



# Fluid-Rock Interactions in a Carbon Storage Site Analogue, Green River, Utah

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## Declaration

Except where indicated, this thesis describes my own work and contains nothing which is the outcome of work done in collaboration with others. No part of this dissertation is substantially the same as any work that has been, or will be submitted for any other qualification at any other University. The number of pages is within the prescribed limit.

> NIKO KAMPMAN January 2011

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Reactions between  $CO_2$ -charged brines and reservoir minerals might either enhance the long-term storage of  $CO_2$  in geological reservoirs or facilitate leakage by corroding cap rocks and fault seals. Modelling the progress of such reactions is frustrated by uncertainties in the absolute mineral surface reaction rates and the significance of other rate limiting steps in natural systems. This study uses the chemical evolution of groundwater from the Jurassic Navajo Sandstone, part of a leaking natural accumulation of  $CO_2$  at Green River, Utah, in the Colorado Plateau, USA, to place constraints on the rates and potential controlling mechanisms of the mineral-fluid reactions, under elevated  $CO_2$  pressures, in a natural system.

The progress of individual reactions, inferred from changes in groundwater chemistry is modelled using mass balance techniques. The mineral reactions are close to stoichiometric with plagioclase and K-feldspar dissolution largely balanced by precipitation of clay minerals and carbonate. Mineral modes, in conjunction with published surface area measurements and flow rates estimated from hydraulic head measurements, are then used to quantify the kinetics of feldspar dissolution. Maximum estimated dissolution rates for plagioclase and K-feldspar are  $2x10^{-14}$  and  $4x10^{-16}$  mol·m<sup>-2</sup>·s<sup>-1</sup>, respectively. Fluid ion-activity products are close to equilibrium (e.g.  $\Delta G_r$  for plagioclase between -2 and -10 kJ/mol) and lie in the region in which mineral surface reaction rates show a strong dependence on  $\Delta G_r$ . Local variation in  $\Delta G_r$  is attributed to the injection and disassociation of  $CO_2$  which initially depresses silicate mineral saturation in the fluid, promoting feldspar dissolution. With progressive flow through the aquifer, feldspar hydrolysis reactions consume H<sup>+</sup> and liberate solutes to solution which increase mineral saturation in the fluid and rates slow as a consequence. The measured plagioclase dissolution rates at low  $\Delta G_r$  would be compatible with far-from-equilibrium rates of  $\sim 1 \times 10^{-13}$  mol·m<sup>-2</sup>·s<sup>-1</sup> as observed in some experimental studies. This suggests that the discrepancy between field and laboratory reaction rates may in part be explained by the differences in the thermodynamic state of natural and experimental fluids, with field-scale reactions occurring close to equilibrium whereas most laboratory experiments are run far-from-equilibrium.

Surface carbonate deposits and cementation within the footwall of the local fault systems record multiple injections of CO<sub>2</sub> into the Navajo Aquifer and leakage of CO<sub>2</sub> from the site over ca. 400,000 years. The  $\delta^{18}$ O,  $\delta^{13}$ C and  ${}^{87}$ Sr/ ${}^{86}$ Sr of these deposits record rapid rates of CO<sub>2</sub> leakage (up to ~1000 tonnes/a) following injection of CO<sub>2</sub>, but rates differ by an order of magnitude between each fault, due to differences in the fault architecture. Elevated  $pCO_2$  enhances rates of feldspar dissolution in the host aquifer and carbonate precipitation in fracture conduits. Silicate mineral dissolution rates decline and carbonate precipitation rates increase as pH and the  $CO_2$ charge dissipate. The Sr/Ca of calcite cements record average precipitation rates of  $\sim 2x10^{-6}$ mol/m<sup>2</sup>/s, comparable to laboratory derived calcite precipitation rates in fluids with elevated Mn/Ca and Fe/Ca, at  $\Omega_{cc}$  of ~1 to 3. This suggests that far-from-equilibrium carbonate precipitation, which blocks fracture conduits and causes the leaking system to self-seal, driven by CO<sub>2</sub> degassing in the shallow subsurface, can be accurately modeled with laboratory derived rates. Sandstones altered in CO<sub>2</sub> leakage conduits exhibit extensive dissolution of hematite grain coatings and are chemically bleached as a result. Measurements of Eh-pH conditions in the modern fluid, and modeling of paleo-Eh-pH conditions using calcite Fe and Mn concentrations, suggests that the CO<sub>2</sub>-charged groundwaters are reducing, due to their low dissolved O<sub>2</sub> content and that pH suppression due to high  $pCO_2$  is capable of dissolving and transporting large concentrations of metals. Exhumed paleo-CO2 reservoirs along the crest of the Green River anticline have been identified using volatile hosting fluid inclusions. Paleo-CO<sub>2</sub>-charged fluids mobilized hydrocarbons and CH<sub>4</sub> from deeper formations, enhancing the reductive dissolution of hematite, which produced spectacular km-scale bleached patterns in these sediment.

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## Chapter 1

## Introduction

## 1.1. Global Warming

Climate change is one of the primary environmental concerns of the  $21^{st}$  century. Over the past century, atmospheric carbon dioxide (CO<sub>2</sub>) concentrations have steadily increased, having now risen to over 387 ppm from the pre-industrial level of 280 ppm and are expected to continue rising at 2 ppm annually (IPCC, 2007). Increases in CO<sub>2</sub> concentrations are attributed predominantly to the burning of oil, gas and coal for electrical generation, transportation, industrial and domestic uses, with deforestation and cement production making significant contributions.

Interpretation of the temperature record on a scale of centuries to millennia indicates a slight increase in global average annual temperatures in the last 150 years, in the order of  $0.76 \,^{\circ}\text{C}$ (IPCC, 2007), and predictions are that, if emissions growth continues unabated, a warming of 1.1 to 6.3 °C will be observed by the end of this century (IPCC, 2007). It is very likely and generally accepted that the main cause of the observed global warming is the increase in atmospheric concentrations of greenhouse gases, primarily carbon dioxide (CO<sub>2</sub>), methane (CH<sub>4</sub>) and nitrous oxide  $(N_2O)$  (IPCC, 2007). Although a direct causal link between the rise in greenhouse gas concentrations in the atmosphere and global warming has not been demonstrated, significant circumstantial evidence points toward this link, which has been generally accepted by a broad segment of the scientific community (e.g. IPCC, 2007; AGU, 2003). And in agreement, increasing empirical evidence points to a causal relationship between elevated concentrations of green house gases in the atmosphere and changes in the radiative heat forcing, global surface temperatures and atmospheric  $pCO_2$  within the recent geological past (e.g. Crowley *et al.*, 2003; Indermuhle et al., 1999; Keeling and Whorf, 2005; Petit et al., 1999; Tripati et al., 2009). The detailed response of the highly nonlinear climate system to increasing CO<sub>2</sub> concentration in the atmosphere, and to the resulting increased heat load, is uncertain because of the inherent complexity of the climate system and natural variability; however, the close coupling between the carbon cycle, including  $CO_2$  and  $CH_4$ , and palaeo-climate suggests that changes in the former will be accompanied by changes in the latter (AGU, 1999).

