the film thickness by 37 %. The greatly enhanced film integrity is therefore a direct consequence of the annealing protocol. A complementary TGA measurement of the films subject to this temperature procedure is shown for comparison. After 60 min of annealing to 300 °C, the films retained 63 % of their initial weight. This compares to a weight of 33 % after removing the residual organic material and crystallising the TiO_2 network at 500 °C. A significant amount of organic material is therefore still present at 300 °C to protect the pores during successive layer deposition.

Figure 7.6 shows a schematic outline of the proposed layer-by-layer preparation route. A solution of PI-*b*-PEO BCP and TiO_2 sol in an azeotrope mixture of toluene and 1-butanol is co-deposited on a FTO-covered glass substrate by spin coating, doctor blading or dip-coating.
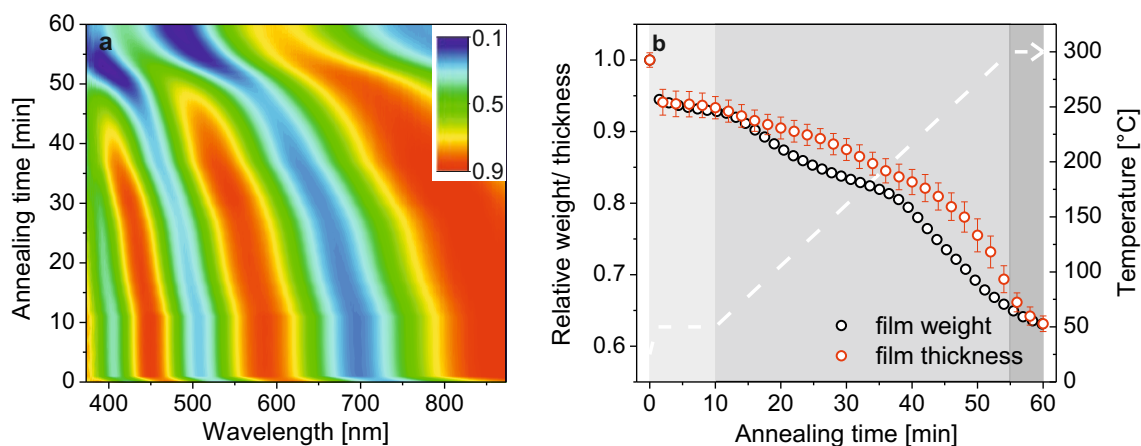

Figure 7.5: **Effect of annealing protocol on film shrinkage. a)** Optical response of a hybrid film subject to the proposed 60 min annealing protocol. The time-resolved reflection intensity, normalised to that of a bare silicon wafer, is represented in a multi-colour scheme. **b)** Corresponding development of the optical film thickness during the temperature treatment as derived by least square fitting of the reflectance spectra. In contrast to annealing at a fixed temperature, shrinkage occurs gradually, leading to a thickness reduction by 37 % (statistical average of five runs). For comparison the weight loss of the films was derived by TGA under the identical heating procedure. The temperature profile of the protocol is shown as a white dashed line.

Upon evaporation of the solvent, the hybrid material phase separates into nanometre-sized domains, where the TiO_2 sol resides in the hydrophilic PEO block to form a matrix that surrounds the pore forming hydrophobic PI block. The use of an azeotrope with a common high boiling point promotes a slow and simultaneous evaporation of hydrophobic and hydrophilic solution components. After coating from solution the film contains residual solvent, and the inorganic material has not yet fully condensed into a TiO_2 network. The hybrid film is then subjected to a temperature protocol of 10 min at 50 °C, followed by a 45 min linear heating ramp to 300 °C and a final dwell time of 5 min at this temperature. The 60 min annealing procedure typically leads to a thickness shrinkage of ∼ 40 %. Best results were achieved when the amount of dry film did not exceed ∼ 700 nm per layer deposition. A stack is produced by repeating the film deposition and annealing cycles to reach the desired final film thickness in typically three to seven steps. Finally, a high temperature step at 600 °C for 3 h removes the organic components and crystallises the TiO_2. See experimental section for further details.

This protocol enabled the gradual build-up of a thick film in a layer-by-layer fashion, releasing most of the stresses caused by volume reduction before deposition of the subsequent
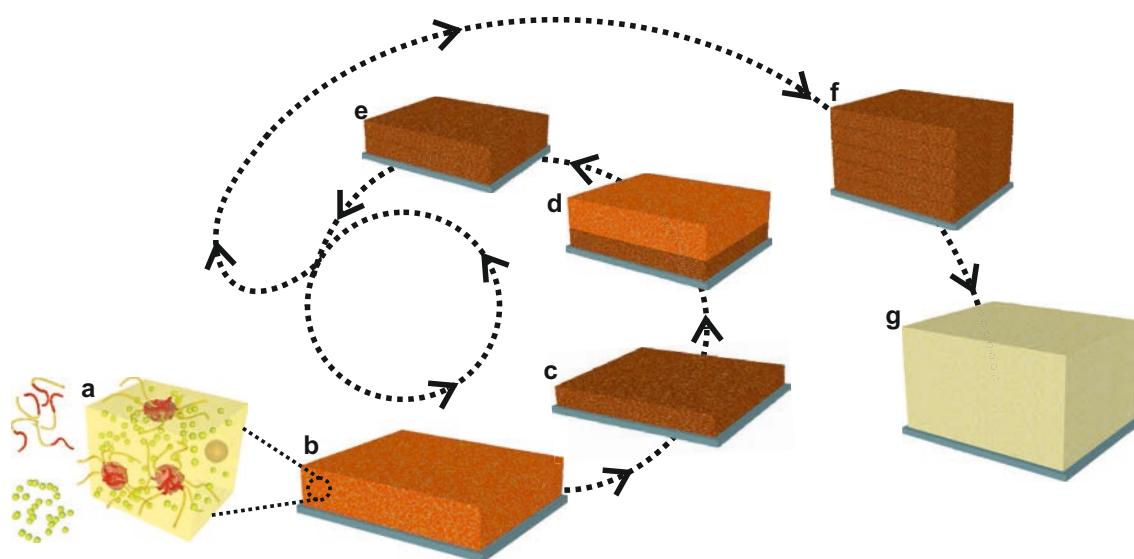

Figure 7.6: **Schematic of film fabrication. a)** A solution of PI-*b*-PEO BCP and TiO_2 sol is co-deposited on a FTO-covered glass substrate by spin coating, doctor blading or dip-coating. The inorganic component preferentially resides in the PEO phase and is therefore structure-directed during the self-assembly process of the amphiphilic BCP. **b)** After deposition from solution, the film contains residual solvent and the inorganic material has not yet fully condensed into a TiO_2 network. **c)** The hybrid film is then subjected to a 60 min temperature ramp to 300 °C, leading to a thickness shrinkage of ∼ 40 %. **d)** - **e)** Film deposition and heating are repeated several times to reach **f)** the desired overall film thickness. **g)** A final high temperature calcination at 600 °C removes the organic components and crystallises the TiO_2 film.

layer. The beneficial effect of this method is shown in Figure 7.7, where a 2.5 μm thick stack consisting of six layers is compared to a 2.5 μm thick film made in a single step. Figure 7.7a displays an optical transmission micrograph shortly after the deposition of a highly concentrated solution to form a 2.5 μm thick film. The evaporation of solvents caused the formation of cracks even before temperature annealing. After annealing, calcination and TiO_2 crystallisation at high temperatures, the film has broken up into isolated islands of mesoporous TiO_2, shown in the scanning electron micrograph in Figure 7.7b. As a consequence, a large area of the substrate (> 40 %) was left uncovered. In contrast, an equally thick film deposited in six cycles showed no cracks before and after annealing at 600 °C (Figure 7.7c-d).

The use of the PI-*b*-PEO BCP is particularly attractive because the combination of a high PI-PEO Flory-Huggins interaction parameter with low glass transition temperatures of both blocks and the large degree of polymerisation results in a much more robust and fast phase separation as compared to other BCP systems [28]. Instead of relying on time consuming protocols, the PI-*b*-PEO microphase morphology forms within minutes, allowing fast and reliable multilayer assembly.
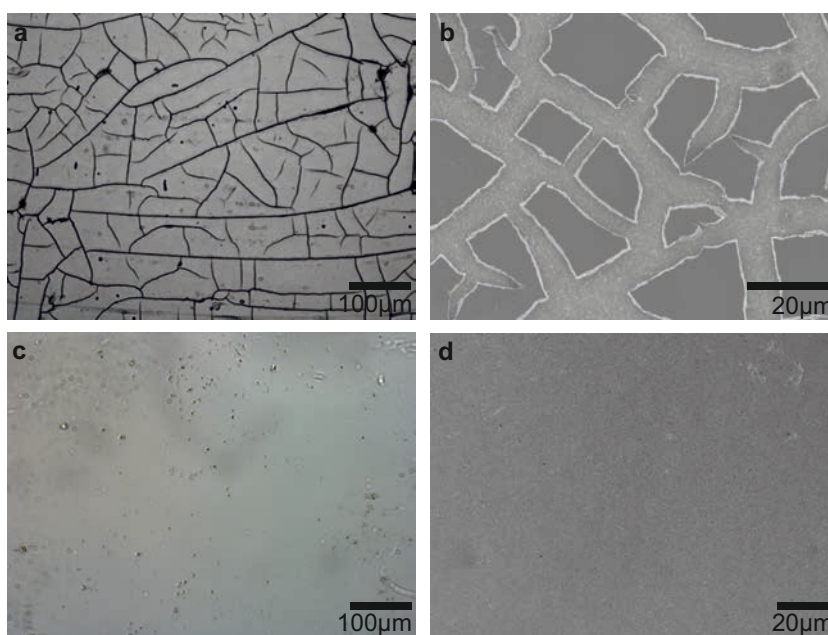
Figure 7.7: **Film quality and cracking behaviour. a) - b)** A 2.5 μm thick film was deposited in a single step. **a)** Transmission optical micrograph of the hybrid film. Evaporation of solvents led to the formation of cracks even at room temperature. **b)** SEM top-view image after high temperature treatment. Initial cracks expanded during calcination and TiO_2 crystallisation, leaving a large substrate area uncovered (> 40 %). **c) - d)** Formation of a similarly thick film in 6 cycles. **c)** Optical micrograph of the hybrid film before and **d)** SEM image of the 2.5 μm thick film after calcination and TiO_2 crystallisation.

The morphology of a TiO_2 photoanode fabricated by four deposition and annealing cycles and a final high temperature step is shown in Figure 7.8. Pores are well discernible on the surface of the 1.3 μm thick stack, indicating that the pore network is fully accessible from the top. No solid TiO_2 overlayer has formed that could impede the infiltration of the network. Figure 7.8b shows the cross-section of a fully assembled ss-DSC, after dye sensitisation and infiltration of the network with the hole conductor spiro-OMeTAD.

Thick porous multilayer photoanodes assembled into ss-DSCs exhibited remarkable photovoltaic performance. Figure 7.9a presents the current-voltage characteristics of the best performing device, with a short circuit current (J_{sc}) of 8.0 mA/cm^2, an open-circuit potential (V_{oc}) of 0.81 V and a fill factor (FF) of 0.63, resulting in a power conversion efficiency (η) of 4.0 % using the organic dye CN04 [13]. This is a significant improvement over previously reported efficiencies of BCP-assembled ss-DSCs, where $\eta_{max} = 2.5$ % [15] and $\eta_{max} = 1.5$ % [29]. In both cases, the attainable film thicknesses were limited by cracking and delamination, resulting in insufficient light absorption of the manufactured devices. Devices were also assembled with the indolene based organic dye D102 which is often used to create reliable ss-DSCs. Figure 7.9b shows the best working devices employing this dye. Devices based on BCP-assembled and conventional NP photoanodes reach similar power conversion efficiencies of ~ 3.6 %. While the NP system has a higher value of J_{sc}, the BCP multilayer devices excel in open-circuit voltage and fill factor. Figure 7.9c-d shows an overview of the key photovoltaic device parameters J_{sc}, η, V_{oc} and FF as a function of the film thickness of the BCP-assembled photoanode (data from 12 devices were averaged for each thickness). A reasonably constant performance was observed for photoanode thicknesses between 1.3 and 2.0 μm. Devices with
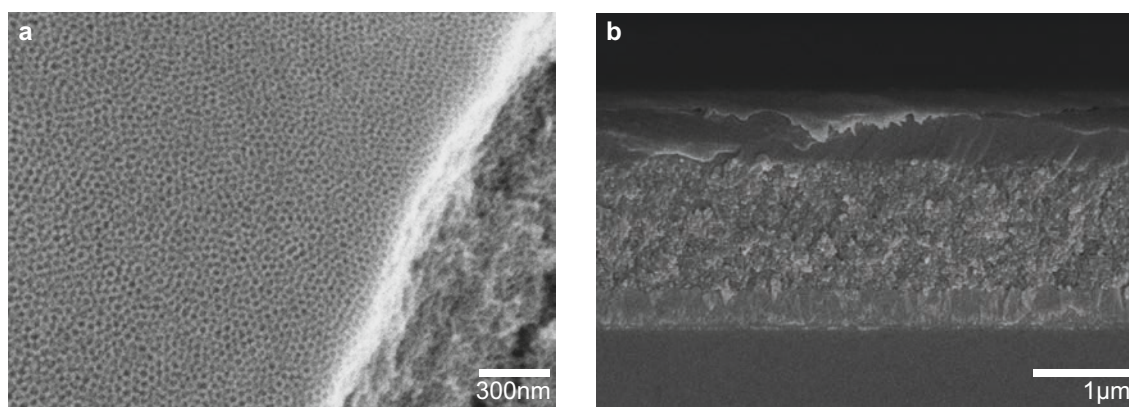
Figure 7.8: **Electron micrographs of the photoelectrode morphology. a)** SEM top-view of a 1.3 μm thick mesoporous TiO_2 film, assembled in four deposition and annealing cycles. The pores arising from BCP assembly are fully accessible and no overlayer has formed. **b)** Cross-sectional SEM image of a fully assembled ss-DSC, where the network has been infiltrated with the hole conducting organic material Spiro-OMeTAD.

photoanode thickness of 2.5 μm resulted in a significantly lower J_{sc}, whereas $V_{oc} \sim 0.87$ V and $FF \sim 0.7$ were retained for this thickness.

BCP-assembled photoanodes have been previously reported to exhibit faster electron transport compared to random NP networks [15]. Figure 7.10 shows a comparison between multilayer BCP-derived photoanodes and devices incorporating standard NP films of the same thickness in terms of charge recombination, transport and collection rates as a function of the applied bias. It is evident that charge transport in a five-layer BCP device is notably faster, indicating excellent electronic connectivity between the segments. For the direct comparison of ~ 1.7 μm thick films, BCP- and NP-derived devices exhibited transport rates of $4500\,\text{s}^{-1}$ and $2250\,\text{s}^{-1}$, respectively, when operated at the maximum power point.

The high transport rates k_{trans} can be attributed to the fact that the presented route allows the formation of exceptionally large TiO_2 nanocrystals within the mesoporous network while
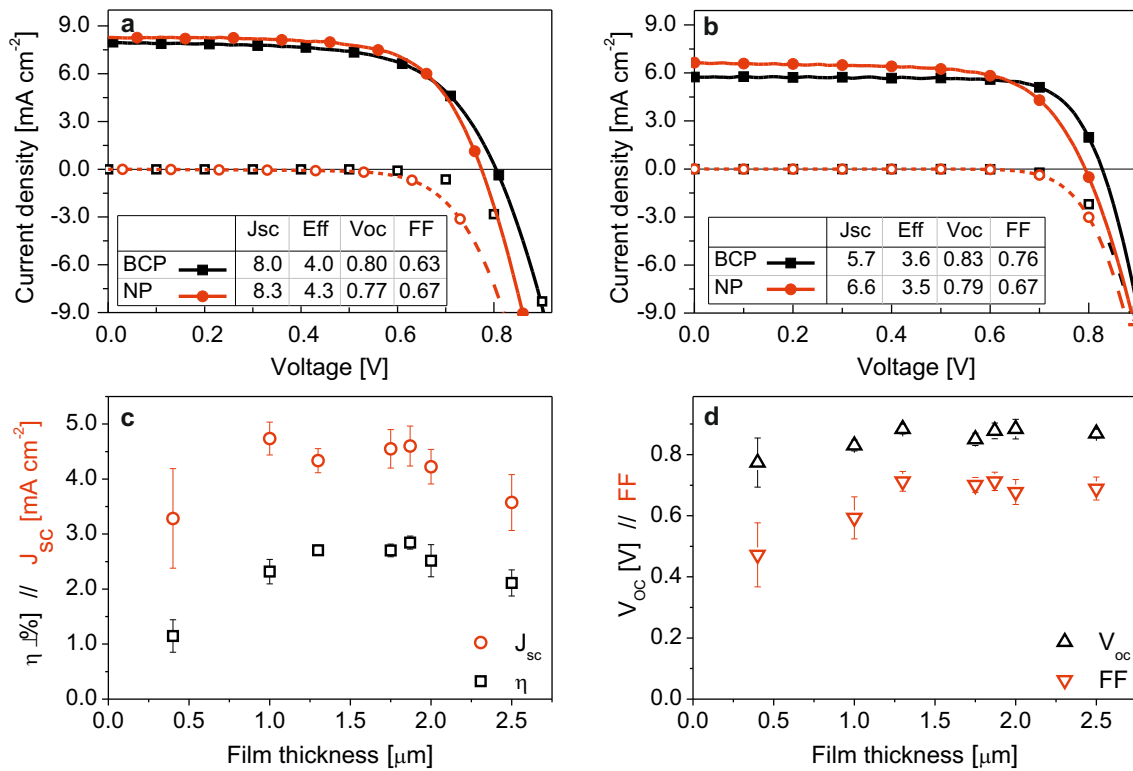
Figure 7.9: **Photovoltaic device performance. a)** Current-voltage characteristics of the highest efficiency ss-DSCs based on a 1.3 μm thick BCP-derived photoanode compared to a NP assembly. The dye CN04 was used in both devices [13]. The filled symbols correspond to a simulated AM 1.5 full sun light illumination (100 mW/cm^2), the open symbols represent the dark current. **b)** Current-voltage curves of similar devices using the dye D102. **c) - d)** Key photovoltaic device parameters as a function of the thickness of the active layer. **c)** Short circuit current (J_{sc}) and power conversion efficiency (η) of BCP-assembled devices. **d)** Open-circuit voltage (V_{oc}) and fill factor (FF).
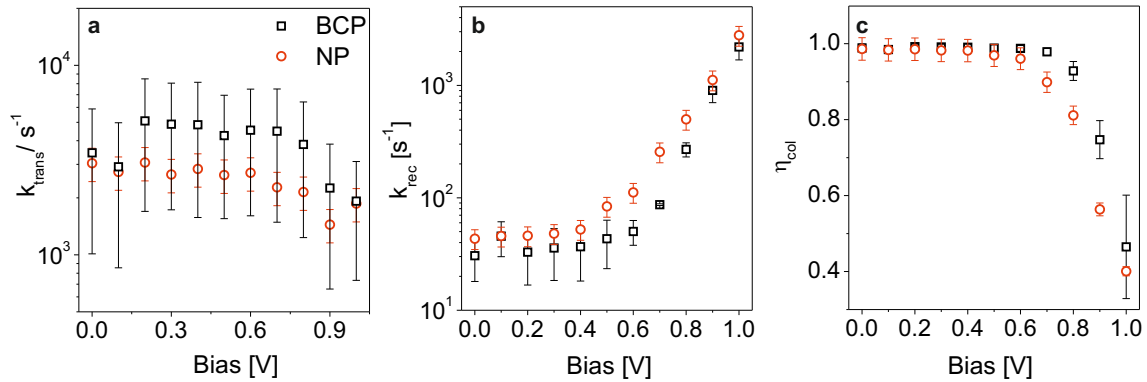
Figure 7.10: **Electronic device characteristics.** Direct comparison between BCP-assembled photoanodes and conventional NP devices of similar thickness (1.8 μm). **a)** Transport rates (k_{trans}), **b)** recombination rates (k_{rec}) and **c)** charge carrier collection efficiencies (η_{col}) as a function of the applied bias. While the collection efficiency for standard NP devices deteriorates above 0.5 V, BCP-derived devices retain high efficiencies close to V_{oc}.