#### 1.1.1. Global Warming Mitigation

Scientific consensus on global warming and the fear of abrupt climate change (IPCC, 2007; Schneider, 2004) is leading to increased efforts to develop new technologies and sciences in an attempt to mitigate global warming. Such climate change mitigation strategies include reducing demand for emissions-intensive goods and services, increasing efficiency gains, increasing use and development of low-carbon technologies, and reducing fossil fuel emissions (Parry et al., 2007). A reduction in the release rate of  $CO_2$  to the atmosphere is considered an essential first step in the control of global warming. It is widely agreed that for a rapid reduction in global  $CO_2$ emissions to be successful a spectrum of new technologies and energy policies is required. Principally this will involve an increase in the utilization of non-fossil fuel based energy sources such as solar, wind, wave, nuclear and geothermal power and the sequestration of gas emissions from existing and future fossil or bio-fuel based power stations. Given predictions that a significant fraction of global energy production will continue to be generated from bio- or fossil fuels, CO<sub>2</sub> emissions will continue into the next century (Coyle, 2009; Faiman et al., 2007; Shafiee and Topal, 2008). Thus a safe and secure method of sequestering  $CO_2$  out with the atmospheric system is being sought. Carbon sequestration can take many forms, including the direct sequestration of  $CO_2$  from the atmosphere through enhancement of surface silicate weathering, stimulation of surface ocean productivity, reforestation, physical sequestration of  $CO_2$  in the deep ocean and in geological environments, as well as mineral carbonation on exhumed or in-situ geological strata. Among these CO<sub>2</sub> capture and geological storage, which entails CO<sub>2</sub> capture from large industrial processes and injection into deep geological formations, plays an important role (IEA, 2005, 2006).

### **1.2.** Carbon Capture and Storage

The capture of  $CO_2$  from large anthropogenic point sources and storage in geological formations including depleted oil and gas reservoirs, coal beds and aquifers has received increasing scientific attention as a safe and long-term storage option (Gale, 2004; Holloway *et al.*, 2005). Geological storage can in addition be used in combination with enhanced oil or gas exploitation ( $CO_2$ -EOR) (e.g. Damen *et al.*, 2005). Whilst no immediate technological barriers inhibit the implementation of carbon capture and storage, uncertainty in our understanding of aspects of the physical and chemical impacts of long-term storage of  $CO_2$  in the subsurface undermines our ability to satisfy operational, regulatory and public acceptance criteria (Rudnicki and Wawersik, 1999). Globally distributed saline aquifers represent the largest single reservoir type for geological storage of anthropogenic  $CO_2$  (Bachu *et al.*, 2005; Saylor and Zerai, 2004). The feasibility of storing  $CO_2$  in aquifers has been thoroughly discussed in the literature and continues to be debated. These studies include an evaluation of the feasibility of  $CO_2$  aquifer storage (summarized in Cook, 2006; Gale, 2004; Bachu, 2008). Recently, extensive experimental, field, and modeling studies of geological carbon storage have been conducted (Gaus, 2009; Gaus et al., 2005; Giammar et al., 2005; Gunter et al., 1997; Holloway et al., 2007; Horita., 2002; Hovorka, et al, 2006, 2005; Johnson et al., 2001; Jones et al., 2006; Kaszuba, et al., 2003, 2005; Knauss et al., 2002; McPherson and Lichtner, 2001; Oelkers et al., 2005, 2008; Palandri and Kharaka, 2002, 2005; Pearce et al., 2006; Pruess et al., 2003; Rochelle et al., 1999; Rosenbauer, and Koksalan, 2002; Soong, et al., 2004; Strazisar and Zhu, 2002; White et al., 2001; Xu et al., 2004, 2005, 2007). Whilst the engineered aspects of geological storage have been successfully demonstrated through a small number of commercial scale CO<sub>2</sub>-injection projects including Sleipner, Norwegian North Sea (Korbol and Kaddour, 1995); Snøhvit; Norway (Maldal and Tappel, 2004) and In Salah, Algeria (Rutqvist et al., 2009); and an increasing number of small-scale experimental projects including Ketzin, Germany (Schilling et al., 2009); Nagaoka, Japan (Kikuta et al., 2004); Frio, USA (Hovorka et al., 2006; Kharaka et al., 2006a, 2006b) and large-scale CO<sub>2</sub>-EOR projects at Weyburn, Canada (Emberley et al., 2004, 2005; Wilson and Monea, 2004) and Otway, Australia. A comprehensive summary of geological carbon storage is given by Bickle, (2009).

### **1.2.1.** CO<sub>2</sub> Storage Integrity

Carbon dioxide injected into saline aquifers below ~ 800 m water-depth will form a supercritical phase. The critical pressure and temperature of  $CO_2$  are 7.4 MPa and 31.1°C, corresponding to a critical density of 0.468 g/cm<sup>3</sup> (Leitner, 2000). This is equivalent to reservoir depths of ca 800-1500 m depending on local land surface temperature, heat flow and lithology. Supercritical  $CO_2$  combines gas- (e.g. low viscosity, typically around  $10^{-4}$  to  $10^{-3}$  Pa·s for supercritical gases), and liquid- (e.g. high density, relative to gas) properties. A supercritical fluid is liable to very large changes of density, especially close to the critical point.

Carbon dioxide is retained in geologic formations in four ways. First,  $CO_2$  can be trapped as a gas or supercritical fluid under a low-permeability caprock. The safety of the injected  $CO_2$  on a short timescale is related to buoyancy-driven flow of the immiscible part of the injected  $CO_2$ and the trapping capabilities of the formation. Second,  $CO_2$  can become physically trapped within the reservoir pore space via residual or capillary trapping owing to surface tension phenomena in multiphase systems (e.g. Suekane *et al.*, 2008; Taku Ide *et al.*, 2007). Third,  $CO_2$  can dissolve into the groundwater, becoming trapped as a soluble phase. The dissolution of  $CO_2$  in groundwater increases the acidity of water and affects the solubilities of minerals composing the host rock matrix. Fourth,  $CO_2$  can react directly or indirectly with minerals and organic matter in the geologic formation leading to the precipitation of secondary carbonates and the solubilization of organic matter. The former process, so-called 'mineral trapping', is potentially attractive because it could immobilize  $CO_2$  for long time-scales, and prevent its easy return to the atmosphere. The interaction of  $CO_2$  with alkaline aluminosilicate minerals will also result in the formation of soluble carbonates and bicarbonates in solution, thereby enhancing "solubility trapping".

The long-term containment of  $CO_2$  in the subsurface will depend on the performance of the materials sealing the host formation. Acceptable performance will need to be demonstrated in order to satisfy operational, regulatory and public acceptance criteria (Friedmann *et al.*, 2007). Some of the  $CO_2$  injected into geological reservoirs is expected to dissolve relatively rapidly into formation waters and the resulting acidic solution will undergo geochemical reactions with host reservoir minerals and the reservoir seal which will ultimately control the long term containment and integrity of the stored  $CO_2$ . These reactions may either stabilise the  $CO_2$  or enhance leakage. The nature and kinetics of the geochemical interactions between  $CO_2$ , formation fluids, carbonate and silicate minerals in the reservoirs and their clay-rich caprocks are inadequately known (Gale, 2004).

Short term leakage from geological storage sites (see Oldenburg, (2007) for a complete summary) will involve process related to the buoyant migration of free phase  $CO_2$  laterally and vertically within the subsurface and may lead to introduction of  $CO_2$  into shallow potable aquifers (e.g. Nicot, 2008; Wang and Jaffe, 2004) and surface leakage (e.g. Beaubien *et al.*, 2004).  $CO_2$  leakage within the wellbore, via the cement casing and through existing wells is also of concern (e.g. Preuss, 2004; Nordbotten *et al.*, 2005). Additionally, the leakage of  $CO_2$  from its host reservoir on longer timescales may be facilitated by migration through the caprock (Fleury *et al.*, 2009; Gherardi *et al.*, 2007; Li *et al.*, 2005; Morris *et al.*, 2009) and via fracture networks and through the reactivation of local faults (Barnes *et al.*, 1978; Irwin and Barnes, 1975; Kennedy *et al.*, 1997; Pruess, 2005) under conditions of over-pressuring (e.g. Lewicki *et al.*, 2007). The surface leakage of  $CO_2$  has a range of environmental (see Oldenburg and Unger, 2003) and economic impacts (see Zwaan and Gerlagh, 2009), a comprehensive summary is given by Bachu (2008).

#### **1.2.2.** Modeling Long-term Storage Integrity: Insights at the Field-Scale

Understanding the geochemical behaviour of anthropogenic carbon dioxide stored in geological reservoirs, over a range of time-scales, is crucial for quantifying the risk of leakage and the evolution of the sequestered form of that  $CO_2$  through the life of an individual storage site. The relatively low temperatures expected in typical storage sites imply rate-controlled systems that deviate from thermodynamic equilibrium (e.g. Lasaga, 1998; Lasaga and Luttge, 2004; Stumm and Morgan, 1996). Prediction of the long-term fate of this carbon dioxide requires determination of the relevant gas-fluid-mineral reactions and their chemical kinetics (e.g. Xu *et al.*, 2004).



**Figure 1.2-1** Reaction schemes showing the serial and parallel reactions occurring during the dissolution of anorthite. The protons formed by the  $CO_2$ -dissolution branch (blue) will hydrolyse the plagioclase, resulting in the release of  $Ca^{2+}$  ions. The calcium and bicarbonate or carbonate ions form the parallel branches (red) will together result in the precipitation of calcite. For a complete discussion see Chapter 2.

These gas-fluid-mineral reactions may act either to increase the stability of stored  $CO_2$  by precipitating carbonate minerals or enhance leakage by corroding well cements, existing boreholes, cap rocks and fault seals. Solubilisation of heavy metal bearing minerals in shallow groundwater systems is also of concern for the contamination of potable water sources (e.g. Wang and Jaffe, 2004). In addition, changes to the reservoir porosity and permeability structure, through clay and carbonate mineral precipitation, may alter injectivity and flow within the reservoir.

The main gas-fluid-mineral reactions that will occur as a result of  $CO_2$  injection can be summarised by a number of serial and parallel reactions, as shown in Fig. 1.2-1. The rate-limiting step in such serial-parallel reaction sequences will in general be the slowest step of the fastest parallel branch. Amongst the above reactions, it is well established that the silicate dissolution reactions are likely to be the slowest and hence most important in controlling reaction progress (e.g. Sorai *et al.*, 2005). The accurate modelling of  $CO_2$ -fluid-mineral reactions therefore requires a robust knowledge of the dissolution kinetics as well as the solubilities of silicate and aluminosilicate minerals.

Experimentally determined reaction rates and reaction product pathways have to-date been the major source of data used to constrain simulation of multicomponent, multiphase  $CO_2$ -fluid-rock systems (Gunter, 1996; Knauss *et al.*, 2001; Johnson *et al.*, 2001; Johnson and Nitao, 2003, Xu *et al.*, 2004, 2005, 2007). However, significant discrepancies have been found between the mineralogical products and reaction kinetics of natural and experimental systems (Brantley *et al.*, 1993, 2007; Kim, 2002; Malmstrom *et al.*, 2000; Taylor and Blum, 1995, 2000; White *et al.*, 1996; White and Brantley, 2003).



**Figure 1.2-2** A compilation of field and laboratory dissolution rates for plagioclase plotted against the duration of the 'experiment'. Significantly the natural dissolution rates are up to 5 orders of magnitude slower than, far-from-equilibrium, laboratory-derived rates at similar pH and temperature conditions. The cause of the discrepancy between experimental and in-situ reaction rates is uncertain but may reflect the proximity of natural systems to equilibrium, efficiency of solution/mineral contact, ageing of mineral surfaces, the nature of defects, etch pits and leached layers on mineral surfaces, surface coatings, gradients in solution chemistry in micro-pores and overestimates of dissolution rate for minerals with slow dissolution kinetics due to the lag in step density decrease following the change in dissolution mechanism from etch pit to step retreat as equilibrium is approached (e.g. Brantley and White, 2003).

Modelling the progress of such reactions is frustrated by uncertainties in the absolute mineral surface reaction rates and the significance of other rate-limiting steps in natural systems (see White and Brantley, 2003 for a complete review). It is well established that silicate dissolution rates in the natural environment are typically 2 to 5 orders of magnitude slower than, far-from-equilibrium, laboratory-derived rates at similar pH and temperature conditions (Fig. 1.2-2) (White and Brantley, 2003), and the laboratory rates are typically the only rates available for simulations (e.g. Knauss *et al.*, 2005; White *et al.*, 2005; Xu *et al.*, 2004). Quantification of the kinetics of fluid-mineral reactions in natural systems, rich in CO<sub>2</sub>, is thus required for the accurate prediction of the long-term performance of geological storage sites.