maintaining the BCP imposed morphology [15] (see Chapter 6). Charge recombination rates were significantly reduced in the BCP system with $85 \, s^{-1}$, compared to $255 \, s^{-1}$ for the corresponding NP devices at the maximum power point. These highly conducting networks exhibit a somewhat reduced surface area compared to the standard NP-based photoelectrodes [15]. As the recombination rate k_{rec} is usually linked to the surface-to-volume ratio of the structure, it is expected to see enhanced transport rates and lower recombination [30, 31]. The bias-dependent charge collection is therefore remarkably different in both systems. For the NP devices, charge collection efficiency (η_{col}) decreased above 0.5 V, while charge collection in BCP devices remained close to unity up to 0.7 V. At $V_{oc} = 0.9 \, V$, the charge collection efficiency for the BCP-derived devices $\eta_{col} = 0.86$ compared to $\eta_{col} = 0.56$ for the NP system. This is consistent with the exceptionally high fill factor of 0.76 obtained with some of these devices. These results are particularly important since they promise more efficient operation at higher bias, i.e. an enhanced fill factor. In fact, large fill factors (> 0.7) were observed with the dye D102 for film thicknesses up to 2.5 μm. Furthermore, the open-circuit potential of the BCP-derived devices was above 0.85 V for films thicker than 1.0 μm, which can be explained by the improved transport properties and the narrower distribution of sub-band-gap states [32].

7.4 Conclusions

In summary, a straight-forward route is demonstrated for the fabrication of thick mesoporous films with a well defined pore morphology. A study of the time- and temperature-dependent evolution of the shrinkage process of ~ 700 nm thick spin-cast layers enabled the identification

of the optimal processing parameters for layer-by-layer film formation of thick films, avoiding the formation of cracks and delamination by the gradual release of in-plane stresses. Following a fast, simple and effective annealing protocol, film shrinkage is maximised for each deposition cycle, while preserving the polymer to protect the underlying pores. As a consequence, the time and effort to build-up a multilayer stack is drastically reduced. The resulting mesoporous TiO_2 photoanodes exhibit a continuous network with large accessible pores. Increased pore size, film thickness and temperature-stability led to greatly enhanced power conversion efficiencies in solid state dye-sensitised solar cells, which are now comparable to the long-optimised NP system. Significantly enhanced charge transport and charge collection rates at high bias make this system a promising candidate to increase the fill factor and open-circuit potential of thick film ss-DSCs.

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Chapter 8

Tunable mesoporous Bragg reflectors based on block copolymer self-assembly

8.1   Introduction

A distributed Bragg reflector (DBR) is defined as a one-dimensional (1D) periodic dielectric lattice of alternating high and low refractive index materials. Reflection of light at each of the layer interfaces leads to multiple interference and thus, a characteristic reflection and transmission behaviour. The underlying theoretical aspects of DBRs are discussed in Chapter 2, including the position of the fundamental Bragg peak λ_{max} (equation 2.32), the width of the reflectance peak $\Delta\lambda_{max}$ (equation 2.35) and the expected reflectance $\mathcal{R}$ (equation 2.31). Thus, the structural colour response of a multilayer stack can be finely tuned by varying the refractive index, the thickness and the number of alternating layers [3]. DBRs are of technological interest because of their spectrally selective wave guiding properties. Well-established applications include Fabry-Pérot interferometers, optical resonators for distributed feedback lasers and optical cavities for controlling the spontaneous emission rates and spectra from emitting media [4, 5]. Simple configurations are typically realised by sequential coating of thin solid films of alternating refractive index. Polymer-based DBRs allow mechanical tunability throughout the visible spectrum [6]. Direct access to a 1D dielectric lattice via solution processing has been achieved by the self-assembly of block copolymers (BCPs) with sufficient dielectric contrast into a lamellar morphology [7, 8].

An interesting recent area of research is the development of mesoporous DBRs (MDBRs), which access new fields of applications due to their porosity on the sub-optical length scale. Their ability to detect changes in the ambient environment makes them ideally suited as sensing materials. Adsorption and desorption of gas phase molecules in the pores leads to reversible changes in the refractive index of the building blocks and thereby in the photonic properties of the stack [9, 10, 11, 12]. MDBRs have been successfully used as biosensors when functionalised to bind specific molecules [13]. This can be extended to an array of MDBRs with different chemical or biochemical functionalisations to allow detection and discrimination of different vapour species such as small molecules and bacteria [14]. The coupling of MDBRs to surface layers [15] and resonance cavities [16] is particularly attractive as it allows sensing with greater accuracy. As outlined in Chapter 3, MDBRs also have great potential in optoelectronic devices. The localisation of light of a specific part of the spectrum leads to efficiency enhancements in dye-sensitised solar cells due to the increase in absorption probability [17]. When infiltrated with light emitting polymers, MDBRs can exhibit distributed feedback lasing [18]. Recently, the coupling of plasmonic particles to MDBR-based resonant cavities has been shown [19].

The material routes towards MDBRs are numerous. Initially, 1D refractive index lattices were realised in porous silicon by periodically changing the etching conditions to achieve high and low porosity layers in an alternating order [20]. In the mid 2000s, Ozin and coworkers introduced the concept of solution-processed MDBRs by the alternate spin coating of Pluronic BCP-assembled mesoporous TiO_2 and SiO_2 layers [9]. While the morphology within the network showed good structural order, processing was extremely time consuming with fabrication times up to several days for each individual layer of the stack [21]. A less complex route to form porous TiO_2 and SiO_2 networks is the random packing of nanoparticles (NPs). This was introduced by Cohen *et al.* [22] and further simplified by Míguez and coworkers. [23]. The optical properties of NP-based MDBRs can be tuned by changing the layer thickness and the materials of the building blocks, but variation of porosity is difficult. The random-close packing of the NPs allows only limited control over the pore fraction and dimensions by changing the NP size and by adding sacrificial material [24, 25]. The necessary refractive index contrast is therefore typically achieved by stacking TiO_2 and SiO_2 layers of similar porosity, which leads to electrically insulating MDBRs and therefore limits their application in optoelectronic devices. Furthermore, a random network of sintered NPs lacks detailed control over pore diameters and pore size distribution, limiting functionality for sensing applications and infiltration by other functional materials [26, 27]. A vacuum-based method that offers fine control over the refractive index is glancing angle deposition (GLAD) that involves physical vapour deposition at an oblique angle α [28]. The ballistic shadowing which arises from tilting the

substrate with respect to the vapour flux enables to vary the packing density of the nucleated columnar structures [29]. The dynamic variation of α thus allows to fine-tune the refractive index with high precision to form a MDBR [30].

Herein, an alternative concept for the fabrication of MDBRs is presented that relies on the self-assembly of the BCP PI-*b*-PEO in combination with simple hydrolytic sol-gel chemistry. This system enables extended control of porosity and pore size in the resulting inorganic layers by the interplay between the self-assembly of the sacrificial BCP host PI-*b*-PEO and the co-assembled TiO$_2$. Processing conditions are identified that allow for the formation of a multilayer stack with periodic high and low refractive index layers. The effects of this approach on the optical quality and pore accessibility of the resulting MDBRs are theoretically and experimentally characterised.

8.2   Experimental

Two stock solutions with differing ratios of TiO$_2$ sol to PI-*b*-PEO BCP were prepared as follows. First, a titanium containing sol was obtained by the rapid addition of 0.69 ml HCl (37 %) to 1 ml titanium ethoxide (purum) under vigorous stirring. In parallel, two polymer solutions were prepared by dissolving 0.1 g of PI-*b*-PEO (molecular weight $M_n = 34.4$ kg/mol, 28 wt% PEO) in 7 ml tetrahydrofuran (THF). After stirring for 90 min, the sol was added to the polymer solution. A weight ratio of 3:1 (TiO$_2$ 3:1) and 1:2 (TiO$_2$ 1:2) between the resulting TiO$_2$ and the initially used polymer were chosen for the high and low refractive index layers, respectively.

For TiO$_2$ 3:1, 1.31 ml sol was added, followed by the evaporation of volatile components at 50 °C in a Petri dish. Once dry, the hybrid material was quickly redissolved in a in a solvent mixture of 49 vol% toluene and 51 vol% 1-butanol. The solution containing TiO$_2$ 1:2 was prepared similarly, but in this case 0.22 ml sol was added to the polymer base solution and the solvent mixture for redissolving the dried hybrid material consisted of an azeotrope mixture of 72.84 wt% toluene and 27.16 wt% 1-butanol. Subsequently the concentrations of the hybrid solutions were adjusted to match the film thickness requirements. Films were then deposited by spin coating (2000 rpm, 20 s) onto previously cleaned microscope slides. Subsequent to each film layer deposition, an annealing cycle of 10 min at 100 °C, 200 °C and 300 °C was applied. Layers from TiO$_2$ 3:1 and TiO$_2$ 1:2 were deposited in alternating fashion to build-up the MDBR stack. Finally the MDBR was calcined at 500 °C (three hours, heat ramp 5 °C/min) to remove the organic material and crystallise the TiO$_2$.

8.3   Results and discussion

The BCP PI-*b*-PEO plays a key role in the presented fabrication route as it co-assembles the inorganic material into ordered spatial domains during the phase separation process. The sol acts as a guest that selectively complexes with the PEO phase of the sacrificial BCP host. This provides fine control over the refractive index of the resulting inorganic material through the mixing ratio of the components in the initial solution. In this study, two stock solutions were prepared with mixing ratios of 3:1 (TiO$_2$ 3:1) and 1:2 (TiO$_2$ 1:2) between the TiO$_2$ and the BCP, which then served as a fabrication base for the solution processing of the hybrid films.

A major challenge for the fabrication of BCP-derived mesoporous films is the considerable shrinkage that occurs during the several processing steps. The aim of the presented approach was to establish a processing protocol that could accommodate the shrinkage step-by-step, while minimising the necessary fabrication time. To optimise MDBR fabrication, the film shrinkage process was therefore monitored *in situ*. TiO$_2$ 3:1 and TiO$_2$ 1:2 were spin-coated onto silicon wafers, and the reflection spectra of individual layers were collected during annealing on a hot plate. Additionally, thermogravimetric analysis and *ex situ* thickness tracking were employed to understand temperature and time dependence of the shrinkage process (see Chapter 6). Based on these results a 30 min annealing protocol was established, consisting of three consecutive 10 min steps at 100 °C, 200 °C and 300 °C. Figure 8.1a and b shows reflection spectra of TiO$_2$ 3:1 and TiO$_2$ 1:2 hybrid films during the annealing protocol taken in one-minute intervals. The reduction in film thickness shifts the reflectance maxima and minima to smaller wavelengths. For clarity, the spectral position of the maximum reflectance is plotted in Figure 8.1c and d as a function of time for both mixing ratios. TiO$_2$ 3:1 shrinkage (Figure 8.1b and d) was significantly faster than for the lower inorganic loading of TiO$_2$ 1:2 (Figure 8.1a and c). In both cases, the results indicate that the shrinkage process was completed within the 10 min interval at each temperature. In this material system a substantial fraction of organic matter is still present in the film after annealing at 300 °C (see Chapter 7). The sacrificial material plays a crucial role in the stack build-up. The pores of underlying films are thereby protected and cannot clog up during sequential spin-coating, which should lead to highly interconnected inorganic networks after a final calcination step. Cyclic annealing after each layer deposition has another beneficial effect: the condensation of the inorganic network prevents the partial dissolution of the film's surface when contacted by the solution for the next layer. This is essential for the formation of well defined interfaces, a requirement for high optical quality of the MDBRs.

A comparison between the underlying concept and the experimental realisation is shown in Figure 8.2. The dissimilar weight ratios of organic and inorganic material in the two stock
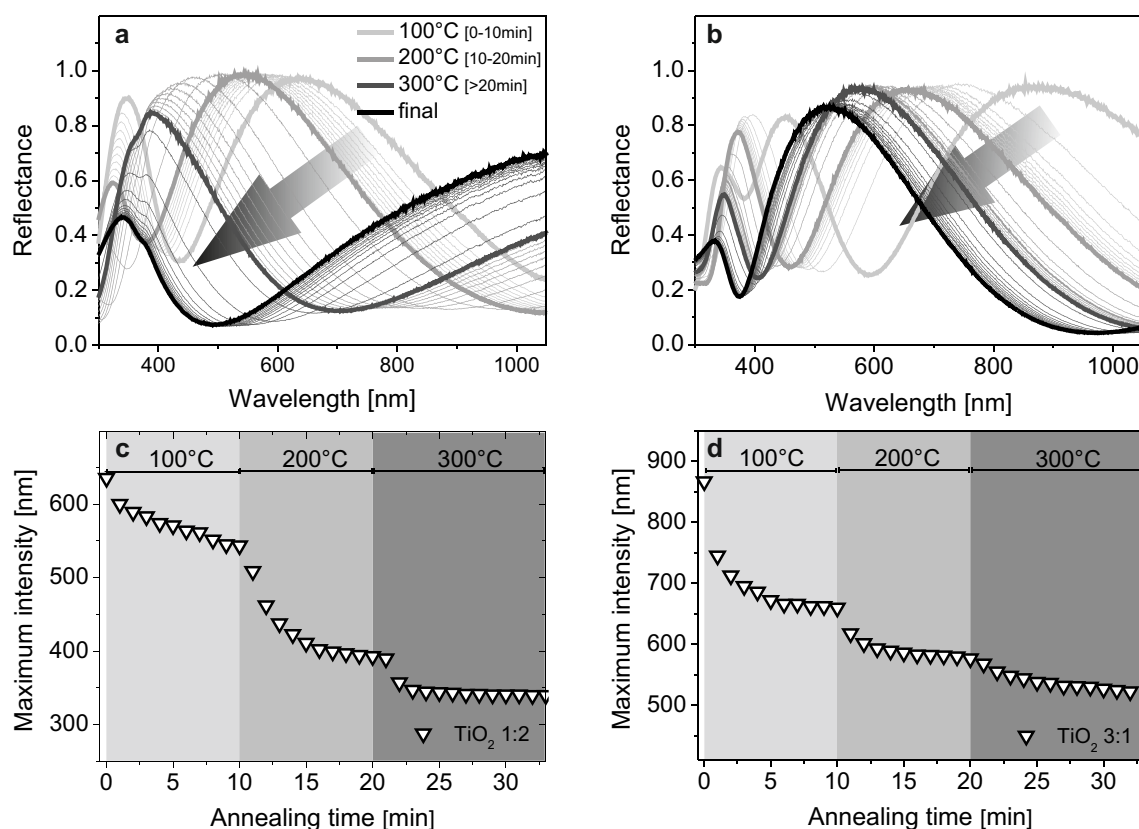
Figure 8.1: **Temperature-dependent shrinkage of hybrid films. a)** *In situ* reflectance of a hybrid TiO$_2$ 3:1 film during consecutive annealing at 100 °C (light grey), 200 °C (grey) and 300 °C (dark grey) for 10 min each. The reflection intensity of the films was normalised by the reflectivity of a bare silicon wafer. **b)** *In situ* reflectance of a hybrid TiO$_2$ 1:2 film exposed to the identical temperature protocol. **c)** - **d)** Corresponding plots of maximum reflectance intensity for TiO$_2$ 3:1 and TiO$_2$ 1:2, respectively.

solutions results in a different materials arrangement upon phase separation. A higher TiO$_2$ content leads to a denser structure, where less sacrificial pore forming material is incorporated. Increasing the polymer content results in a mainly organic film that yields a more porous network of lower refractive index. A periodic modulation of high and low refractive index in the stack is therefore achieved by spin coating hybrid layers from TiO$_2$ 3:1 and TiO$_2$ 1:2 solutions in alternating fashion, followed by a 30 min annealing after every film deposition.