#### **1.2.3.** Natural Analogues

Carbon dioxide occurs naturally as a result of geologic processes in large, often high-purity (>90%) deposits in many sedimentary basins forming an ideal analogue to the subsurface storage of anthropogenic CO<sub>2</sub> (Allis *et al.*, 2005; Czernichowski-Lauriol *et al.*, 1999; Evans *et al.*, 2004; Gaus *et al.*, 2005; Haszeldine *et al.*, 2005; May, 2005; Moore *et al.*, 2003, 2005; Pauwels *et al.*, 2007; Pearce *et al.*, 1996, 1999, 2004; Stevens *et al.*, 2001; Worden, 2006). Several CO<sub>2</sub> fields in the United States, Hungary, France, Australia and Argentina have been exploited to provide injectant for enhanced oil recovery projects and industrial quality CO<sub>2</sub> (Wycherley *et al.*, 1999).

The introduction of a volatile species such as  $CO_2$ , be it anthropogenic or naturally produced, into subsurface geological reservoirs will result in chemical disequilibria and the initiation of various chemical reactions. Its abundance and the rapid kinetics of reactions involving dissolved carbonate species make it an important buffer of pH and a volatile component which dominates the overall equilibrium state of many natural systems (e.g. Coudrain-Ribstein *et al.*, 1997; Hutcheon and Abercrombie, 1989, 1990; Hutcheon *et al.*, 1992). In sedimentary formations the partial pressure of  $CO_2$  ( $pCO_2$ ) can be more than 10–100 times greater than atmospheric  $pCO_2$  at 25 °C (Coudrain-Ribstein *et al.*, 1998; Gaucher *et al.*, 2007). The mechanism of  $CO_2$  generation in some sedimentary basins and magmatic systems produces large quantities of  $CO_2$  which are able to migrate from its source through the basin interacting with reservoir fluids and minerals.

Examination of natural analogue sites allows characterization of physiochemical processes, important for predicting the fate of geologically stored CO<sub>2</sub>, which cannot be captured at the laboratory scale and which, otherwise, would only be available through multiple, costly experimental CO<sub>2</sub> injection projects. These include observations, at the field-scale, of 1) multiphase flow where geophysical or isotopic constraints (such as stable or noble gas isotope systematics) are available; 2) gas-fluid-mineral reaction kinetics (and their inherent complexity in natural reservoirs with highly complex mineralogies, fluid chemistries and permeability structures); 3) the structural, hydrodynamic and geochemical controls on CO<sub>2</sub> leakage, at a variety of temporal scales, which can only be made from natural observations (or from the failure of industrial CO<sub>2</sub> storage projects).

Access to fluids and gas samples from the deep subsurface is often difficult and costly. This thesis examines the geochemistry of a natural, leaking accumulation of carbon dioxide at Green River, Utah, in the Colorado Plateau, USA (Fig. 1.2-3) where fluid and gas effusion allows direct observation of physiochemical processes occurring in the subsurface.



Figure 1.2-3 The Colorado Plateau, located in the south western USA, is an extensive uplifted region covering portions of Utah, Colorado, Arizona and New Mexico. Natural accumulations of subsurface CO<sub>2</sub> gas are common in this province and the adjacent southern Rocky Mountain region, where eighteen  $CO_2$ fields have been identified (Allis et al., 2001). Some CO<sub>2</sub> fields, notably Bravo Dome (NM), McElmo and Sheep Mountain (CO), Farnham Dome (UT), Springerville (AZ), and Big Piney-LaBarge (WY) have been exploited for commercial purposes, mainly for enhanced oil recovery and dry ice production (Allis et al., 2001). The source of the  $CO_2$  is considered to be dominantly volcanogenic, juvenile  $CO_2$  generated from Cenezoic magmatic activity and mantle degassing (Gilfillan et al., 2005, 2008, 2009). The gas reservoirs, usually sandstone or dolomite, lie in four way dip closed or anticlinal structures with mudstone or anhydrite top seals. Fault seals are common along the margins of the reservoirs (Allis et al, 2001; Shipton et al., 2004). The commercially producing fields contain from 28 to 2800 billion m<sup>3</sup> of CO<sub>2</sub> gas (Allis et al., 2001). The gases from the fields can be > 98% CO<sub>2</sub> with trace quantities of N<sub>2</sub> (4%), He (0.1-1%), Ar, and CH<sub>4</sub> (Allis et al., 2001). Associated with these large subsurface CO<sub>2</sub> accumulations is a region of surface CO<sub>2</sub> leakage near Green River, Grand and Emery County, Utah, the focus of this thesis. Significant volumes of CO<sub>2</sub> escape to the surface in intimate association with the Little Grand and Salt Wash fault zones, along the northern edge the Paradox Basin.

## **1.3.** Project Aims and Scope

Understanding the geochemical behaviour of anthropogenic carbon dioxide stored in geological reservoirs, over a range of time-scales, is crucial for quantifying the risk of leakage and the

evolution of the sequestered form of that  $CO_2$  through the life of an individual storage site. Observations from natural analogue sites provide insights into physical and chemical processes which differ at the field and laboratory scales. Direct measurement of the rate of  $CO_2$ -promoted fluid-mineral reactions and quantification of their geochemical dependencies, in natural  $CO_2$ charged groundwater systems can provide important insights into these processes over large physical and temporal scales. Several approaches have been employed in this project to assess the nature and rates of  $CO_2$ -promoted fluid-mineral reactions and their controls. These have included hydrological and geochemical modelling of an active  $CO_2$ -charged groundwater system from which rates of reactions where quantified using mass balance techniques and from petrological constrains on the reacting mineral properties. Measurement of the composition of secondary carbonate minerals, in conjunction with theoretical aspects of trace element incorporation in carbonates, was used to measure in-situ calcite precipitation rates. The synthesis of these approaches allowed quantification of their chemical controls and provides a possible explanation for the orders of magnitude difference in field-scale and laboratory mineral-fluid reaction rates.

Observations of the long term performance of  $CO_2$  leakage from natural sites, via the examination of the geochemical and isotopic composition of dated near-surface carbonate deposits, is used to constrain the interplay of structural and chemical processes in controlling leakage sites and rates, the role of fluid-mineral interactions in generating and closing leakage pathways and their relation to geochemical processes in the host aquifer. These methods provide insights into leakage processes which cannot be discerned from present day measurements alone. Additionally, the relationship between the modern  $CO_2$ -system and exhumed paleo-reservoirs, which exhibit extensive chemical bleaching were hematite grain coatings have been dissolved by the passage of diagenetic fluids, is investigated. Various isotopic, petrological and geochemical methods, and observations from volatile-hosting fluid inclusions, are employed to investigate the mineralogical impact and nature of the volatile-rich diagenetic fluids. The identification of exhumed  $CO_2$  reservoir analogues has important implications for the future examination of  $CO_2$ -fluid-mineral reactions and transport processes at the field scale.