Figure 8.2d-f shows the experimental realisation of the MDBR stack structure after calcination at 500 °C to remove the structure-directing BCP, reveal the pores and crystallise the TiO$_2$ network. Cross-sectional slices were prepared by focussed ion-beam milling to visualise the entire MDBR stack structure. The two different MDBR layers are clearly discernible in the transmission electron microscopy (TEM) image of Figure 8.2d. The darker layers correspond to a high electron density and therefore a high TiO$_2$ content (TiO$_2$ 3:1), with the brighter layers stemming from TiO$_2$ 1:2. The films were sputter-coated with platinum for the ion milling

process. As a consequence, the top layer in this image was partially infiltrated by the metal that is perceptible as black penetration of the top layer.

Top-view scanning electron microscopy (SEM) images of TiO_2 3:1 and TiO_2 1:2 films are presented in Figure 8.2e and f. In contrast to earlier work [31], no solid TiO_2 overlayer was observed in any of the thin films. These results imply that in the given wt% range, the organic structure-directing agent is able to incorporate the full amount of inorganic material into the PEO block, allowing reliable phase separation and refractive index tuning without segregation of inorganic material. The difference in porosity for films stemming from high and low TiO_2 loading is clearly visible. TiO_2 1:2 exhibits a very open pore structure with thin walls that are surrounded by a large volume fraction of pores. In contrast, TiO_2 3:1 features a more dense structure with similar pore sizes but a much lower pore density. The morphological dissimilarity results in a significant difference in the effective refractive index of the building blocks, with $n_{1:2} \sim 1.41$ and $n_{3:1} \sim 1.69$ as determined by imaging ellipsometry at $\lambda = 632\,nm$. Extending the mixing ratio to higher TiO_2 loadings, the refractive index could be tuned to any value between 1.4 and 1.9. This range is well above previously reported solution-based approaches to tune the refractive index by porosity for MDBR manufacture [21, 24, 25].
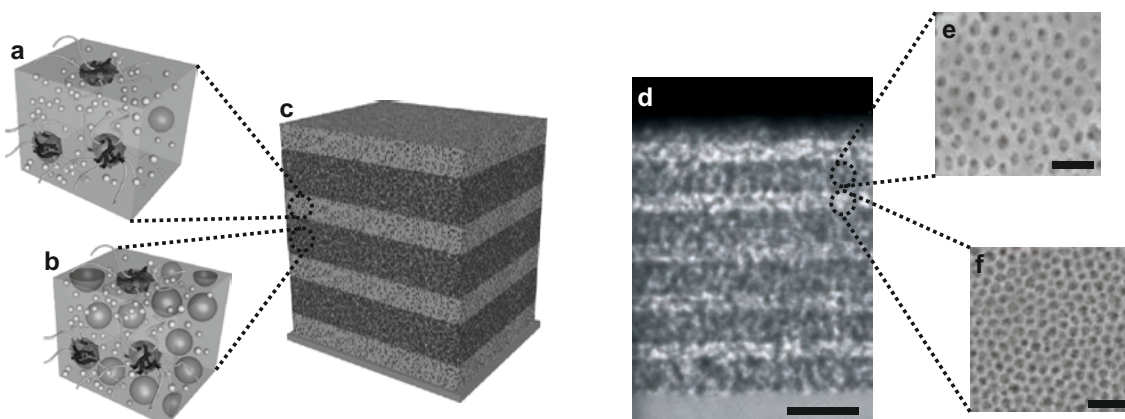
Figure 8.2: **Schematic vs. electron micrographs of MDBR structure.** **a)** - **c)** Schematic of MDBR building blocks. The two stock solutions differ in the TiO_2 to polymer weight ratio (3:1 vs. 1:2). The dissimilar ratio of organic and inorganic material is reflected in the micro-phase separation of the co-assembled material after spin coating. **a)** A higher TiO_2 content results in a denser structure with less sacrificial pore forming material. **b)** Increasing the organic content leads to a more porous network of lower refractive index. **b)** MDBR stacks are built-up by spin-coating from alternating solutions, followed each time by an annealing step. **d)** - **f)** Electron microscopy of the building blocks after calcination at $500\,°C$. **d)** TEM cross-sectional view of a MDBR stack. The darker layers reflect the high TiO_2 content of TiO_2 3:1, whereas the brighter layers correspond to TiO_2 1:2. **e)** SEM top view of a TiO_2 3:1 film with a refractive index of $n_{3:1} \sim 1.69$. **e)** SEM top view of a highly porous film TiO_2 1:2 film with $n_{1:2} \sim 1.41$. Scale bars represent $200\,nm$.

Figure 8.3: **Optical properties of MDBRs. a) - d)** Photographic images of exemplary MDBRs consisting of five layers TiO_2 3:1 and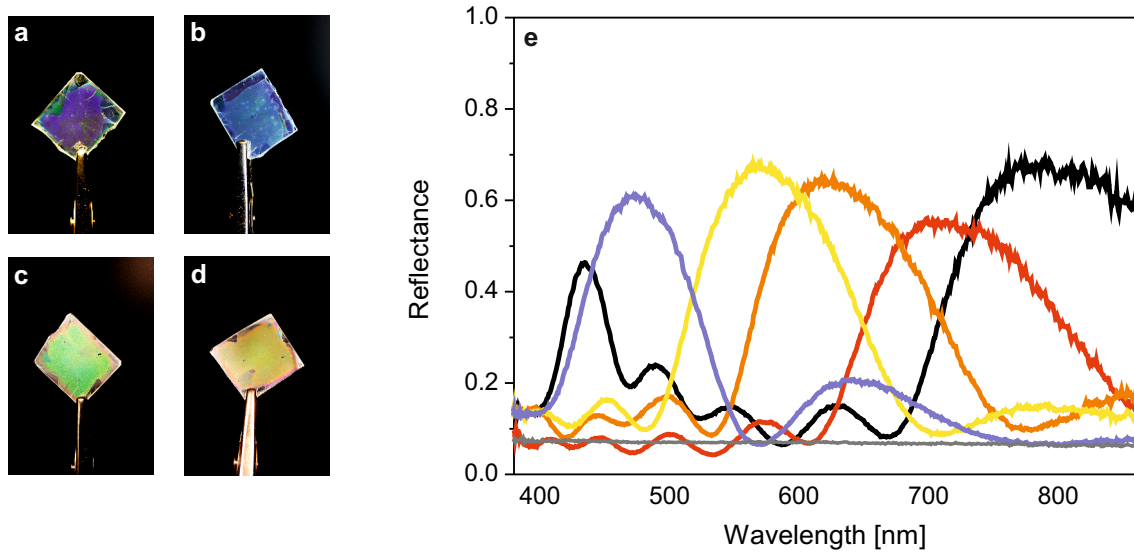 four layers TiO_2 1:2. The parameters of the TiO_2 3:1 layers were kept constant while the TiO_2 1:2 layers were varied in thickness to give rise to characteristic reflection colours of **a)** violet, **b)** blue, **c)** green and **d)** yellow. **e)** Reflectance of MDBRs, where the five layers TiO_2 3:1 were kept constant, while the four layers TiO_2 1:2 were varied in thickness between 78 nm and 292 nm to tune the characteristic reflectance across the visible spectrum.

The MDBRs have a well-defined band gap that gives rise to a characteristic colour appearance. This is visible in photographic images of MDBRs shown in Figure 8.3a-d. When altering the thickness of the low refractive index component, the reflected MDBR colour shifts from purple to blue to green to yellow. These images illustrate that the presented method is able to uniformly stack nine layers and maintain a highly uniform optical response. The experimental reflection spectra in Figure 8.3e are in line with the photographs. Here, the reflectance of a nine-layer MDBR was tuned from $\sim$ 475 nm to $\sim$ 800 nm, i.e. across the visible spectrum by varying the concentration of the TiO_2 1:2 solution. While the five TiO_2 3:1 layers were kept constant at 75 nm, the thickness of the TiO_2 1:2 layers was varied between 78 nm and 202 nm by adjusting the solution concentration.

In order to evaluate the regularity of the multilayer stack, the experimental results were compared to theoretical calculations of a perfectly ordered dielectric lattice. For this purpose, film parameters of the individual layers were determined by imaging ellipsometry, yielding $n_{3:1} \sim 1.70 \pm 0.02$, $h_{3:1} \sim 76 \pm 2$ nm, $n_{1:2} \sim 1.40 \pm 0.02$ and $h_{1:2} \sim 132 \pm 2$ nm ($\lambda = 632$ nm). Based on these parameters modelling was carried out for a different number of layers by using a home-built Matlab algorithm that follows Rouard's technique [3, 32] (see Chapter 2.3). The modelled optical response of an ideal lattice is compared to experimental reflectance results in Figure 8.4b, c and d for five, nine and thirteen layers, respectively. Experimental and theoret-

ical data bear close resemblance, demonstrating the high optical quality of the samples. This can be attributed to the well defined optical interfaces, the highly reproducible thickness and the refractive index of the layers that are facilitated by the herein presented fabrication route.

Pore interconnectivity is an important property for many technological applications of MD-BRs. To confirm the accessibility of the porous network throughout the entire stack, the MDBR was infiltrated by different liquids with refractive indices ranging from 1.33 to 1.55. Figure 8.5a shows the reflection spectra of a nine-layer MDBR in air and after infiltration of the network with H_2O, 2-propanol, chloroform and 1,2-dichlorobenzene. The shift of the Bragg peak to longer wavelengths is the result of a change in the effective refractive index contrast of the layers, as the air in the pores is replaced by the higher refractive index liquids. The dip in maximum reflectance arises from the change of the optical medium at the MDBR's surface (see equation 2.31). The uniform shift of the characteristic Bragg peak suggests a homogeneous infiltration of the optical components from top to bottom. Shown in Figure 8.5b, these results are in good agreement with the modelled shift of the peak position following the symmetric Bruggeman effective medium approximation (see Chapter 2.5). An accessible pore volume of 28 % and 56 % was assumed for TiO_2 3:1 and TiO_2 1:2, respectively.

The herein presented materials route offers several advantages over the state-of-the-art. In contrast to NP-based approaches, the porosity can be finely tuned over a wide parameter space. The pore size of the network is relatively uniform and can be controlled, as it is determined by the molecular weight of the polymer's PI block. It has already been shown that the average pore diameter can be varied in a range from 15 nm to 55 nm by using different BCPs [33] (see Chapter 5). This is in contrast to NP networks, where the pore formation is based on the random dense packing of NPs. As a consequence, these random networks suffer from
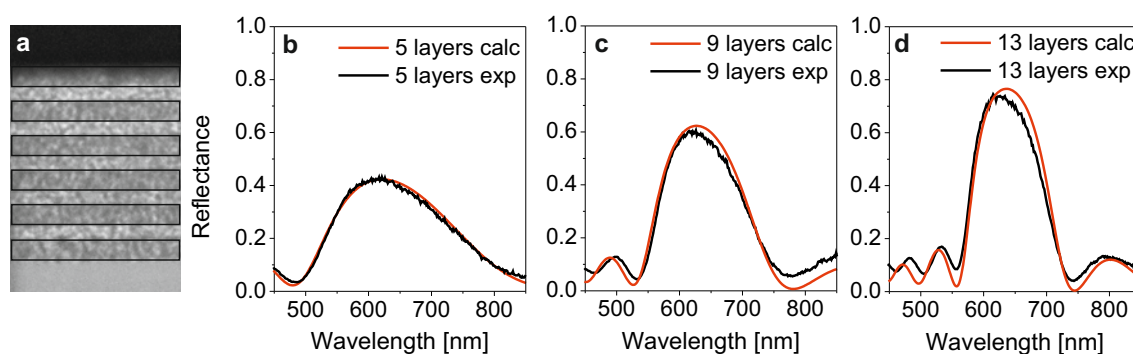
Figure 8.4: **Experiment vs. modelling of a perfectly regular stack. a)** Segmentation of cross-sectional TEM image into layer units. **b) - d)** Comparison of experimental reflectance with calculations of an perfectly regular stack for **b)** five, **c)** nine and **d)** thirteen layers, respectively. The optical properties of the individual building blocks were determined by ellipsometry. Modelling was carried out using a Matlab algorithm based on Rouard's technique.
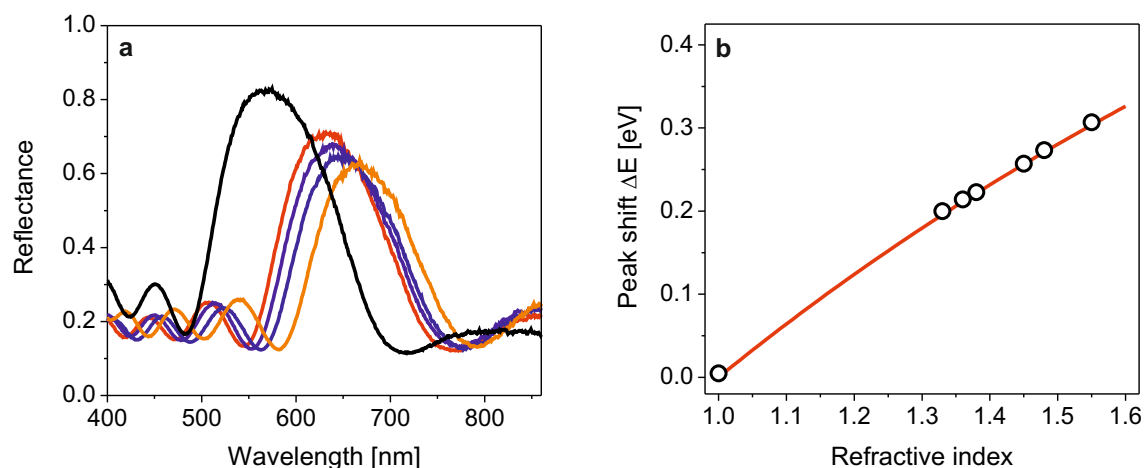
Figure 8.5: **Infiltration of an MDBR stack. a)** Optical response of a nine-layer MDBR stack in air (black) and after infiltration with H_2O (red), 2-propanol (blue), chloroform (green) and 1,2-dichlorobenzene (orange). **b)** Corresponding shift of the Bragg peak position as a function of the refractive index for six different infiltrated liquids. The red line corresponds to the theoretical shift of the Bragg peak, calculated by the symmetric Bruggeman effective medium approximation.

a polydisperse pore size distribution and allow only little control over porosity and pore sizes [26]. This route therefore decouples two important parameters in MDBR stack design - porosity and pore size - and allows control of both properties in a wide parameters space. Previous approaches to polymer-directed MDBR fabrication were limited by the extremely long fabrication times and did not allow for significant variation in porosity and pore size [9, 21]. The present route is fundamentally different due to the properties of the structure-directing agent PI-*b*-PEO. The high Flory-Huggins interaction parameter of the isoprene and ethylene oxide blocks, their low glass-transition temperatures and the high molecular weight are the main reasons why microphase separation occurs orders of magnitude faster than in the commercially available Pluronic (PEO-*b*-PPO-*b*-PEO) [34]. The large PI volume fraction (76.9 %) is the origin of the high porosity, yielding an inorganic material that is less susceptible to shrinkage and structural collapse. On the other hand it allows a large variation in the mixing ratio between the organic host and the inorganic guest, enabling fine control over the refractive index in the mesoporous films in the range of $1.4 < n < 1.9$. Moreover, the structural stability and fidelity during calcination can be maintained up to 700 °C, which allows superior electronic properties (see Chapter 7).

The presented approach is promising for a wide range of applications. In sensing, adsorption-desorption properties and their correlated MDBR optical response depend on the pore size as well as the chemical and structural nature of the pore walls [10], all of which can be individually controlled by the presented MDBR manufacture route. The variation of porosity should allow the optical detection of gas phase molecules and surface-binding molecules from solu-

tion. The fact that the MDBR can now be fully made out of a single, n-type material with full pore interconnectivity is promising for integration into optoelectronic devices, such as hybrid lasers or dye-sensitised solar cells. BCP-derived TiO_2 networks have recently shown outstanding performance as electrode materials in solid state dye-sensitised solar cells, which was attributed to the improved conductivity compared to NP films, as well as the manipulation of sub-bandgap states [35, 36]. The MDBR stack of Figure 8.2d is therefore an interesting candidate for the manufacture of dye-sensitised solar cells with integrated DBRs.

8.4   Conclusions

To summarise this chapter, a new materials route for MDBR manufacture is presented that harnesses the self-assembly of the PI-*b*-PEO block-copolymer in combination with simple hydrolytic sol-gel chemistry to generate optically uniform layers of well defined porosity. Varying the inorganic-to-organic mixing ratio enabled fine-control of the pore density (and thereby the refractive index), while the pore size can be tuned by the polymer's molecular weight. A 30 min annealing protocol per layer ensures sharp optical interfaces and supports the build-up of a crack-free stack. The resulting MDBRs exhibit a continuous network of pores with well defined dimensions, allowing full accessibility of the film with other functional materials. There is now an abundant range of sol-gel chemistry based approaches that are compatible with block-copolymer assembly [37, 38]. It is therefore possible to extend the presented TiO_2-based MDBRs to a wide range of ceramics and metal oxides. With the fine control over pore size, porosity and material composition, this approach presents new opportunities for MDBR manufacture and integration into functional devices.

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Chapter 9

Dye-sensitised solar cell based on a three-dimensional photonic crystal

9.1 Introduction

Ever since the pioneering work of O'Regan and Grätzel, dye-sensitised solar cells (DSCs) have attracted great interest as a promising technology for future sustainable energy generation [3]. The operation principle of a DSC as well as current challenges in device development are discussed in Chapter 3. In general, improvements in the overall power conversion efficiency have been focussed on further development of new dyes, manipulating the regeneration process by the use of alternative redox couples, improving the electronic properties of the n-type photoanode material and increasing long term stability by better encapsulation [4]. One way to further improve the efficiency of the device is to broaden the region of maximum incident photon-to-electron conversion efficiency (IPCE). The IPCE can reach values around $90\,\%$ at wavelengths of high dye extinction, typically in a spectral range from $510 - 560\,\text{nm}$. In contrast, the IPCE drops significantly in the tail of the absorption spectrum [5]. The engineering of dyes with a panchromatic absorption spectrum is therefore of central importance [6]. A complimentary route to reach broader absorption is the integration of optical elements in the device architecture. These can increase the optical path of the incident light and thereby the probability of the photons to be absorbed. Scattering layers in form of TiO_2 particles of several hundred nanometres in size have been found particularly beneficial [7, 8] and are now a common element in record efficiency cells [9, 10]. While the implementation of scattering particles has proven highly beneficial for enhanced light absorption, the diffusive scattering

over a broad spectral range has the detrimental effect of turning the cells opaque. This deprives the DSC from one of its unique selling points and thus, its potential use for integrated architecture. As a result, photonic band gap materials in the form of three-dimensional (3D) inverted TiO_2 opal or porous Bragg stacks have been applied to DSCs in order to enhance light harvesting in specific parts of the spectrum while retaining the cell's transparency in others [11, 12, 13, 14]. Several theoretical approaches report a variety of possible effects, including the slow propagation of photons near the edges of a photonic gap [15], Bragg diffraction in a periodic dielectric lattice [16], multiple scattering at disordered regions in the photonic crystal (PC) [17] and the formation of multiple resonant modes [18]. The latter effect, predicted by Mihi and Míguez [18] via a scalar wave approximation, has generated interest as it promises significant enhancement over a large part of the spectrum. According to these calculations, resonant cavities, determined by the penetration depth of the incoming light and the thickness of the mesoporous film between the PC and the substrate, give rise to photon localisation in the cell and therefore a much higher probability of photon absorption (see Chapter 3.2). The main challenge for the integration of a 3D PC into the DSC device structure lies in the appropriate coupling of the layers. An opaline array grown onto the mesoporous layer by evaporation induced self-assembly can only serve as a template, as to realise the necessary refractive index contrast. This has to be converted by infiltration with a high refractive index material, typically TiO_2, without clogging the mesoscopic pores of the underlayer that would otherwise inhibit sensitisation and electrolyte infiltration of the double layer device. In early approaches inverse opal PC layers could only be deposited directly on the transparent electrode rather than on top of a mesoporous TiO_2 layer [11, 12]. In order to minimise direct back-reflection of the incident photons, the cells had to be illuminated from the backside of the device, leading to a significant loss due to absorption in the platinum counter-electrode and the excess path length through the electrolyte [19]. Míguez and coworkers proposed that resonant modes, covering a large part of the spectrum, could only be exploited if the mesoporous TiO_2 layer was positioned in between the PC and the conductive substrate [20]. This was attempted in several studies [21, 22]. Recently, Lee *et al.* presented a new material route that enabled the beneficial layer sequence by infiltrating and thereby protecting the mesoporous underlayer with a copolymer during the subsequent fabrication of the inverse opal top layer. [23]. The effect of such a double layer configuration was subsequently characterised in great detail. According to their findings the material lacked the necessary intimate physical contact between the mesoporous and inverse opal layers to induce resonant modes. Furthermore, poor coupling of the two layers prevented charge carriers that were generated in the inverse opal layer to contribute to the overall photocurrent. This study emphasised the need for an approach to simultaneously deposit the mesoporous TiO_2 and the pore protective material in order to achieve pore and

electrical contact between the layers and thus fully integrate the PC into the device.

In this chapter a novel material route is presented for the assembly of a double layer DSC that couples an optically active 3D PC overlayer with a high surface mesoporous underlayer. Self-assembly-directed material synthesis on two length-scales enabled the fabrication of a double layer DSC with electric and pore connectivity at the mesoporous and the microporous level. Subsequent device characterisation allowed correlation of the construct's photonic properties to light harvesting and overall performance of the resulting DSC.

9.2   Experimental

For the fabrication of the block-copolymer (BCP) assembled mesoporous underlayer, a titanium containing sol was prepared by the rapid addition of 0.69 ml HCl (37 %) to 1 ml titanium ethoxide (purum) under vigorous stirring. A solution of 0.1 g PI-b-PEO BCP (M_n = 35.7 kg/mol, 23 wt% PEO) in 7 ml of tetrahyfrofuran (THF) was prepared alongside. After 90 min of stirring, 0.873 ml of the resulting sol was added to the polymer solution, before the volatile components were evaporated at 50° C in a Petri dish. Shortly after, the dry material was redissolved in an azeotrope mixture of of 72.84 wt% toluene and 27.16 wt% 1-butanol. Films were then deposited by spin-coating of the 20 wt% solution (5 s, 1500 rpm). After annealing the films by slow ramping up to 130° C (180 min linear ramp, 30 min dwell), a thin overlayer was removed by reactive ion etching (CF$_4$, 2 min, 50 W, 16 mbar, 3.56 MHz, 310 V, home-build system). The 3D PC was subsequently fabricated on top of this layer in three steps: a face-centred-cubic (FCC) colloidal array was deposited by evaporation induced self-assembly of polystyrene spheres. Three different sphere diameters (d_{iam}) were used for comparison: 240 nm (PC1, 0.5 vol% in ethanol, Ikerlat), 260 nm (PC2, 1.0 vol% in ethanol, Ikerlat) and 350 nm (PC3, 0.5 vol% in ethanol, Polybead). The template was then infiltrated by a binary atmospheric pressure chemical vapour deposition (APCVD). Subsequently, the samples were exposed by another cycle of reactive ion etching (CF$_4$, 5 min, see conditions above). Finally, the TiO$_2$ double layer structure was revealed by the calcination of the samples at 500 °C. For device characterisation, DSCs were assembled following a protocol as described elsewhere (dye N719) [24]. Please see reference [1] for further experimental details.

9.3   Results and discussion

A schematic representation of the fabrication method for a double layer self-assembled DSC is shown in Figure 9.1. In contrast to earlier approaches, a solution of PI-b-PEO BCP and TiO$_2$ sol served as fabrication base for the mesoporous underlayer. The layer was deposited

by spin coating or blade coating and temperature annealed to allow condensation of the in-organic network. At this fabrication stage the microphase-separated hybrid layer exhibits a continuous interdigitation between the BCP host material and the co-assembled TiO_2. As a consequence, the inorganic material is fully surrounded by protective organic material for further processing. The template for the PC top layer was subsequently deposited onto the hybrid film by evaporation induced self-assembly of polystyrene microspheres [25]. The covered substrate was placed vertically in an ethanolic suspension. Upon solvent evaporation, a uniform face-centered-cubic (FCC) colloidal PC template was formed on the hybrid under-layer. This three-dimensional template was then infiltrated by a binary atmospheric pressure chemical vapour deposition (APCVD, [26]). The template was heated to $80\,°C$ before being subjected to water vapour and titanium tetrachloride vapour in alternating cycles to form amor-phous TiO_2. Since the hybrid underlayer is non-porous, the APCVD of TiO_2 does not clog the
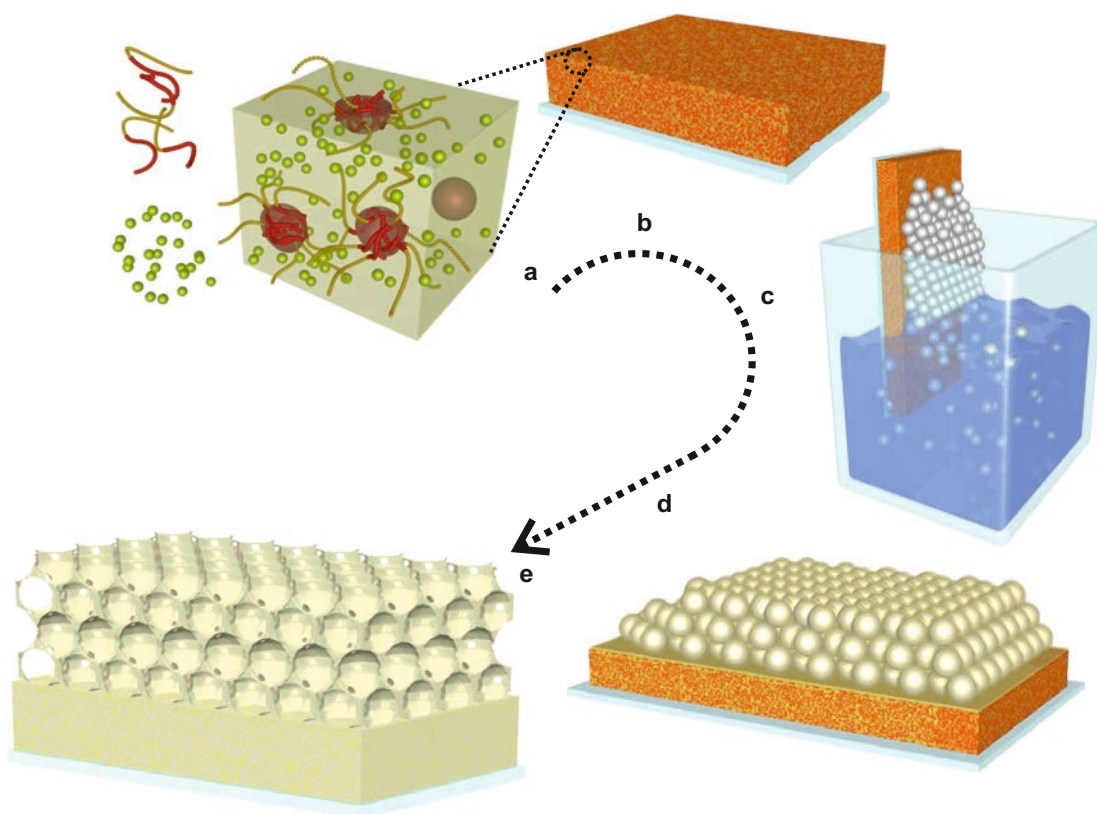
Figure 9.1: **Schematic of double layer assembly. a)** A solution of PI-*b*-PEO BCP and TiO_2 sol is **b)** co-deposited onto a FTO-covered glass substrate by spin-coating and solvent evaporation. **c)** The covered substrate is subsequently placed vertically in an ethanolic suspension of polystyrene microspheres to induce the self-assembly of the 3D PC template. **d)** This is followed by infiltration of the the interstitial pores in the colloidal array by APCVD of amorphous TiO_2. **e)** High tempera-ture calcination removes the BCP and colloids and crystallises the double layer TiO_2 photoanode.

pores of the underlying TiO_2 mesostructure, which would otherwise hinder sensitisation and electrolyte infiltration. After reactive ion etching of the continuous TiO_2 top layer, the double layer structure was heated to $500\,°C$ in order to remove the sacrificial polymer, crystallise the TiO_2 and reveal the pores on the 20 nm and 200 nm length scale, formed by BCP and colloidal self-assembly in the consecutive layers.

Electron microscopy of the TiO_2 double layer morphology is presented in Figure 9.2. The micrographs confirm the successful accomplishment of the fabrication route including the self-assembly of a 3D FCC polystyrene PC template on top of the hybrid thin film, the subsequent APCVD infiltration with TiO_2 and final removal of the organic material by calcination. A mesoscopic layer thickness of $\sim 465 \pm 30$ nm was measured by film profilometry, while the PC thickness was about 10 colloidal layers for a 0.5 vol% suspension and 20 colloidal layers for a 1.0 vol% suspension, as determined by SEM image analysis. The pore connectivity between both layers is visible in Figure 9.2b, confirming that the fabrication method provided an effective protection for the mesopores during the filling of the PC template by APCVD. This is an important requirement for effective dye sensitisation of the high surface area mesoscopic underlayer as well as the unhindered electrolyte diffusion throughout the photoanode. Furthermore, the APCVD infiltration appeared to be uniform throughout the crystal with no evidence of delamination from the PC overlayer.

Figure 9.3a shows the top surface of the (111) crystal plane of the inverse opal TiO_2 PC layer obtained after deposition of 240 nm PS spheres, APCVD, CF_4 etching of the TiO_2 overlayer and high temperature calcination. Figure 9.3b displays a photograph of a TiO_2 double layer (PC3). Note the complementary colours of the reflected and transmitted light. In Figure
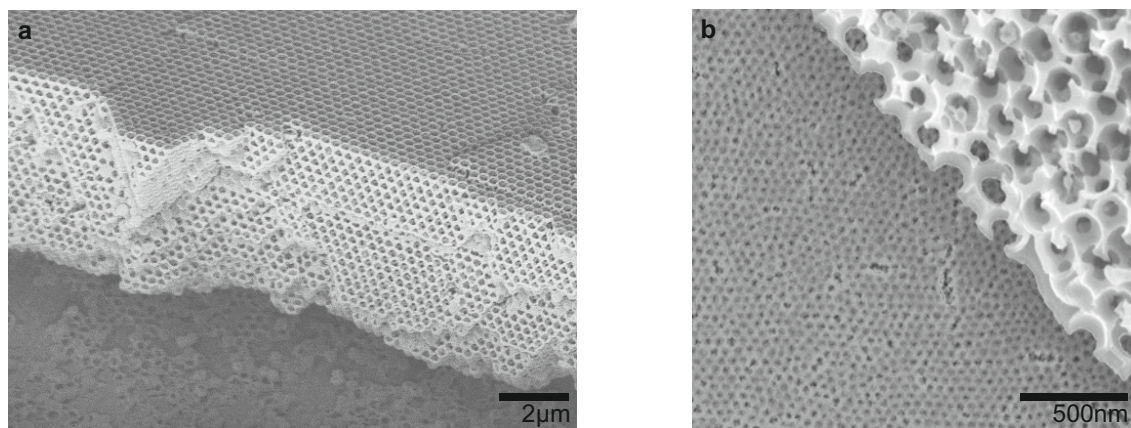

Figure 9.2: **Electron microscopy of a TiO_2 double layer morphology.** SEM cross-sectional micrographs of **a)** the inversed TiO_2 opal PC on top of a mesoscopic TiO_2 underlayer after high temperature calcination. **b)** High resolution micrograph showing good pore connectivity between mesopores and micropores. **a), b)** *Reprinted from [27]. Copyright Stefan Guldin.*

9.3c the optical transmission spectrum through the self-assembled FCC PC template is shown for all three diameters used in this study. The transmission dips at 500 nm (PC1), 540 nm (PC2) and 825 nm (PC3), corresponding to the Bragg reflection peaks of the (111) Γ-L pseudo-gap of PS spheres with diameters of 210 nm, 227 nm and 350 nm, respectively (n_{eff} = 1.46). In Figure 9.3d the transmission spectrum for the different stages of the fabrication process is shown for PC3. After infiltration of the colloidal array with amorphous titania, the transmission dip shifted to 850 nm. Calcination and crystallisation of the TiO_2 lattice contraction led to an TiO_2 inverse opal with 240 nm pores, which is in line with the corresponding TiO_2 transmission spectrum in air. From these measurements, it follows that the presented fabrication method is capable of producing high quality photonic crystal structures with the expected optical characteristics.
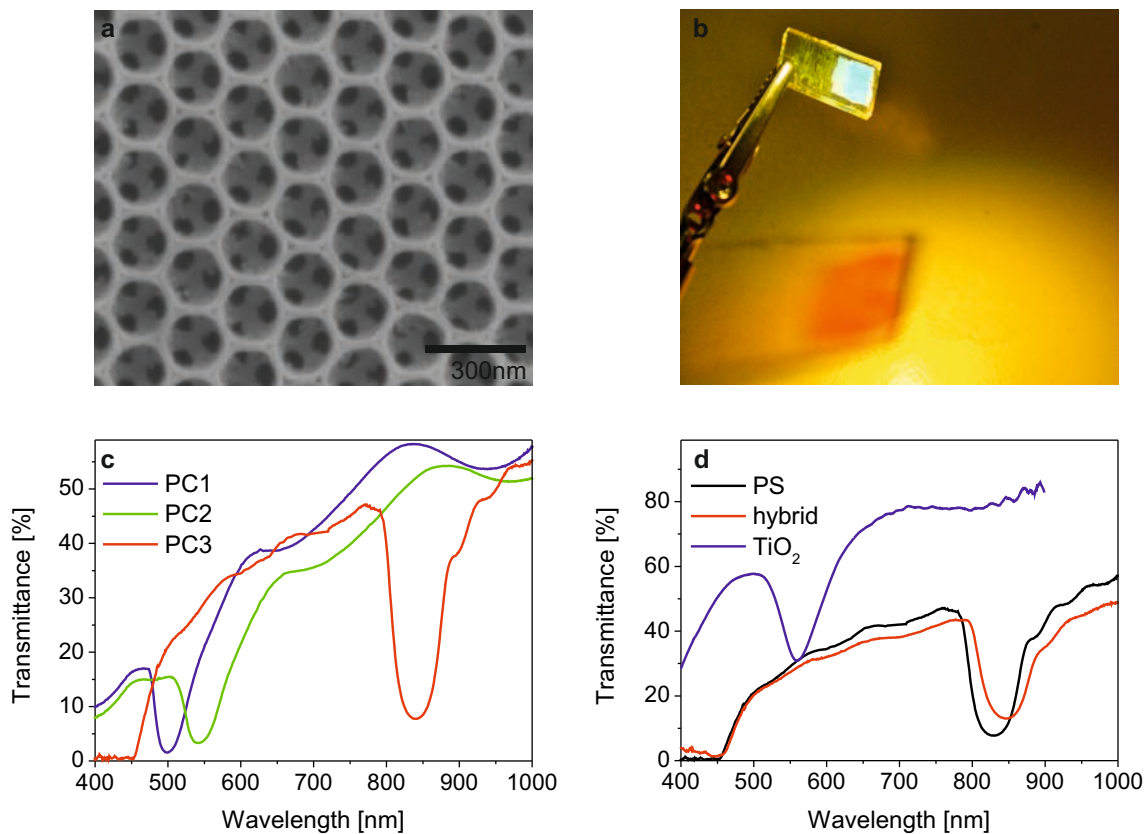
Figure 9.3: **Optical properties of 3D PC. a)** SEM micrograph showing the (111) top surface of the resulting inverse TiO_2 opal PC1. **b)** Photograph of a TiO_2 double layer with PC3. **c)** Uv-vis transmittance spectrum of the colloidal PC templates for PC1 (blue, d_{iam}: 240 nm), PC2 (green, d_{iam}: 260 nm) and PC3 (red, d_{iam}: 350 nm). **d)** Transmission spectrum of the PC3 sample for the different stages of the fabrication process: PS colloidal array in air (black), infiltrated template (red) and TiO_2 inverse opal in air after calcination (blue). *a), c) Reprinted from [27]. Copyright Stefan Guldin.*

In order to reveal the significance of the PC top layer for light harvesting, the IPCE behaviour of double layer DSCs was compared to a single layer reference device. For this study, a relatively thin TiO$_2$ underlayer (465 ± 30 nm) was chosen to avoid the formation of cracks. These typically appear in films thicker than about 1 μm and may give rise to light scattering. (The findings presented in Chapter 7 would now allow the fabrication of significantly thicker crackfree films.) A double layer device consisting of a 465 nm underlayer with 32 % porosity and a 1.4 μm PC top layer with 78 % porosity was modelled to have a similar surface area as an approximately 900 nm thick single mesoporous film, which was therefore used as a reference.