### 1.4. Thesis Outline

In **Chapter 2** the general geology of the field area at Green River, Utah is briefly discussed and the  $CO_2$ -leaking groundwater system is introduced. The thermodynamics of  $CO_2$  and  $CO_2$ -fluidmineral reactions is then briefly discussed, the theory of which, is applied in many subsequent chapters. The  $CO_2$ -spring geochemistry is then addressed. The isotopic composition of the effused fluids and gases are used to place constraints on the origin of the groundwater and  $CO_2$ . Hydrological modelling is then used to place constraints on the flow paths between individual springs. The fluid geochemistry is then addressed, supported by the hydrological modelling and thermodynamic considerations, to place constraints on the nature of the fluid-mineral reactions that control solute composition. Thermodynamic modelling is then used to quantify the in-situ  $CO_2$  solubility and place an upper limit on the degree of  $CO_2$  degassing experienced by the fluids during accent to the surface. Finally, time series fluid geochemistry from the largest of the  $CO_2$ -degassing springs, Crystal Geyser, is used to place constraints on the origin of the fluids, mixing processes in the subsurface and the role of cold water geysering in stimulating leakage from  $CO_2$ -rich groundwater systems.

**Chapter 3** utilizes the geochemical and hydrological models of Chapter 2, in conjunction with mass balance modelling techniques, and petrological measurements on the reacting mineral phases, to place constraints on the kinetics of the controlling fluid-mineral reactions, and their chemical dependencies, in the modern groundwater system. Comparable laboratory experiments are reviewed, the discrepancies discussed, and the implications for field-scale silicate mineral dissolution rates are evaluated.

**Chapter 4** uses petrological, isotopic and geochemical methods to investigate the history of  $CO_2$ -leakage from the Green River anticline, recorded in surface and shallow subsurface carbonate deposits. Isotopic measurements on U-Th dated carbonate deposits are used to reconstruct the last 400,000 year leakage history of the  $CO_2$  system and to place constraints on the style, location and duration of leakage and its relationship to fluid-mineral reactions in the host reservoir and in fracture conduits. Carbonate mineral compositions are used to constrain calcite precipitation rates in the modern setting and their controls and chemical dependencies are discussed.

**Chapter 5** uses petrological, isotopic and geochemical methods, in conjunction with a Raman microspectroscopy study of volatile hosting fluid inclusions, to investigate the nature of volatile rich diagenetic fluids which caused widespread chemical bleaching in Jurassic sandstones outcropping along the crest of the Green River anticline. Fluid inclusion Raman microspectroscopy and microthermometry are used to place constraints on the composition of the volatile phase(s) and the timing of this alteration. Its relation to chemical bleaching within Jurassic sediments of the wider Paradox Basin region is discussed. Additionally, volatile hosting fluid inclusions in bleached portions of travertine feeder systems are investigated using Raman spectroscopic techniques and the two systems are compared.

Finally, tabulated analytical results for water chemistry, gas analyses, XRF, point counting, electron microprobe, and fluid and mineral, stable and radiogenic isotope geochemistry are presented for reference.

## Chapter 2

## Hydrogeology and Geochemistry of a CO<sub>2</sub> Leaking Groundwater System, Green River, Utah

## 2.1. Introduction

 $CO_2$ -charged fluids and gas escape to the surface along faults and through abandoned petroleum exploration wells in the vicinity of Green River, Utah, USA. This provides an opportunity to examine a  $CO_2$ -rich groundwater system as an analogue to processes occurring in anthropogenic  $CO_2$  storage sites. A number of studies have examined various aspects of the origin of the carbon dioxide and effused groundwaters (Baers and Rigby, 1978; Gilfillan, 2004; Heath, 2004; Wilkinson *et al.*, 2008), the nature and magnitude of  $CO_2$  leakage from this site, (Allis *et al.*, 2005), rates of  $CO_2$  effusion from the largest of the  $CO_2$  degassing geysers (Gouveia *et al.*, 2005; Gouveia and Friedmann, 2006), and the role of the local structure and fault architecture on controlling the sites of  $CO_2$  leakage (Dockrill, 2005; Dockrill *et al.*, 2010, Shipton *et al.*, 2004, 2005).

 $CO_2$ -rich groundwaters are widely reported, (e.g. Chernichowski-Lauriol *et al.*, 1996; Pearce et al., 1996) although few contain sufficiently quantities of dissolved CO<sub>2</sub> to sustain cold water geysering (Glennon and Pfaff, 2005; Rinehart, 1980). Many studies have suggested that much of the  $CO_2$  gas in these  $CO_2$ -charged groundwater systems has a deep origin being sourced from magma and/or mantle contributions (Cartwright et al., 2002; Gilfillan et al., 2006, 2008; Pauwels and Fouillac, 1997). Other sources of  $CO_2$  production in the geosphere have been identified including the metamorphism of carbonate rocks, diagenetic reactions between carbonate and silicate minerals, the thermal alteration of coal and other organic material, the biodegradation of oil and gas and the dissolution of carbonate rocks (Hutcheon and Abercrombie, 1990; Wycherley et al., 1999). CO<sub>2</sub>-rich groundwaters typically show very high alkalinity and solute concentrations [1.3-110 mEq L<sup>-1</sup> alkalinity, 200-10,400 mg L<sup>-1</sup> total dissolved solids] (Choi et al., 2005). It is generally accepted that H<sup>+</sup> from the dissociation of carbonic acid enhances fluid-rock reactions in these systems, elevating the solute load of these groundwaters (e.g. Schofield and Jankowski, 2004). This however, is somewhat inconsistent with laboratory experimental results. Many experimental studies agree that dissolution of silicate minerals is enhanced by high  $H^+$  concentrations in acidic solutions. However, the reactions have been shown to be independent of pH (e.g. Drever 1994; Oxburgh et al. 1994) in neutral solutions 5 < pH < 9. Almost all CO<sub>2</sub>-charged groundwaters fall within this pH range (Choi et al., 2005 and references therein). CO<sub>2</sub> rich groundwaters with pH < 5 are rarely observed in the field, because only very dilute solutions can exhibit pH values less than 5 by dissolution and dissociation of CO<sub>2</sub>. This is due to the complexing effect of base cations on speciation in the carbonate system (see section 2.5.1.2).