The effect of the PC top layer on the absorption spectrum of the overall device was herein of particular interest. Double layer devices incorporating 3D PCs of different pore diameters, related to the sphere size used in their fabrication, were compared to the absorption of a reference cell without a PC but a thicker mesoporous layer. For all IPCE measurements, a 1mm^2 surface was illuminated from the FTO side with an intensity of 100 mW/cm^2 (AM 1.5). The IPCE characteristics of the three PC cell types are shown in Figure 9.4. Two main characteristics of the double layer devices are apparent in the IPCE and normalised IPCE spectra. First, double layer devices with a comparable surface area to that of the single layer reference were found to have comparable peak absorption values in the measured spectral range, as seen for PC1 (a) and PC3 (c). In contrast, PC2 has a significantly thicker PC top layer ($\sim$ 3 μm) and therefore, a roughly 40 % higher surface area when compared to the double layer devices PC1 and PC2, or the reference cell. The fact that the IPCE increased accordingly supports the assertion that the PC top layers are electrically connected and contribute to light harvesting over the entire measured spectrum.

The PC layers were also optically characterised. The spectral region of the stop-band in the device is illustrated as hatched areas in Figure 9.4. When normalised to the IPCE maxima in Figure 9.4d-f, the significance of a PC top layer for spectrally selective light harvesting is revealed. Comparing the normalised IPCE of different PC double layer devices with the reference cell, it is evident that the observed absorption spectrum of the device is strongly influenced by the PC top layer. The broadening of the normalised absorption peak moves with the position of the Bragg peak, from deep blue to red. The physical origin of this effect cannot be exclusively related to scattering effects. These would occur most efficiently around $\lambda \sim 1.35 \cdot d_{\mathrm{iam}}$, where d_{iam} is the diameter of the scattering object, i.e. in the deep blue for all three model systems [28]. Furthermore, scattering at defect planes should be closely related to the ratio of d_{iam}/λ, leading to very low scattering probabilities in the observed region of enhancement for all three feature sizes [17]. Nevertheless, a small fraction of the observed absorption shift can be correlated with scattering, best seen in Figure 9.4f as a slightly increased absorption shoulder in the blue. Furthermore, the slight increase in relative absorption between
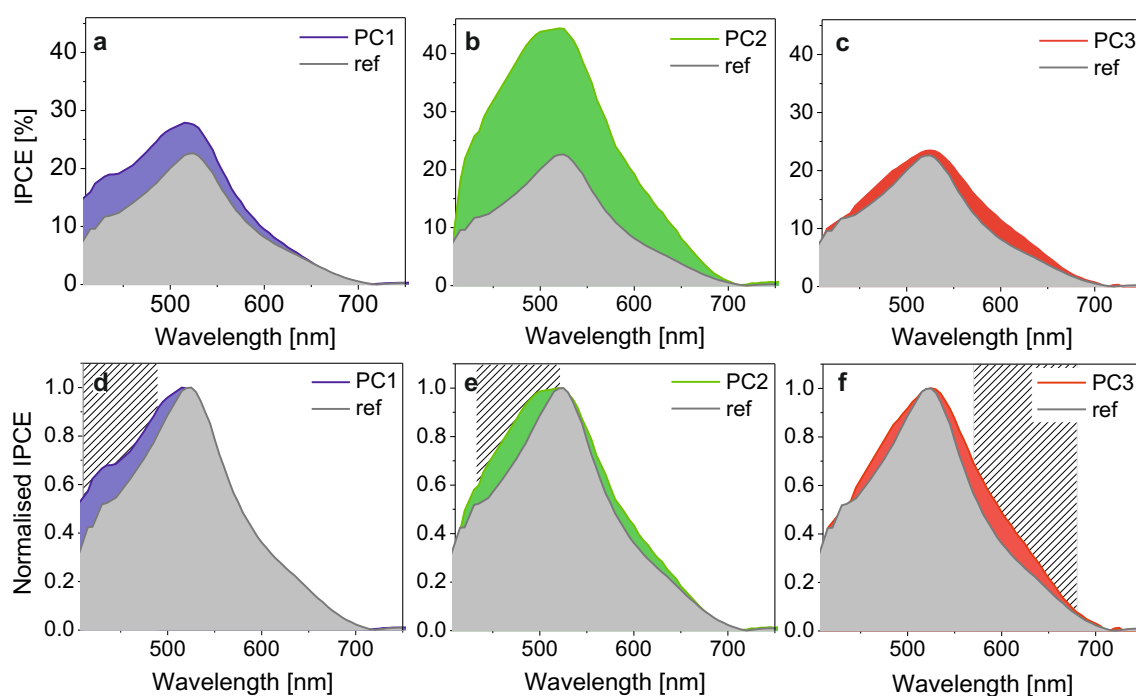
Figure 9.4: **Incident-photon-to-electron conversion efficiency.** **a)** - **c)** IPCE of devices with photonic crystal top layers compared to a single layer reference device. The available surface area of devices **a)** PC1 (blue) and **c)** PC3 (red) are comparable to the surface area of a 900 nm thick mesoporous single layer device (black). **b)** PC2 (green) has a PC of double thickness coupled to the 465 nm thick underlayer and therefore significantly more surface area. **d)** - **f)** Relative spectral IPCE of the different cell types normalised at a wavelength of 520 nm. The hatched area illustrates the active region of the 3D PC ($n_{TiO2} = 2.3$, $n_{elec} = 1.34$).

550 nm and 650 nm in PC2 can be related to the increased overall surface area of the device as compared to PC1, PC3 and the reference cell. Due to the poor absorption of the dye in this wavelength range, an increased film thickness will lead to a relative enhancement of the IPCE in this region [29]. In contrast, the substantially increased IPCE in the red for the PC3 cell in Figure 9.4 arises from the PC resonance at 625 nm. Finally, the enhancement is found in a wider spectral region than is expected in the case of slow photon propagation modes at the red edge of the photonic band gap [15].

These results are in agreement with a recent experimental study by Lee *et al.* who identified three main effects for the increase in photocurrent in double layer DSCs [23]: (I) multidirectional scattering of short wavelength photons due to defects in the PC layer [12], (II) back reflection of light in the stop band region of the PC due to the PC layer acting as a dielectric mirror, and (III) an absorption enhancement caused by resonant modes as predicted by Mihi and Míguez [18]. Lee *et al.*'s approach of adding a photonic crystal top layer resulted, however, only in a weak correlation between the absorption properties of the device and the optical

properties of the 3D PC. They assigned this finding to a lack of physical contact between the layers and a rough interface [23]. In contrast, the herein presented fabrication method results in a close contact and a smooth interface between the mesoporous TiO_2 and the photonic crystal. This enables a significant enhancement in specific parts of the action spectrum as well as additional charge carrier generation arising from the photoactive material of the photonic crystal, which is now a functional part of the DSC.

Figure 9.5a shows a schematic of a DSC based on the self-assembled double layer photoanode. Current-voltage ($J - V$) measurements of the cell types were carried out under standardised AM 1.5 illumination of 100 mW/cm^2 (active area 0.13 cm^2, spectral mismatch 22 %). In Figure 9.5b the $J - V$ curves are shown for the double layer PC3 device in comparison to a reference cell. The PC3 exhibited a 10 % increase in photocurrent compared to the reference cell, with $J_{sc} = 4.7$ mA/cm^2. This is in accordance to the IPCE measurements shown in Figure 9.4c. The double layer device featured, however, a slightly lower open circuit potential V_{oc} (0.74 V $vs.$ 0.77 V) and a 15 % decrease in fill factor FF (0.52 $vs.$ 0.61). As a consequence, the overall conversion efficiency η of 1.8 % was 0.2 % lower than for the reference cell. Míguez and coworkers recently pointed out that very thick inverse opal films (> 5 μm) are likely to have an adverse effect on charge transport and recombination through the cell, which may result in a penalty in photovoltage and photocurrent under real operation conditions [13]. Device fabrication has not been optimised in this study and only served as a proof of principle. Therefore, this hypothesis can be neither rejected not supported. Meanwhile other groups have further developed the presented concept and achieved efficiencies of up to 4.6 % [30, 31, 32]. Fabrication techniques for the assembly of a defect-free 3D PCs made of TiO_2 have evolved [33, 34], and studies on the development of BCP-derived TiO_2 films have led to the forma-

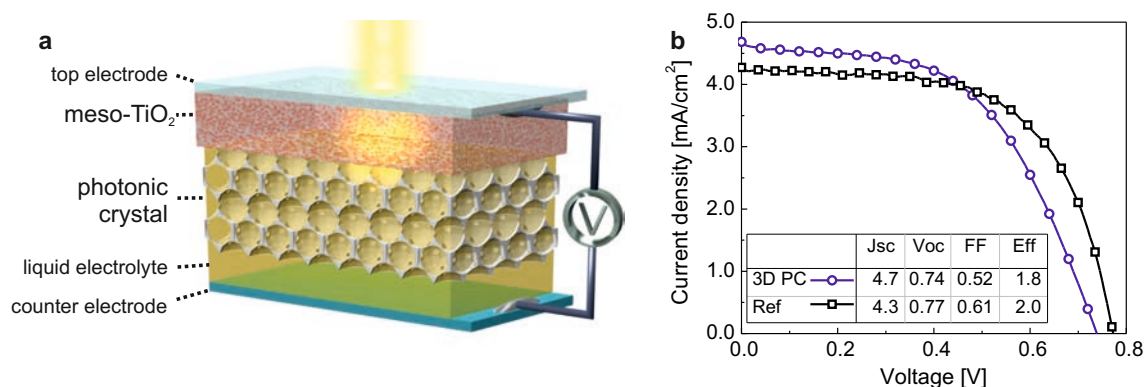
Figure 9.5: **Device schematic and $J - V$ characteristics. a)** Schematic of a fully assembled DSC based on the self-assembled double layer photoanode. **b)** $J - V$ characteristics of the double layer device PC3 (blue) and a reference single layer cell of similar internal surface area (black) under standardised AM 1.5 illumination.

tion of significantly thicker crack-free films [35] (see Chapter 6). These advances may soon lead to further overall efficiency improvements. As an alternative concept to a 3D PC, the integration of a 1D PC in form of an mesoporous Bragg reflector (MDBR) has recently been proposed with reported efficiencies of up to 7.0 % [13, 36]. MDBRs typically exhibit a broader stop-band and promise a less elaborate fabrication. Certainly the approach of BCP-directed, tunable MDBRs, presented in Chapter 8, is viable to improve this concept. The fully electron-conducting architecture would enable light absorption and charge generation by the optical element, thus integrating the 1D PC as an active component in the device. Another promising concept is to couple PC-based reflectors behind the counterelectrode, where they are not an electronically active part of the device but enable effective light management and redistribution of non-absorbed photons. A recent study by Hwang *et al.* emphasises that non-absorbed light can be better redistributed in the device by a coherent diffraction element such as a 3D PC in comparison to a metallic backreflector or a scattering layer [37]. Comparing these three optical elements to a reference DSC, they found an overall conversion enhancement of 14 % for a 3D PC, compared to 4.7 % when using a metal back reflector and 2.1 % for a scattering layer. This lead to an overall power conversion efficiency of 12.2 % for PC-based DSCs.

9.4   Conclusions

In conclusion, a fabrication method for a TiO_2 electrode architecture is presented which couples an optically and electrically active 3D PC top layer to a high surface area mesoporous underlayer. In contrast to earlier studies, the double layer structure exhibits porosity at the mesoporous and the microporous length scales as well as pore and electronic connectivity at all levels. This construct enables effective dye sensitisation, electrolyte infiltration and charge collection from both the mesoporous and the PC layers. Due to the smooth layer interface and the direct physical and electronic contact between the layers, light harvesting in specific parts of the spectrum was significantly increased by exploiting PC-induced resonances. Further investigation of its device photovoltaic characteristics, including charge mobility and recombination rates as well as optimisation of the PC structure are needed to fully exploit the IPCE increase. This is the first approach to fully integrate a PC top layer into a functioning DSC, opening an additional parameter space for effective light management. Finally, since the integration of an electrically and optically active PC increases the absolute IPCE and broadens the light harvesting capability of DSCs, this approach should be useful in solid state devices where pore infiltration is a limiting factor [38, 39] as well as in weakly absorbing organic photovoltaic devices [40].

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Chapter 10

Block copolymer assembled antireflective coatings with self-cleaning properties

Work in preparation for publication by Stefan Guldin *et al.* [1]

10.1 Introduction

Since Fraunhofer's [2] and Lord Rayleigh's [3] first experimental approaches to reduce light reflection off optical interfaces, antireflective coatings (ARCs) have been in the constant focus of scientific and industrial interest. While the underlying physical origin is long understood, the implementation of broadband antireflective coatings on low refractive index substrates remains a challenge. Antireflection (ar) is typically achieved by destructive interference of light reflected from the two (or more) interfaces of a thin film optical coating (schematic in Figure 10.1). Two conditions have to be fulfilled for a single layer ARC: (1) Phase matching requires an optical layer thickness h_{ar} of one quarter of the wavelength of the incident light λ: $n_{ar}h_{ar} = 1/4\lambda$. (2) Complete destructive interference further depends on amplitude matching of the reflected beams, i.e. $n_{ar} = \sqrt{n_0 n_s}$, with n_{ar}, n_0, n_s as the refractive indices of the ARC, the medium of the incident beam and the substrate, respectively [4]. While the first condition is easily met with modern deposition techniques, the second requirement poses a challenge. Many transparent substrate materials have a refractive index of around 1.5, thus requiring $n_{ar} \sim 1.22$. For thin film processing, magnesium fluoride with $n \sim 1.37$ is one of the lowest-index materials, which fulfills the second condition only for high refractive index substrates ($n_s \sim 1.9$) and yields a much lower optical performance when used as coating for common glasses and transparent plastics [4]. A further decrease in refractive index can only be achieved by the introduction of porosity on the sub-optical length scale. The effective refractive index

is then a direct consequence of the material-air composite and can be approximated by various effective medium theories, such as the Bruggeman model [5, 6, 7] (see Chapter 2.5).

Phase separation on the nanometre scale with subsequent removal of one sacrificial phase is a practical route to ultralow refractive index layers. This concept was established by Walheim *et al.* for nanophase separated polymer films [8] and subsequently extended to mesoporous inorganic coatings [9]. Other methods to prepare low refractive index layers by solution processing include the controlled assembly of colloids by electrostatic attraction [10] and the layer-by-layer deposition of SiO_2 nanoparticle films [11]. Gombert *et al.* introduced an antireflective film based on the replication of a sub-wavelength surface relief from a master template by nanoimprint-lithography [12]. Vacuum-based fabrication methods for ultralow refractive index layers on glass include glancing angle and chemical vapor deposition [13, 14].

An alternative concept to antireflection takes inspiration from the nanostructured topography of the corneal lenses, found in moth eyes [15, 16]. Cone-like structural features arranged on a hexagonal grid with a lattice constant below the diffraction limit give rise to a continuous refractive index gradient between air and substrate, therefore removing the sharp optical interface. This was initially realised for microwave frequencies by standard photolithography [17]. Recently, reactive ion etching using colloidal masks [18] or a metal-particle containing resist [19] allowed access to sub-100 nm feature sizes and therefore reduced light reflection in the visible spectrum. Although this is a promising concept, the necessary fabrication routes are elaborate and yield so far no competitive optical response compared to interference-based ARCs.

While research-grade nanostructured ARCs are close to perfection, their implementation in commercial products is hampered by their lack of wear resistance and optical variability caused by contamination of the composite network. In particular for outdoor applications, ARCs need to be structurally resistant and should recover from ambient pollution. The latter can in principle be implemented through self-cleaning based on surface superhydrophobicity or photocatalysis [20]. Superhydrophobic surfaces are self-cleaning in a sense that particulate contaminants adhere only very weakly and are easily washed off by water. Photocatalytic coatings, on the other hand, do not rely on a cleaning medium, but decompose organic contaminants by light induced redox-reactions. While photocatalytic self-cleaning is in principle more robust, the inclusion of a photocatalytic component in ARCs, typically TiO_2, poses a major challenge because of the high refractive index of $n_{TiO_2} > 2.5$. Several concepts have been proposed to combine self-cleaning and antireflection, including the surface coating of a colloidal-based ARCs with TiO_2 [21], the co-deposition of TiO_2 and SiO_2 nanoparticles to form a porous ARC [11] and a double layer structure of low refractive index SiO_2 and TiO_2 [22, 23]. All of these approaches require a high-temperature processing step, which prevents

their use on flexible, plastic-based substrates. Furthermore, the structural arrangement on the nanometre-scale limits the achievable porosity and thus, the volume fraction of TiO_2 that can be incorporated without compromising on the resulting effective refractive index.

In this chapter a new concept is presented towards the combination of antireflection and photocatalysis, which relies on the use of a high molecular weight PI-*b*-PEO block copolymer (BCP) in combination with silica-based sol-gel chemistry. The approach makes use of the micellisation of the hybrid system under non-equilibrium processing conditions, as discussed in Chapter 5. Upon spin coating, the sacrificial colloidal micelles arrange in a face-centred cubic (FCC) geometry, thereby co-assembling the inorganic material in an inverse-opal like morphology of ultralow refractive index. Thus, the approach allows for partial substitution of silica-type material with high refractive index TiO_2 nanocrystals. The interplay TiO_2 incorporation and resulting self-cleaning properties is investigated as well as the optical performance of the coatings and their processing on a variety of substrates.

10.2 Experimental

ARC fabrication

Two different PI-*b*-PEO copolymers were used as structure-directing agents in this study: I) BCP-34: M_n = 34.4 kg/mol, 28 wt% PEO and II) BCP-92: M_n =91.6 kg/mol, 28.6 wt% PEO. TiO_2 nanocrystal synthesis was carried out by Dr. Peter Kohn, using a similar method as reported in reference [24]. The resulting wet precipitate was dried for two hours in ambient conditions and then redissolved in an azeotrope solvent mixture of toluene (72.84 wt%) and 1-butanol (27.16 wt%). To maintain consistent concentrations of TiO_2 nanocrystals in the azeotrope solution (20 μg per ml), a fraction of the precipitate was fully dried and heated to 350 °C aside in order to reveal the weight content of TiO_2. The aluminosilicate sol was prepared as described in Chapter 5.2. Three different hybrid solutions were created. For 25 wt% TiO_2 loading, 50 mg polymer was dissolved in 0.7 ml of azeotrope solvent and a further 0.5 ml of TiO_2 solution, before 56 mg aluminosilicate sol was added. For 37.5 wt% TiO_2 loading, 50 mg polymer was dissolved in 0.5 ml of azeotrope solvent and 0.7 ml of TiO_2 solution, before 47 mg sol was blended in. A 50 wt% TiO_2 solution was prepared by adding 50 mg polymer to a mixture of 0.6 ml azeotrope solvent and 0.94 ml TiO_2 solution, before 37.5 mg sol was added. The hybrid solutions were then stirred for one hour and further diluted as needed to match the required film thicknesses. Hybrid films were deposited onto pre-cleaned glass slides by spin coating (2000 rpm, 20 s). The cast films were annealed on a hotplate by gradual increasing the temperature to 200 °C (180 min linear ramp, 30 min dwell time). Finally, the organic

component of the hybrid films was removed by reactive ion etching in oxygen plasma (30 min, 100 W, 0.33 mbar, STS Instruments, 320PC RIE). Because of the limited temperature stability of the PET (polyethylene terephthalate) substrates, thermal annealing of ARCs on flexible substrates was reduced to 130 °C (15 min linear ramp, 5 min dwell time), before the substrates were similarly exposed to 30 min oxygen plasma. For flexible substrates, a aluminium sample holder was built to allow double-sided coating.

ARC characterisation

Optical characterisation was carried out on a Olympus BX51 microscope with 5× magnification, where a 600 µm fibre (Ocean Optics "QP600-2-SR") and a high resolution spectrometer (Ocean Optics "QE65000") were coupled into the beam path. Determination of optical constants was performed on a spectroscopic ellipsometer (Wollam "alpha-SE"), and the data was fitted with the manufacturer's software. For determination of the photocatalytic activity, stearic acid (analytical standard) was deposited by spin coating of a 8.8 mM solution in methanol (1500 rpm, 20 s). A xenon lamp (Bentham "IL75E", 75W) was used to simulate the solar irradiation in the ultra-violet spectral region. The absolute power density of the laboratory light source in the $275 - 375$ nm spectral band, i.e. where TiO_2 absorbs, was adjusted to the integrated value of the solar AM 1.5 spectrum (2.89 mW/cm^2). The uv irradiation intensity was determined using a power meter (Spectra Physics "Mod 407A") with bolometer head and a UV bandpass filter (Thorlabs "FGUV11") [25]. The photocatalytic decomposition of stearic acid was monitored by periodic FTIR measurements (Thermo Scientific "Nicolet iS10").

10.3   Results and discussion

Figure 10.1 illustrates the materials route for ARC manufacture. A high molecular weight PI-*b*-PEO BCP was dissolved in an azeotrope mixture of toluene and 1-butanol. An silica-based sol was prepared separately by the stepwise hydrolysis of a silicon/aluminium alkoxide mix (9/1 molar ratio) [26]. TiO_2 nanocrystals were synthesised via a non-hydrolytic sol-gel chemistry route [27] and compatibilised with the azeotrope solvent mixture. The components were subsequently combined in a organic to inorganic weight ratio of 4 to 3 with varying amount of TiO_2. The hybrid solution could then be processed into a thin film by spin coating, dip coating or meniscus coating. Following a temperature annealing step to condense the inorganic matrix, the organic components were removed by reactive ion etching in an oxygen plasma. See the experimental Section 10.2 for further details.
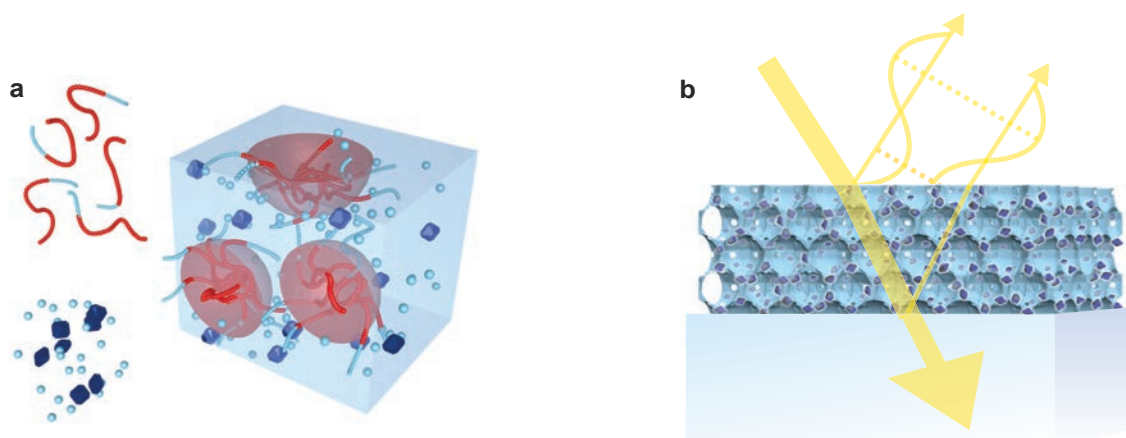
Figure 10.1: **Schematic of ARC manufacture. a**, A solution of PI-*b*-PEO block copolymer, silica-based sol and compatibilised TiO$_2$ nanocrystals is used for the coating of transparent substrates. The inorganic components preferentially reside in the PEO phase and are therefore structure-directed during the micellar packing of the block copolymer. **b**, Subsequent reactive ion-etching in an oxygen plasma removes the polymer and reveals an inorganic inverse opal-type structure that is loaded with TiO$_2$ nanocrystals. Phase and amplitude matching of the optical coating give rise to destructive interference of reflected light, i.e. enhanced transmission, while the embedded photocatalytic TiO$_2$ nanocrystals prevent contamination of the ARC.

The resulting porous inorganic films are shown in Figure 10.2. Scanning electron microscopy (SEM) images show a network morphology that reveals its likely origin. The well-defined pore size and the local hexagonal arrangement is reminiscent of an inverse opal structure. The evolution of this morphology probably involved the formation of block-copolymer micelles in solution, which during solvent evaporation self-assembled into an opal morphology consisting of a PI core and a PEO+sol matrix. The condensation reaction and polymer removal then gives rise to the discernible network structure. Since the micellar size is determined by the polymer architecture, a variation of the solid organic to inorganic volume (or weight) fraction allows fine tuning the porosity, while affecting the pore size only very little. The interplay between mixing ratio and porosity is shown in Figure 10.2a-c, where the polymer weight fraction in the initial solution compared to the total weight of BCP and resulting silica-type material was increased from 33 wt% to 50 wt%. The pore size of the inorganic network can be separately controlled by varying the molecular weight of the sacrificial PI block (see Chapter 5 for further details).

Figure 10.2d shows the morphology of the film with similar inorganic loading as in Figure 10.2c but an increased molecular weight of the PI block. While a molecular weight of 24.8 kg/mol led to a pore size of ∼ 33 nm (Figure 10.2a-c), increasing the PI chain length to 62.7 kg/mol resulted in ∼ 53 nm-wide pores. This is in good agreement with scaling laws governing polymer chains in a good solvent [28]. The radius of gyration of the pore forming

PI block scales by a factor of 1.59 when increasing the molecular weight from 24.8 kg/mol to 62.7 kg/mol. This is consistent with the pore size determination by SEM image analysis, shown previously in Chapter 5. The pore interconnectivity, arising from the close-packing of sacrificial micelles, can be clearly identified.

Spectroscopic ellipsometry of the resulting films revealed that the refractive index could be finely tuned in the range $1.40 < n_{ar} < 1.13$ ($\lambda = 632$ nm) by varying the polymer weight fraction from 28 % to 67 % (see Chapter 5). The Bruggeman effective medium approximation for a network of air voids in an aluminosilicate matrix ($n = 1.52$) results in a porosity value $p \sim 73$ % for $n_{ar} = 1.13$. In conventional approaches to form mesoporous inorganic films, porosity arises from the interstitial space between packed silica nanoparticles or colloids. Random packing, i.e. jamming of monodisperse spheres leads to packing densities of $\sim 62 - 64$ %, i.e. $p \sim 36 - 38$ % [29]. Experimentally, nanoparticle-based approaches readily achieve $p \sim 40$ % [30]. A further increase in pore volume may be realised by the introduction of a sacrificial spacer material, resulting in $p_{max} \sim 50 - 60$ % [31]. The packing density of colloidal monolayers typically yields $p \sim 39$ % [32]. The origin of pore formation in the present route is fundamentally different to previous approaches as the pores arise from sacrificial micelles and not from the close-packing of high refractive index components. The inorganic material resides in the hydrophilic outer layer of the micelles and is therefore co-assembled in an inverse-opal like geometry. As a consequence of the close-packing of pores, porosity values up 73 % were reached after the removal of the BCP. Alternatively, high porosi-
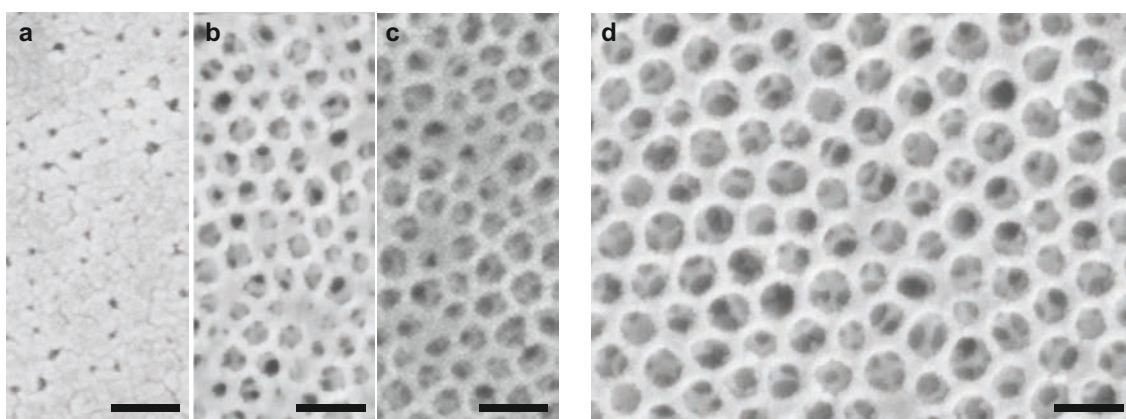
Figure 10.2: **Film morphology of mesoporous optical coatings. a - c** Scanning electron microscopy top-view of mesoporous silica-type films, stemming from a solution of BCP-34 of molecular weight $M_n = 34.4$ kg/mol and a polymer weight fraction of **a**: 33 %, **b**: 40 % and **c**: 50 %, relative to the total weight of BCP in the initial solution and resulting silica-type material. **d** The use of a higher molecular weight polymer BCP-92 ($M_n = 91.6$ kg/mol), results in significantly larger pores and identical refractive index for otherwise similar conditions (here: 50 % polymer weight content). The scale bars represent 100 nm.

ties can be achieved by sol infiltration into a BCP-assembled gyroid template [33], leading to a pore volume of 66 %. However, template formation is dependent on delicate structure control, which requires annealing of the films in a solvent-vapor atmosphere and film thicknesses above 130 nm. In contrast, the pore volume in the presented method can be adjusted by place-holder micelles, where size and concentration can be easily controlled.

Adsorption of organic contaminants from the ambient atmosphere typically deteriorates the performance and long-term usability of mesoporous ARCs, particularly in outdoor applications. TiO_2-based photocatalysis can be used to degrade the adsorbed hydrocarbons and restore ARC performance. In several previous studies the incorporation of photocatalytic TiO_2 was reported, realised either by surface coating [21], blending [11] or in double layer stacks [22, 23]. The amount of TiO_2 that can be added to the ARC is, however, relatively small because of the resulting increase in refractive index. The presented approach leads to exceptionally low refractive index layers, which therefore allows to maximise TiO_2 loading. This was achieved by the incorporation of crystalline 4-nm-sized TiO_2 nanoparticles that were synthesised via a non-hydrolytic sol-gel chemistry route [27, 34].

The sol-gel approach was modified to compatibilise the nanoparticles with the solvent used in the polymer/silica-sol solution. The incorporation of already crystalline TiO_2 has several advantages: No high-temperature step during the film fabrication is necessary to crystallise the TiO_2. Furthermore, rather than forming a stoichiometric $Ti_xSi_{1-x}O_2$ blend, which is often observed for a mix of silica and titania precursors [35], photoactive TiO_2 hot spots are created within the network. While a post-treatment of ARCs with TiO_2 precursor results in additional materials deposition, the present route enables substitutional incorporation. Figure 10.3 shows the variation of the ARC's refractive index as a function of the weight fraction of TiO_2 nanocrystals in the initial hybrid solution. The refractive index scales with the replacement of alumunosilica by TiO_2 according to the Bruggeman effective medium approximation [5, 7]. Starting from a refractive index of ~ 1.13 for a mesoporous silica-type film without TiO_2, this value increased to $n \sim 1.19/1.22/1.26$ when 25/27.5/50 wt% aluminosilicate in the initial solution was replaced by TiO_2 nanocrystals. Thus, due to the ~ 73 % porosity of the inorganic network, up to 50 wt% aluminosilicate can be substituted by TiO_2 while maintaining sufficiently low refractive indices.