Subsurface reservoirs imbue rocks with mineral assemblages of highly different solubilities and dissolution kinetics. The extent to which  $CO_2$ -charged groundwater chemistries are controlled by equilibrated reactions with soluble minerals (e.g. carbonates, sulphates and oxides) and kinetically controlled reactions with relatively insoluble minerals with more complex frameworks (e.g. silicates, aluminosilicates) is largely unevaluated. The complex relationship between mineral hydrolysis in multi-mineral assemblages, pH buffering and alkalinity generation is important as it impacts greatly on the reactivity of stored  $CO_2$ , on the stability and precipitation of  $CO_2$  trapping carbonate minerals, on the potential for  $CO_2$ -rich waters to corrode cap-rocks and on the ultimate solubility of the stored  $CO_2$ .

This chapter presents geochemical data from CO<sub>2</sub>-charged springs and geysers emanating along the crest of the Green River anticline, Northern Paradox Basin, Utah. The general geology of the Paradox Basin is discussed with emphasis on the stratigraphic and structural setting of the Green River anticline and its impact on local hydrology. Spring water chemistry and fluid and gas isotope geochemistry is discussed and used to illuminate the source of the groundwater and the CO<sub>2</sub>. Published measurements of hydraulic head are then used to constrain flow paths between individual springs and aid in the interpretation of the evolution of the groundwater solute chemistry. The degree to which spring water chemistry is controlled by equilibrated fluid-mineral reactions is then evaluated using activity-activity diagrams. The evolution of the solute chemistry will be used in Chapter 3 to place constraints on the rates of the kinetically controlled fluid-rock reactions.

The solute and isotope geochemistry of fluid sampled prior to, and during the course of, a large-scale eruption of Crystal Geyser is then discussed. Observations of changes in the chemical and isotopic composition of the fluid is then used to place constrains on the origin of the solute chemistry and fluid mixing processes in the subsurface.

## 2.2. Regional Geology of the Paradox Basin

This region of SE Utah is underlain by the Paradox basin (Fig. 2.2-1a) a late Palaeozoic intracratonic basin filled with a mixture of carbonate, clastic, and evaporite sediments (Nuccio and Condon, 1996). The Paradox Basin is defined by the maximum extent of salt in the Middle

Pennsylvanian Paradox Formation (Nuccio and Condon, 1996). The basin was primarily a Pennsylvanian and Permian feature (320-245 Ma) that accumulated thick deposits of carbonate, halite, and clastics in response to tectonic down-warping and simultaneous uplift along its northeastern border (Baars and Stevenson, 1981). The shape of the basin was modified by later tectonic events, primarily the Laramide orogeny (80-35 Ma) (Dickinson and Snyder, 1978). Today, the basin has been dissected in places by uplift of the Colorado Plateau (25 Ma – present) and downcutting by the Colorado River and its tributaries (Flowers *et al.*, 2008). The basin is bordered on the northeast by the Uncompahgre Plateau, a broad anticline cored by Precambrian rocks. The east side of the basin is bounded by the San Juan dome. The southeast end of the basin is defined by the San Rafael Swell (Fig. 2.2-1b), a Laramide aged monocline, and the far northern end of the basin merges with the southern Uinta Basin.

Sedimentary rocks of the Paradox Basin (Fig. 2.2-2) overlie an Early Proterozoic metamorphic basement that is locally intruded by granite (Nuccio and Condon, 1996). Cambrian through Jurassic strata unconformably overlies the basement rocks. Remnants of Cretaceous rocks are also present, especially in the north-western and south-eastern part of the basin, but, except for the igneous intrusive centres, Tertiary rocks have been completely eroded away (Nuccio and Condon, 1996). At the surface, the subhorizontal, north-dipping rocks in the study area (Fig.2.2-3) consist of Jurassic and Cretaceous clastic sedimentary rocks that include from oldest to youngest: Entrada Sandstone, Curtis Sandstone, Summerville Formation, Morrison Formation, Cedar Mountain Formation, Dakota Sandstone, and Mancos Shale (Fig.2.2-4).

### 2.2.1.1 Pre-Pennsylvanian Rocks

Cambrian through Devonian sedimentation in Eastern Utah was on a stable shelf in mainly shallow marine conditions (Blakey, 2008). Sub-Pennsylvanian rocks consist of the Lower and Middle Cambrian Tintic Quartzite, Upper Cambrian Ignacio Quartzite, Middle Cambrian Ophir Formation, Middle Cambrian Maxfield Limestone, Middle and Upper Cambrian Lynch Dolomite, Upper Devonian Aneth and Elbert Formations and Ouray Limestone, and the Mississippian Leadville Limestone.

### 2.2.1.2 Pennsylvanian and Permian Rocks

During the Pennsylvanian and Permian, the Uncompany Plateau experienced rapid and largescale uplift, and the adjacent north-eastern side of the Paradox Basin subsided, accumulating sediments of great thickness (as much as 3650m) (Nuccio and Condon, 1996). Deposits within the oldest Pennsylvanian formation, the Molas Formation, are transitional from nonmarine to marine, later being deposited and reworked by streams. The upper part has, in addition to fluvial strata, marine limestone beds deposited by the transgressive Middle Pennsylvanian Sea.



**Figure 2.2-1** Geological features of the Paradox Basin and surrounding region. (a) Structural provinces of the Paradox Basin and bordering uplifts (after Condon, 1997). (b) Main structural features of the Northern Paradox Basin, in the vicinity of the study area. The outlined area in grey is the maximum extent of the Pennsylvanian evaporite formations which demarks the extent of the Paradox Basin. Yellow stars denote the locations of  $CO_2$ -charged springs or regions of dry  $CO_2$  exhalations.



**Figure 2.2-2** Generalized stratigraphic section for the Green River area. Thickness data compiled from Trimble and Doelling (1978) and Hintze (1993). Hydrological data from Hanshaw and Hill (1969) and Hood and Patterson (1984).

The Middle and Upper Pennsylvanian Hermosa Group includes the Middle Pennsylvanian Pinkerton Trail and Paradox Formation and the Middle and Upper Pennsylvanian Honaker Trail Formations (Doelling, 1988). The Pinkerton Trail consists of interbedded marine limestone and dark shale, deposited in shallow-marine conditions of normal salinity. The cyclic Paradox Formation is composed of dolomite, black shale, anhydrite, halite, and other salts (Hite and Buckner, 1981). Halite is the most abundant constituent of the Paradox, occurring in beds tens of feet thick. The Honaker Trail Formation is composed of cyclically deposited limestone, sandstone, and shale. It represents a return to normal marine conditions in contrast to the evaporitic marine conditions of the Paradox Formation (Condon, 1997). The thickness of the formation varies significantly throughout the basin due to salt flowage in the underlying Paradox Formation during deposition.

Continued uplift of the Uncompany Plateau in Late Pennsylvanian and Early Permian time eventually unroofed the Precambrian basement rocks (Nuccio and Condon, 1996). The Permian Cutler Formation is mostly a product of this unroofing process and consists of arkose sandstone, deposited in a series of alluvial fans (Campbell, 1980). In the study area, the Cutler Group includes the Elephant Canyon Formation, the Cedar Mesa Sandstone, the Organ Rock Formation, and the White Rim Sandstone (Baars, 1962).

#### 2.2.1.3 Triassic and Jurassic Rocks

In the Triassic and Jurassic, sedimentation in the area of the Paradox Basin was influenced to a great degree by development of magmatic arcs to the south and west of the current basin (Currie, 1997). Development of the arcs produced periodic uplift in source areas and provided sediment to the Paradox Basin (Nuccio and Condon, 1996). Triassic and early Jurassic sedimentary units contain large volumes of ash derived from volcanic activity in the arcs, creating thick regional aquitards. Times of less tectonic activity, especially in the Middle Jurassic, led to deposition of marine, sabkha, and eolian deposits of high hydraulic conductivity.

Deposition of Permian, Triassic, and Jurassic sediment onto thick sequences of salt in the Middle Pennsylvanian Paradox Formation led to the diapiric rise of the salt in several anticlines in the fold and fault belt. Individual Triassic and Jurassic units thin on the flanks of these anticlines (Doelling, 1988). The basal Triassic unit in the basin is the Early and Middle Triassic Moenkopi Formation. Uplift south of the Paradox Basin in Late Triassic time led to development of a north-westward flowing fluvial system depositing the Upper Triassic Chinle Formation (Huntoon *et al.*, 2002). The thickness of Jurassic sediment is dominated by the Lower Jurassic Glen Canyon Group, which is composed of the Wingate Sandstone, Kayenta Formation, and Navajo Sandstone (Doelling, 1988). The Wingate and Navajo are massive eolian units, the Kayenta is fluvial. Contacts between formations of the group are gradational; an unconformity lies at the top of the

Navajo Sandstone (Doelling, 1988). Unconformably overlying the Glen Canyon Group is the Middle Jurassic San Rafael Group. The San Rafael Group consists of the Page Sandstone, Carmel Formation, Entrada Sandstone, Curtis Formation, and the Summerville Formation. These formations were deposited in and on the margins of an inland sea (Nuccio and Condon, 1996).

#### 2.2.1.4 Cretaceous and Tertiary Rocks

Late Tertiary to Holocene erosion removed Cretaceous and Tertiary rocks throughout most of the Paradox Basin (Nuccio and Condon, 1996). The remaining Cretaceous rocks comprise the Early Cretaceous Morrison Formation and Cedar Mountain Formation (Molenaar, 1981) and the Upper Cretaceous Dakota Sandstone and Mancos Shale. The dominant event of latest Cretaceous and Tertiary time was the development of uplifts and adjacent basins associated with the Laramide orogeny. Major structural features in the Paradox Basin region are the Uncompahyre Plateau, San Rafael Swell, Monument Upwarp, San Juan Dome, and Uinta Basin. Records of Tertiary sedimentation in the Paradox Basin are absent due to late Tertiary uplift and erosion; however, it is very likely that Palaeocene, Eocene, and possibly even Oligocene, Miocene, and Pliocene rocks were once present in the northernmost part of the basin (Nuccio and Condon, 1996).

#### 2.2.2. Local Structure

The northern part of the Paradox Basin, pertinent to this study (Fig. 2.2-1, Fig. 2.2-3), has been termed the Paradox fold and fault belt (Kelley, 1958). This includes the area encompassing the Green River and the major structural features of the Little Grand Wash and Salt Wash fault zones, the sites of natural CO<sub>2</sub> leakage (Dockrill, 2005; Shipton *et al.*, 2004, 2005) (Fig. 2.2-4). This area consists of a series of parallel, northwest-trending faults, anticlines, and synclines. Dissolution of salt along the crests of some anticlines in this region has caused down-faulting and the development of grabens at the crests (Doelling *et al.*, 1988). Rocks as old as Pennsylvanian are exposed in the cores of some anticlines, and remnants of Cretaceous rocks are present in some synclines.

The Little Grand Wash fault is a steeply south-dipping, listric normal fault, with an arcuate surface trace length of about 61 km (Shipton *et al.*, 2004). The fault splays into two strands for ~ 3.3 km of its length (Shipton *et al.*, 2004). The throw of the fault near the Green River is about 290 m and much of the displacement is concentrated along the southern strand (Heath, 2004). The fault may cut rocks from Pennsylvanian to early Cretaceous and sole into the halite-rich Pennsylvanian Paradox Formation (Heath, 2004). To the south, the Salt Wash and the Tenmile Grabens are together about 31 km long and are separated by a step-over zone (Dockrill, 2005). The faults strike about N 70° W (Dockrill, 2005). The southeast end of the Salt Wash faults may link to the northwest tip of the Moab fault (Shipton *et al.*, 2004). At least some

movement of these faults may be related to salt flow, since the faults are located on the northern plunging limb of the broad Cane Creek-Big Flat salt anticline. Doelling *et al.*, (1988) and Condon, (1997) concluded that salt migration commenced in the Permian and continued to the mid Jurassic. Local sedimentation patterns reveal a period of salt movement between Triassic to mid Jurassic resulting in the development of the Green River anticline and adjacent Courthouse Syncline (Dockrill, 2005). Fault movement may also be due to interaction of the Uncompahgre and San Rafael blocks to the east and west, respectively (Campbell and Baer, 1978). Unpublished illite age analysis dates fault movement at 40 Ma  $\pm 10$  corresponding to the early tertiary Laramide orogeny (Dockrill, 2005).