The optical properties of the fabricated ARCs are presented in Figure 10.4. A comparison of non-catalytic films is shown Figure 10.4a. Porosity tuning by adjusting the inorganic to polymer mixing ratio (without the inclusion of TiO_2 nanocrystals) allowed the fabrication of an silica-type film with $n \sim 1.22$ and $h \sim 110$ nm. When coated on both sides of a glass slide, the ARCs demonstrated their high optical quality with light transmittance $\mathcal{T}$ up to 99.8 %, shown in red. In direct comparison, the commercial benchmark for laboratory-use glass, a polymeric
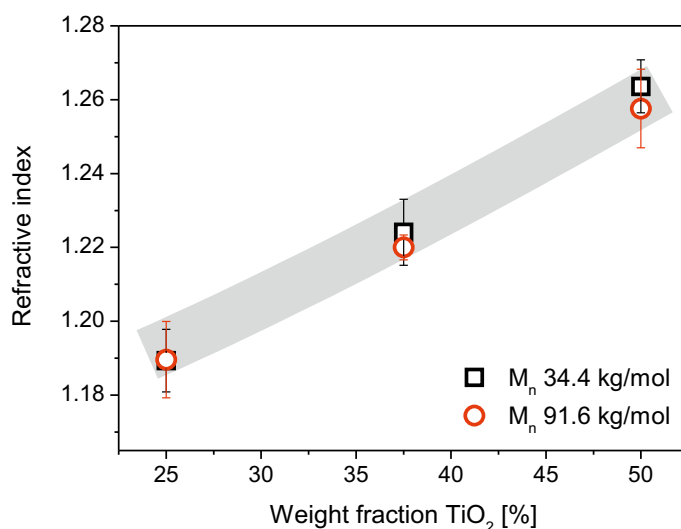
Figure 10.3: **Refractive index as a function of TiO$_2$ nanocrystal loading** for mesoporous films derived from BCP-34 and BCP-92. The weight ratio between inorganic and organic constituents was kept constant at 3:4, while the aluminosilicate weight fraction in the initial solution was partially substituted by TiO$_2$ nanocrystals. As a guideline, the expected scaling of the refractive index as a function of the TiO$_2$ weight fraction, based on the Bruggeman effective medium approximation, is indicated in grey.

adhesive named "Arktop" (Asahi Glass) achieved a similarly high peak value $\mathcal{T}_{max} \sim 99.5\,\%$ (blue), but in a more limited spectral range. The transmittance of a reference glass slide without coating is shown in black. Figure 10.4b displays the optical properties of a highly porous film, where 50 wt% aluminosilicate was substituted by photocatalytic TiO$_2$ nanocrystals. Here, a maximum transmittance of 99.3 % was measured. The inclusion of a photocatalytic materials into inorganic ARCs, using at low temperature protocol, makes the deposition technique attractive for the coating of flexible plastic substrates, such as PET (polyethylene terephthalate). In Figure 10.4c the effect of a double-sided photocatalytic coating onto the optical properties of a PET substrate is displayed. The sample exhibited a slightly lower peak transmittance of 98.8 %, which is on the other hand spectrally more broad band. PET is a promising substrate material for organic solar cells and flexible flat panel displays [36]. Material routes to ARCs on PET are challenged by the limited temperature and chemical stability of the substrate material. Hyun and coworkers reported the reduction of reflectance to $\mathcal{R}_{min} \sim 1\,\%$ by coating the substrate with a mesoporous silica film via a water-soluble structure directing agent [37]. Nanoimprinting of a sub-wavelength surface relief is another viable option, yielding transmittance values of $\mathcal{T}_{max} \sim 98.3\,\%$ ($\lambda \sim 600\,\mathrm{nm}$) [38]. Yet, both approaches do not yield self-cleaning surfaces. The additional coating of the ARC with photocatalytic TiO$_2$ results in a loss in transmittance of around $4 - 8\,\%$ at each layer interface [39]. The presented approach
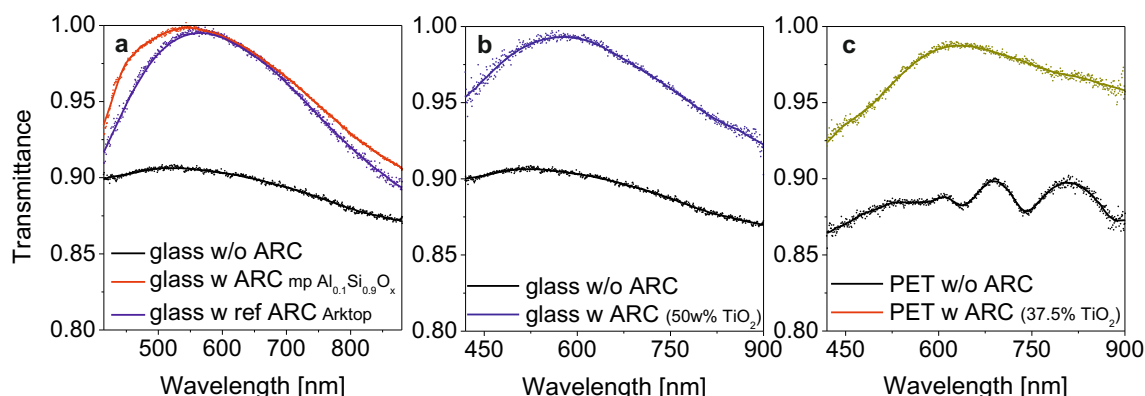
Figure 10.4: **Transmission characteristics of antireflective coatings. a)** Transmittance through an uncoated glass slide (black) in comparison to substrates coated with double-sided BCP-assembled mesoporous ARC (red) or double-sided commercial antireflective adhesive (blue, Arktop). **b)** Optical transmittance of a glass slide with double-sided ARCs, where $50\,wt\%$ aluminosilicate was replaced by high refractive index, photocatalytic TiO_2 nanocrystals. **c)** Optical properties of a PET substrate with and without double-sided coating of photocatalytic ARCs. All BCP-derived coatings were based on BCP-34.

therefore establishes a first practical route to antireflective coatings for PET substrates that are both photocatalytic and highly transmissive.

While the optical characterisation showed good uptake and sub-optical dispersion of TiO_2 in the aluminosilicate network, the actual position of the nanocrystals is crucial for the self-cleaning function. Cluster formation or the inclusion of the TiO_2 nanocrystals far from the network surface would be detrimental for their photocatalytic activity. Figure 10.5 shows the distribution of the TiO_2 nanocrystals, as observed by transmission electron microscopy (TEM). The TEM images of two different pore morphologies show $\sim 3-4$ nm-sized nanocrystals that
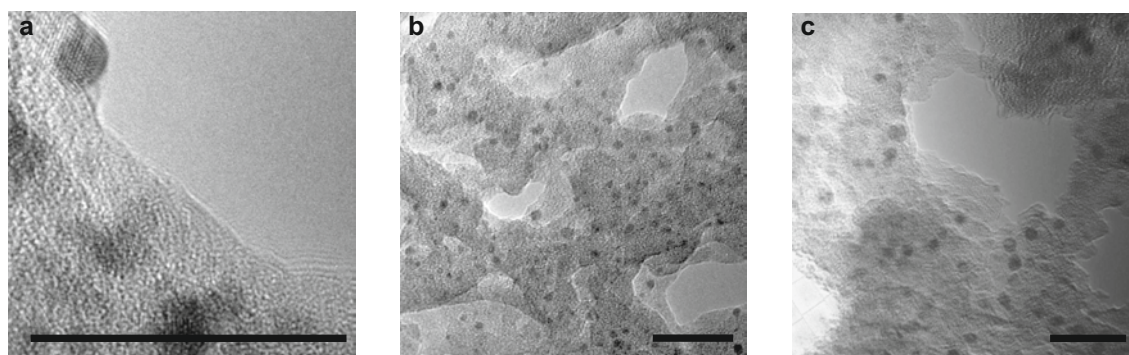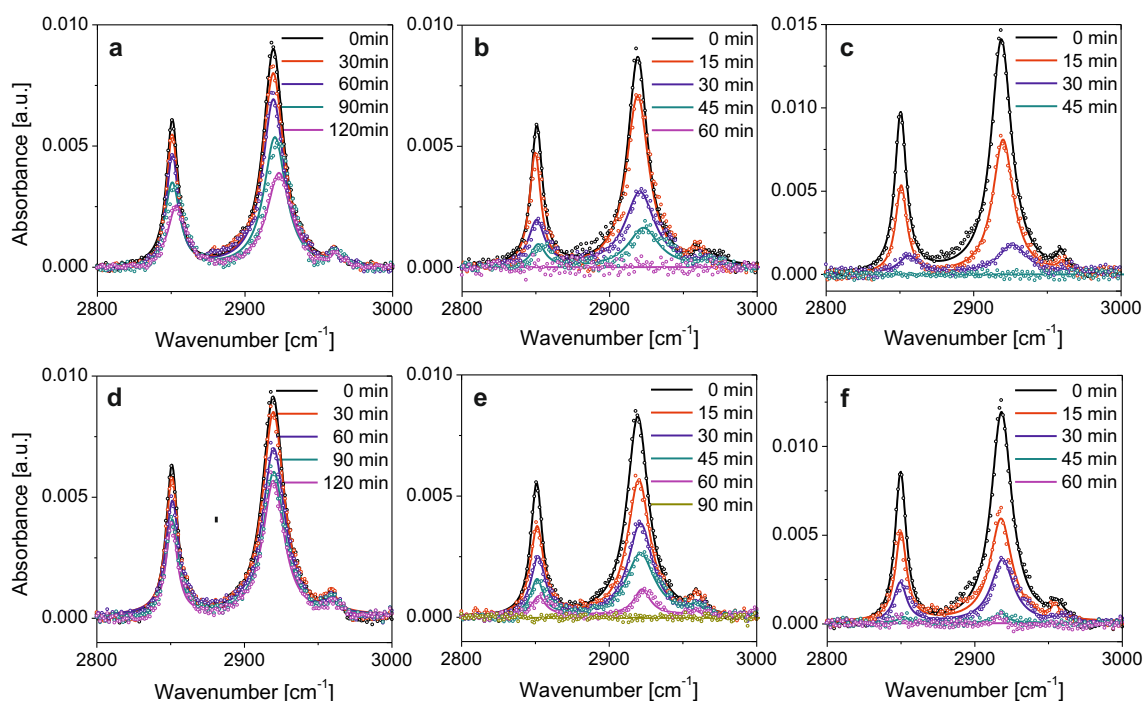

Figure 10.5: **Composition of self-cleaning ARCs.** Transmission electron micrographs showing the distribution of photocatalytic TiO_2 nanocrystals in the inorganic network. **a)** High magnification image of TiO_2 nanocrystals embedded in the silica-type matrix. Film morphology for **b)** BCP-34 and **c)** BCP-92 derived films. The scale bars represent $20\,nm$.

are well dispersed within the silica-based network. No TiO_2 aggregates were found. This is supported by wide angle x-ray diffraction results of dried TiO_2 powder after non-hydrolytic sol-gel synthesis, where a mean crystallite size of 3.5 ± 0.2 nm was determined by a Scherrer analysis of the [101] anatase peak [40].

The self-cleaning effect of photocatalytic TiO_2 surfaces is based on the absorption of ultraviolet light in the TiO_2. A small fraction of the generated charge carriers escapes rapid recombination and migrates to the TiO_2 surface. Electron vacancies cause the oxidation of adsorbed organic molecules, while electrons eventually combine with atmospheric oxygen to form superoxide radicals, which further degrade nearby organic molecules. This so-called "cold combustion" mechanism enables self-cleaning through the conversion organic pollutants to carbon dioxide, water and mineral acids [20]. The decomposition of stearic acid is often used as an organic marker molecule to monitor the photocatalytic performance of self-cleaning surfaces [20, 41, 42]. Stearic acid readily assembles in a homogeneous layer onto inorganic surfaces. Its decomposition can be monitored by Fourier transform infrared spectroscopy (FTIR). As TiO_2 only absorbs in the spectral range $\lambda < 375$ nm ($E_{gap} \sim 3.3$ eV [43]), it was of central importance to closely mimic the solar irradiation (AM 1.5) in the ultraviolet frequency range. This was achieved by a xenon lamp that was calibrated to match the intensity of ambient solar power in this spectral window.

Figure 10.6a-f shows the decomposition of stearic acid adsorbed onto ARCs for two different pore sizes (a-c: 33 nm; d-f: 53 nm), each with TiO_2 loadings of $25 - 50$ wt%. FTIR absorbance spectra were collected in transmission and baseline corrected. In the spectral range from $2800 - 3000$ cm^{-1} stearic acid shows three peaks: the asymmetric in-plane C-H methyl stretching results in absorbance at 2958 cm^{-1}, while the 2923 cm^{-1} and 2853 cm^{-1} peaks correspond to symmetric and asymmetric C-H stretching modes of CH_2, respectively [42]. An integrated absorbance of 0.52 cm^{-1}, 0.42 cm^{-1} and 0.35 cm^{-1} corresponds to a surface coverage of 30 %, 40 % and 130 % (i.e. 1.3 monolayers) for BCP-34 50 w% TiO_2, BCP-92 50 w% TiO_2 and the reference Pilkington sample, respectively. See supplementary information in reference [1] for further details. The integrated area under all three peaks, normalised to the value before irradiation, was used as a quantitative measure for the stearic acid stability on the surface of the ARC. While stearic acid decomposition for samples with 25 wt% TiO_2 loading was rather slow, samples with 37.5 wt% and 50 wt% TiO_2 showed a rapid decay in FTIR intensity. This is further evidenced in Figure 10.7, where the integrated area of stearic acid absorbance is plotted as a function of irradiation time. The intensity decrease for 37.5 wt% and 50 wt% TiO_2 loading can be fitted by a zeroth-order reaction rate. Samples derived from BCP-34 exhibited rate constants k of 0.36, 3.71 and 5.10×10^{13} molecules/min for 25.0 w%, 37.5 wt% and 50 wt% TiO_2 loading, respectively. Decomposition by ARCs with larger pores due to the assembly by

BCP-92 could be fitted with rate constants k of 0.36, 1.54 and 3.12 x 10^{13} molecules/min for 25.0 w%, 37.5 wt% and 50 wt% TiO_2 loading, respectively.

Figure 10.6: **Self-cleaning of optical coatings.** Decomposition of stearic acid as a function of time for different TiO_2 loadings and pore sizes of ARCs. **a) - c)** ARCs derived from BCP-34 with TiO_2 loadings of **a)** 25 wt%, **b)** 37.5 wt% and **c)** 50 wt%. The decay of the characteristic stearic acid absorption peaks at $\sim 2850\,nm^{-1}$ and $\sim 2920\,nm^{-1}$ was monitored by Fourier transform infrared spectroscopy in transmission. **d) - e)** similar data as in **a) - c)** for ARCs derived from BCP-92.
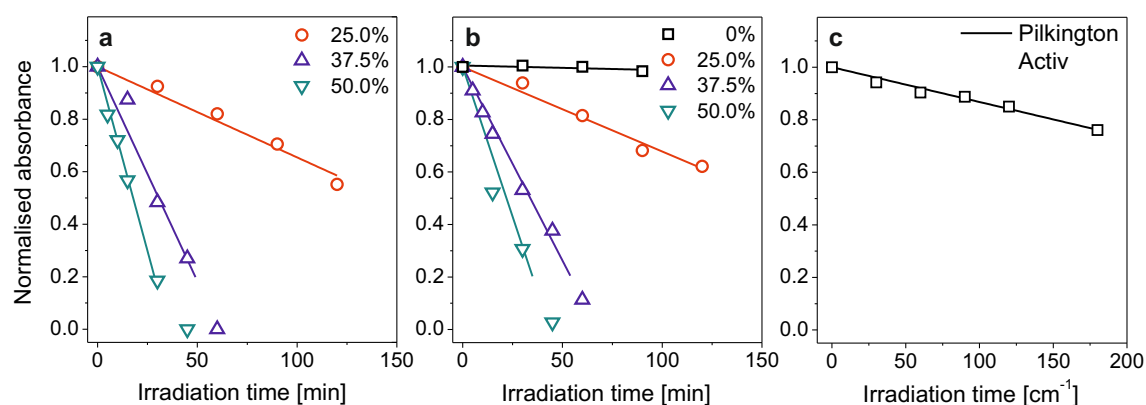
Figure 10.7: **Integrated peak area of stearic acid absorbance as a function of irradiation time.** The area enclosed by the three characteristic peaks of CH$_3$: 2958 cm^{-1}, CH$_2$: 2923 cm^{-1} and 2853 cm^{-1}, normalised to the initial value before irradiation, was used as a measure of stearic acid stability on the ARCs' surfaces. Peak area vs. time for **a)** BCP-34 (pore size $\sim$ 33 nm) and **b)** BCP-92 (pore size $\sim$ 53 nm) derived samples for different TiO$_2$ loadings. **c)** Decay of stearic acid peak area for a commercial reference (Pilkington Activ) which does not have antireflective properties.

Two clear trends could be observed. 1. Increased TiO_2 loading led to accelerated stearic acid decomposition in both sample series. 2. ARCs with smaller pores (d~ 33 nm) outperformed ARCs with larger pores (d~ 53 nm) for the higher TiO_2 content. This behaviour can be linked to the random distribution of TiO_2 nanocrystals in the silica-type matrix, shown in Figure 10.5. Both an increase in TiO_2 loading and a reduction in strut diameter leads to an increase in the number of nanocrystals that are located close to the strut surface and are therefore photocatalytically active. An overview of the photocatalytic decomposition rates is shown in Table 10.1

For reference, the stearic acid decomposition under solar irradiation was also monitored for ARC samples without TiO_2 inclusion. No decrease in FTIR absorbance could be observed after three hours of irradiation, indicating that the stearic acid decomposition solely arises from the photocatalytic activity of the incorporated TiO_2 nanocrystals (see supplementary information in reference [1]). Commercial self cleaning Pilkington glass , which is not anti-reflective, showed a much weaker photocatalytic degradation of stearic acid with a reaction rate k of ~ 0.13×10^{13} molecules/min. This result is somewhat surprising as the commercial glass is covered by a continuous, non-porous coating of TiO_2 that is optimised for self-cleaning without having to achieve a specific refractive index. The greatly decreased photocatalytic activity of Pilkington "Activ" compared to a thin film of TiO_2 nanoparticles has already been shown in earlier studies [42]. In addition, the presented route allows the incorporation of purely crystalline TiO_2, which is know for its superior photocatalytic activity compared to amorphous TiO_2 and mixed crystal phases [44]. While a difference in stearic coverage with 30 %, 40 % and 130 % (i.e. 1.3 monolayers) was observed for BCP-34, BCP-92 and the reference Pilkington sample, this should not be a decisive factor for the greatly enhanced decomposition in the BCP-derived samples. A zeroth-order decomosition observed in all samples indicates that sufficient "hydrocarbon fuel" was present on the surface throughout the self-cleaning process. A coverage below 100 % rather implies that only a fraction of the ARC's surface is actively decomposing.

Table 10.1: **Decomposition rates of self-cleaning samples.**

Sample name	TiO_2 content (w%)	slope	reaction rate (no. molecules x 10^{13}/ min)
BCP-34	50.0	-0.0280	4.71
BCP-34	37.5	-0.0239	2.53
BCP-34	25.0	-0.0035	0.37
BCP-92	50.0	-0.0228	3.32
BCP-92	37.5	-0.0147	1.54
BCP-92	25.0	-0.0032	0.36
Pilkington reference	n.a.	-0.0013	0.15

10.4 Conclusions

In this chapter a new concept for the fabrication of inorganic coatings that combine antireflective and photocatalytic properties is presented. The large volume fraction of the BCP's hydrophobic PI block enabled micellisation of the hybrid system under readily achieved non-equilibrium processing conditions. Upon spin coating, the sacrificial colloidal micelles self-assembled in a close-packed lattice. As the inorganic material resided in the hydrophilic outer layer of the micelles, it was co-assembled in an inverse-opal like geometry. Subsequent removal of the polymer yielded structurally stable and continuous inorganic films. Since the porosity arises from the close-packing of pores rather than high refractive index components, porosity values of up to 73 % were achieved. This enabled the substitution of up to 50 wt% aluminosilicate by high refractive index TiO_2 nanocrystals, while maintaining antireflective properties. As a result, the ARCs showed high performance in photocatalytic self-cleaning while exhibiting an excellent optical response. The high abrasion resistance of aluminosilicate films should further allow excellent durability of the coatings [45]. Low temperature processing enabled the deposition onto flexible plastic substrates. It should be straight-forward to extend the film deposition technique to roll-to-roll processing (i.e. slot-die coating or meniscus coating [36]), making this universal route highly attractive for the manufacture of next generation ARCs.

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Chapter 11

Conclusions

The aim of this thesis was to explore the use of soft matter design principles for improved functionality of inorganic nanoarchitectures. The self-assembly properties of sacrificial block copolymers (BCPs) and colloids were employed as the structure-defining motive for the co-assembly of inorganic materials. This allowed detailed control over film thickness, porosity, pore dimensions and accessibility as well as crystal growth of the resulting inorganic material structures, all of which are decisive attributes for the performance of photonic and optoelectronic devices.

Implementation of the proposed materials architectures in dye-sensitised solar cells (DSCs) yielded promising results. BCP-derived TiO_2 networks offer superior controllability over pore size distribution and charge transport properties. It proved, however, difficult to outperform the long optimised conventional photoanodes in terms of overall device efficiency. This was recently accomplished with a terblock copolymer PI-*b*-PS-*b*-PEO directed TiO_2 photoelectrode, which improved the overall device efficiency of solid-state DSCs compared to the state-of-the-art nanoparticle system [1]. The fundamental understanding of structure formation in thin films (Chapter 5), crystal growth (Chapter 6) and thick film deposition (Chapter 7) should enable further improvement and hopefully foster the viability of this concept for future devices. Especially with the rise of one-electron-based, bulky redox-couples, such as cobalt-based electrolytes [2], the advantages of BCP-derived photoelectrodes should have a positive impact on further efficiency improvements.

The findings presented in Chapter 6 on superior electronic properties of BCP-assembled photoanodes are certainly only a first step in the right direction. Combining the presented concept with hard scaffolding, i.e. the coating of a sacrificial and temperature stable inorganic layer, could be a viable concept to combine high surface area and outstanding charge carrier transport properties [3]. The use of hierarchical photoanode structures by the combination of

different structure-directing agents [4, 5] as well as surface passivation by using a core-shell strategies [6, 7, 8] are emerging concepts that are compatible with this work. So far, only thermally-driven crystal growth was explored, but soft matter self-assembly should also be capable to guide the growth of inorganic material by oriented attachment at low temperatures in solution [9, 10, 11]. Other directions for future research directions include the integration of a three-dimensionally structured transparent conductive electrode for radial electron collection, where aspects presented in this work should make further impact [12, 13, 14].

The work on photonic crystal-based optical elements has been well received and a large number of similar studies have recently emerged. In close relation to the work presented in Chapter 9, advances in the fabrication of thick BCP-assembled films (Chapter 7, [15]) and further development in the fabrication of defect free photonic crystals [16, 17] should lead to overall device improvements. The one-dimensional mesoporous Bragg reflectors (MDBRs) presented in Chapter 8 are ideally suited for the use in DSCs and represent a promising platform to further investigate the effect of complementary photonic elements for overall device efficiency improvements. The advantages of pore size and pore dimensions tunability of BCP-derived MDBRs have not been yet been fully exploited and should foster next-generation devices with improved functionality for sensing, light-emission and coupled device systems [18, 19]. Another field that benefits from the complementary use of 1D and 3D photonic crystals is photocatalytic water splitting [20, 21].

In Chapter 5 the possible application of gyroid-like aluminosilica networks as electrodes in lithium ion batteries was discussed. Reduction of the presented aluminosilica films in magnesium vapor is one route to access a continuous silicon network on the $20 - 40$ nm length scale. Due to the strain associated with the volume change during charging and discharging cycle, networks on the 10 nm length scale suffer from structural collapse, whereas coarser colloidal templated structures do not exhibit the necessary interfacial area to allow fast lithium insertion [22, 23, 24]. The use of large molecular weight BCPs as structure-directing agents on a somewhat intermediate length scale is therefore an ideal candidate for further device improvement.

The author hopes to have communicated some inspiring possibilities that soft matter self-assembly offers for designing tomorrow's materials. When appropriately utilised, these materials represent a unique toolbox for further development of inorganic materials and devices. Thank you for your interest.

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09/1992 - 06/2001	**Bildungszentrum Markdorf - university qualification** Main subjects: mathematics and politics Best student in district with an average grade of 1.0 on a 1-6 scale

HONORS AND AWARDS

12/2012	**Postdoctoral Fellowship of the German Academy of Sciences - Leopoldina** Early career fellowship for outstanding postdoctoral scientists to develop their own independent research.
11/2012	**Springer Outstanding Thesis Award** Publication award by Springer for outstanding PhD research.

11/2010	**NanoDTC Asssociate Student Grant** Travel grant for outstanding doctoral candidates to promote cross-disciplinary research within the center themes of self-assembling functional nano-materials and devices.
06/2009	**EMRS Young Scientist Award** In recognition of the outstanding paper contributed to the 2009 spring meeting of the European Materials Research Society.
06/2007	**Hölderlin Scholarship** Stipend for a research year abroad funded by the Studienstiftung des deutschen Volkes and Siemens.
04/2004 - 09/2008	**Fellow of the "Studienstiftung des deutschen Volkes"** Program of the German government to support highly talented and socially committed students (top 0.5 %, enabling fully funded undergraduate studies).
03/1999	**Markdorfer Wirtschaftspreis** Scholarship for a 3 month stay at Columbus East High School, Indiana/USA (regional award for highly talented students).

WORK EXPERIENCE

since 09/2012	**École Polytechnique Fédérale de Lausanne**, Lausanne, CH Experimental research in the field of nanoparticles and soft matter self-assembly.
08/2007 - 08/2012	**University of Cambridge**, Cambridge, UK Experimental research in the field of soft matter physics and functional materials. See below for details on acquired scientific skills.
06/2009 - 08/2009	**Cornell University**, Ithaca, NY, USA Scientific stay in the group of Prof. Ulrich Wiesner. Work focus on materials chemistry, electron microscopy and small angle x-ray scattering.
03/2007 - 04/2007	**Science resort of the Bavarian Broadcasting Corp.**, Munich, GER Independent production of a 4 min documentary about energy saving lamps in the program NANO (200,000 viewers).

01/2006 - 06/2007	**Bosch and Siemens Home Appliances**, Munich, GER
	Part time position initially on the thermoacoustics of a plant oil cooker. In 2007 development of a financial concept under the Kyoto clean development mechanism to stimulate the distribution of a plant oil cooker in developing countries.
10/2004 - 02/2005	**Industrial Research ltd.**, Christchurch, NZ
	Internship on the development of a heat exchanger for a fuel cell device.
08/2001 - 05/2002	**Civilian service** Kiel, GER
	Care and nursing of disabled adults.
since 07/1997	**Boarder's point by Sport Guldin**, Markdorf, GER
	Management of the self-founded snowboard department "Boarder's point" in the sport store owned by my parents. Organization of non-commercial ski- and snowboard excursions for young people with currently 4,000 participants per year (since 2001 in consulting function).

TEACHING

2009 - 2011	**Supervisor "Introduction to Experimental and Theoretical Physics"**, 1st year physics, Physics Department, University of Cambridge, UK
2010	**Supervisor "Soft matter & Biophysics"**, 4th year physics, Physics Department, University of Cambridge, UK
2009	**Research co-supervisor "Plasmonic Enhancement of Dye-Sensitized Solar Cells"**, physics 4th year project, Tjonnie G.F. Li, University of Cambridge, UK
2009	**Lab demonstrator "Systems & Measurements"**, 2nd year physics, Physics Department, University of Cambridge, UK
2008	**Lab demonstrator "Waves & Optics"**, 2nd year physics, Physics Department, University of Cambridge, UK

SCIENTIFIC SKILLS

Material Fabrication	Atomic layer deposition[B], block copolymer templating[A], colloidal templating[A], chemical vapor deposition[B], reactive ion etching[A], sol-gel chemistry[A], solution processing[A]
Microscopy	Confocal microscopy[B], scanning electron microscopy[A], transmission electron microscopy[B]
Scattering	Dynamic light scattering[A], small-angle X-ray scattering[B], wide-angle X-ray scattering[A]
Other Techniques	Atomic force microscopy[B], ellipsometry[A], micro-spectroscopy[A], nitrogen physisorption[B], photovoltaic device characterization[A], thermogravimetric analysis[B], uv-vis spectroscopy[B], FT-IR spectroscopy[B]
Computing	Adobe Photoshop[A], CorelDraw[A], LaTeX[A], Matlab[B], Microsoft Office[A], Origin[A]
Languages	German (mother language), English (fluent), French[A], Spanish[A]

[A] advanced, [B] basic

OTHER SCIENTIFIC ACTIVITIES

Organiser of	Main conference organiser of the "Soft Nanophotonics Winterschool" in 2009, 2010 and 2011 (University of Cambridge, 40-60 participants per year)
Reviewer for	ACS Applied Materials & Interfaces, ChemSusChem, Electrochemistry Communications, Energy & Environmental Science, Journal of the American Chemical Society, Journal of Physics D: Applied Physics, Langmuir, Nanotechnology

PATENTS

Pending	*Self-cleaning antireflective optical coatings* - **S. Guldin**, U. Steiner, UK patent application 1212361.8, 11/07/2012.

PUBLICATIONS (ResearcherID A-7209-2011)

[19] *Ordered mesoporous titania from highly amphiphilic block copolymers: tuned solution conditions enable morphology control* - M. Stefik, J. Song, H. Sai, M.C. Orilall, **S. Guldin**, P. Boldrighini, U. Steiner, Sol M. Gruner, U. Wiesner, in preparation.

[18] *Novel Fabrication Method of Gyroid and Worm-like ZnO Mesoporous Structures for Photovoltaic Applications* - E. Kim, Y. Vaynzof, **S. Guldin**, U. Steiner, in preparation.

[17] *Effect of DIO solvent additive on the stability of PTB7:PCBM solar cells* - P.E. Hopkinson, B. Schmidt-Hansberg, **S. Guldin**, N. Greenham, in preparation.

[16] *Crystal nucleation and growth in mesoporous TiO_2* - P. Kohn, **S. Guldin**, U. Wiesner, U. Steiner, in preparation.

[15] *Transport limitations in self-assembled photoanodes for solid-state dye-sensitized solar cells* - P. Docampo, **S. Guldin**, U. Steiner, H.J. Snaith, under review.

[14] *Self-cleaning antireflective optical coatings* - **S. Guldin**, P. Kohn, M. Stefik, J. Song, G. Divitini, C. Ducati, U. Wiesner, U. Steiner, under formal review at Nature Communications.

[13] *Pore-filling of spiro-OMeTAD in solid-state DSCs determined via optical reflectometry* - P. Docampo, A. Hey, **S. Guldin**, R. Gunning, U. Steiner, H.J. Snaith, Advanced Functional Materials, vol. 22, pp. 5010-5019, 2012.

[12] *Biomimetic Layer-by-Layer Assembly of Artificial Nacre* - A. Finnemore, P.S. Cunha, T. Shean, S. Vignolini, **S. Guldin**, M. Oyen, U. Steiner, Nature Communications, vol. 3, art no. 966, DOI: 10.1038/ ncomms1970, 2012.

[11] *Triblock terpolymer directed self-assembly of mesoporous TiO_2* - high performance photoanodes for solid state dye-sensitised solar cells - P. Docampo, M. Stefik, **S. Guldin**, N.A. Yufa, R. Gunning, U. Wiesner, U. Steiner, H.J. Snaith, Advanced Energy Materials, vol. 2, pp. 676-682, 2012.

[10] *A 3D optical metamaterial made by chiral self-assembly* - S. Vignolini, N.A. Yufa, P.S. Cunha, **S. Guldin**, I. Rushkin, M. Stefik, K. Hur, U. Wiesner, J.J. Baumberg, U. Steiner, Advanced Materials, vol. 24, pp. OP23-OP27, 2012.

[09] *Layer-by-layer formation of block copolymer derived TiO_2 for solid state dye-sensitised solar cells* - **S. Guldin**, P. Docampo, M. Stefik, G. Kamita, U. Wiesner, H.J. Snaith, U. Steiner, Small, vol. 8, pp. 432-440, 2012.

[08]   *Mesoporous Bragg reflectors - block-copolymer self-assembly leads to building blocks with well defined continuous pores and high control over optical properties*, **S. Guldin**, M. Kolle, M. Stefik, U. Wiesner, U. Steiner, Proceedings of the SPIE, vol. 8095, DOI: 10.1117/12.893818, 2011.

[07]   *Self-assembly as a design tool for the integration of photonic structures into excitonic solar cells*, **S. Guldin**, P. Docampo, S. Hüttner, P.Kohn, M. Stefik, H.J. Snaith, U. Wiesner, U. Steiner, Proceedings of the SPIE, vol. 8111, DOI: 10.1117/12.893798, 2011.

[06]   *Tunable mesoporous TiO_2 Bragg reflectors based on block-copolymer self-assembly* - **S. Guldin**, M. Kolle, M. Stefik, R. Langford, U. Wiesner, U. Steiner, Advanced Materials, vol. 23, no. 32, pp. 3664-3668, 2011.

[05]   *Improved conductivity in dye-sensitized solar cells through block-copolymer confined TiO_2 crystallization* - **S. Guldin**, S. Hüttner, P. Tiwana, M.C. Orilall, B. Ülgüt, M. Stefik, P. Docampo, M. Kolle, G. Divitini, C. Ducati, S.A.T. Redfern, H.J. Snaith, U. Wiesner, D. Eder, U. Steiner, Energy and Environmental Science, vol. 4, no. 1, pp. 225-233, 2011.

[04]   *Dye-sensitized solar cell based on a 3D photonic crystal* - **S. Guldin**, S. Hüttner, M. Kolle, M. Welland, P. Müller-Buschbaum, R. Friend, U. Steiner, N. Tetreault, Nano Letters, vol. 10, no. 7, pp. 2303-2309, 2010.

[03]   *Control of solid-state dye-sensitized solar cell performance by block copolymer directed TiO_2 synthesis* - P. Docampo[*], **S. Guldin**[*], M. Stefik, P. Tiwana, M.C. Orilall, S. Hüttner, H. Sai, U. Wiesner, U. Steiner, H.J. Snaith, Advanced Functional Materials, vol. 11, no. 20, pp. 1787-1796, 2010.

[02]   *Monolithic route to efficient dye-sensitized solar cells employing diblock copolymers for mesoporous TiO_2* - M. Nedelcu[*], **S. Guldin**[*], M.C. Orilall, J. Lee, S. Hüttner, E.J.W. Crossland, S.C. Warren, C. Ducati, P.R. Laity, D. Eder, U. Wiesner, U. Steiner, H.J. Snaith, Journal of Materials Chemistry, vol. 7, no. 20, pp. 1261-1268, 2010.

[01]   *Block-copolymer directed synthesis of mesoporous TiO_2 for dye-sensitized solar cells* - M. Nedelcu, J. Lee, E.J.W. Crossland , S.C. Warren, M.C. Orilall, **S. Guldin**, S. Hüttner, C. Ducati, D. Eder, U. Wiesner, U. Steiner, H.J. Snaith, Soft Matter, vol. 1, no. 5, pp. 134-139, 2009.

[*] authors contributed equally to this work.

TALKS AND CONFERENCE PARTICIPATION

27 oral and poster contributions in seminars, workshops and conferences, including:

[01] *Mesoporous Bragg reflectors - block-copolymer self-assembly leads to building blocks with well defined continuous pores and high control over optical properties*, talk, SPIE Optics & Photonics, August 2011, San Diego, USA.

[02] *Tunable mesoporous Bragg reflectors based on block-copolymer self-assembly*, conference poster prize, 5th International Conference on Nanophotonics, May 2011, Shanghai, China.

[03] *Photonic sensing with tunable mesoporous Bragg reflectors based on block-copolymer self-assembly*, talk in invited session on bioinspired Nanophotonics, Conference of the European Materials Research Society, May 2011, Nice, France.

[04] *Self-assembly as a design tool for the integration of photonic structures into excitonic solar cells*, invited talk, Symposium on Nanophotonics and Renewable Energy, Chinese Academy of Sciences, January 2011, Beijing, China.

[05] *Catching the light - self-assembled TiO_2 nanostructures in a double layer dye-sensitized solar cell*, conference poster prize, Conference on self-assembly and self-organization at surfaces and interfaces, EU Patterns network, December 2008, Selwyn College, Cambridge, UK.

REFEREES

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