### 2.2.3. CO<sub>2</sub>-charged Springs

Almost pure CO<sub>2</sub> gas [95.7-99.4 % CO<sub>2</sub>; 3.4-0.5 % N<sub>2</sub>; 0.1-0.9 % O<sub>2</sub>, 0.01-0.05 % Ar; 0.00-0.01 % He; Heath (2004)] is discharged from the Green River anticline along the Little Grand and Salt Wash fault systems, in the vicinity of Green River forming a series of geysering, cold water springs and dry exhalations (Fig. 2.2-5). CO<sub>2</sub>-charged springs and mofettes emanate along and within complexities of the local normal fault systems or as fluid escapes from abandoned petroleum exploration and water wells (Fig. 2.2-6). Most springs occur in the northern fault footwalls of Little Grand Fault (Green River Airport Well [Grand Fault Unit 14-24], Crystal Geyser [Glen Ruby #1-X]) or Salt Wash Graben (Small Bubbling Spring, Big Bubbling Spring, Pseudo Tenmile Geyser, Torry's Spring [Delaney Petro Corp #1]) where these faults intersect with the crest of the Green River anticline (Fig 2.2-4). Two springs lying off the normal fault systems (Tumble Weed Geyser and Chaffin Ranch Geyser), are located towards the anticlines axis and are sourced from abandoned water wells. Tenmile Geyser lies in the hangwall of the northern fault of the Salt Wash Graben and is thought to represent effusion from a well penetrating to considerable depth, through to the footwall of the fault, but no record of this well could be found. Fluid discharge varies between individual springs typically being greater in the open conduits formed by wells. All the springs have been observed to geyser at some point in their history, but the height of these eruptions and volumes of expelled fluid vary considerably. Only Chaffin Ranch Geyser and Crystal Geyser erupt with any regularity. The most dramatic of these is Crystal Geyser on the eastern bank of the Green River in the footwall of the Little Grand Wash fault zone. This cold-water geyser has erupted at 8-22 hour intervals since the Glen Ruby #1-X well was drilled to the base of the Triassic section (TD 801 m) in 1935 (Baer and Rigby, 1978). The well was spudded into a 21.5m thick travertine mound attesting to a long history of leakage from this site prior to drilling of the well (Shipton et al., 2004). Layered, ochre coloured travertine deposits accumulate within the immediate vicinity of all the emanations (Fig. 2.2-7). Many springs are also demarked by the precipitation of salt crusts as surface runoff evaporates.



**Figure 2.2-3** Map showing the main geographic features of the region surrounding Green River and the locations of all known  $CO_2$ -escapes. Dotted lines show the location of the cross sections in Figure 2.4-10.



**Figure 2.2-4** Surface geology of the Green River anticline redrawn after Doelling (2000). Structure contours are for the top of the Navajo Sandstone (after Dockrill, 2005). The map shows the clustering of springs along the axis of the anticline, within the damage zones of the Little Grand Fault and the northern fault of Salt Wash Graben.



**Figure 2.2-5** Photographs of springs, geysers, and groundwater leakage from abandoned wells. (a) Crystal Geyser. This geyser erupts periodically about once every 16 hours to a height of ~20 m from the Glen Ruby #1-X abandoned oil exploration well drilled during 1935 and 1936 (b) a side seep ~8m from Crystal Geyser. (c) Chaffin Ranch Geyser; regularly geysers, sourced from a water well drilled for livestock.(d) Torreys spring sourced from the Delaney Petroleum Co. #1 well (e) Tumble Weed Geyser, sourced from a water well drilled for livestock



**Figure 2.2-6** Photographs of springs, geysers, sourced from abandoned wells and natural leaks. (a) Past eruption from Crystal Geyser showing a large discharge of water, much greater than what is seen today; estimated eruption high 23m (Shipton, 2004) (b) Modern eruption of Crystal Geyser, exhibiting its maximum height of ~12m (c) Pseudo-tenmile Geyser, a natural seep at the intersection of the Salt Wash Graben and the apex of the Green River anticline (d) Tenmile Geyser with well casing; thought to be an exploration well drilled within the Salt Wash Graben through to the underlying footwall. (e) Big Bubbling Spring, a natural seep at Salt Wash Graben.



**Figure 2.2-7** Field photographs of modern Crystal Geyser (a,e) travertine mound and travertine formed around Green River Airport Well (b), Chaffin Ranch Geyser (c) and Tumble Weed Geyser (d). (a) Hemispherical pools that form the terrace morphology on travertine surface (b) Friable travertine poor in Fe, iron content of the travertine has a significant impact on its strength. (c) Fe-rich irregular travertines when the fluid flux is low (d) Large pools form around some of the springs where discharge can exceed local evaporation. The pools contain a travertine substrate. (e) Fe-rich, down-stepping lobate mounds that radiate out from geyser vent, with conically shaped speleothems on sub-vertical surfaces of the mound.

## **2.3.** Geochemical Sampling and Results

Knowledge of any groundwater system is often limited to the chemical data collected from surface spring waters. Manipulation of chemical data allows a valuable window into the deep workings of a groundwater system, provided that hydrology and geology of the site are sufficiently understood. Of particular importance when quantifying physiochemical controls on solute composition from spring fluids are: 1) knowledge of the conditions from which the fluids were sourced (e.g. host lithology, *P*, *T*) and; 2) any geochemical processes which may alter groundwater chemistry as fluids ascend to the surface, such as  $CO_2$  degassing and calcite precipitation. These aspects of  $CO_2$ -spring chemistry are discussed in this section, especially with relevance to the carbonate system and fluid-mineral reactions controlling solute chemistry.

### 2.3.1. Field Sampling Methods

Water samples collected from the springs were filtered through 0.2 µm nylon filters on site and stored in pre-cleaned high-density polyethylene bottles, prewashed with filtrate, one sample acidified to ~pH 2-3 with HNO<sub>3</sub> for analyses of cations and one un-acidified sample for analysis of anions. All samples where stored in 60 mL plastic bottles free of air to minimise degassing and oxidation. pH, alkalinity (by Gran titration (Stumm and Morgan, 1996)) and temperature were measured in the field. The pH probe was calibrated daily with 4.0 and 7.0 pH standards.

Oxidation-reduction potential (mV) was measured in-situ using a Hach Lange MC3051Pt-9 ORP platinum electrode filled with an Ag/AgCl reference electrode and saturated KCl filling solution. These measurements were then converted to Eh values by using measured temperature values in order to establish standard hydrogen electrode corrections. ORP standard (Orion @ #967961) was used to perform ORP electrode checks where the measured value of the standard was 220 ± 3 mV at 25°C. The platinum electrode was cleaned at the end of each sampling day and stored according to manufacturer's guidelines. ORP electrodes can be erratic when used in ground water and often do not stabilize rapidly (Stumm and Morgan, 1981). For each spring, measurements were recorded every five minutes over a thirty minute sampling interval and the average reported.

Exsolved gases were collected in 10 mm diameter, internally polished, refrigerationgrade copper tubes (EAWAG, 2000). Individual sampling units comprise two sections of copper pipe separated by a Swagelok<sup>®</sup> needle valve closed at either end with high grade thread sealing nuts. During sampling polyerothene tubing and funnels where connected to either end of the piping to create a sampling environment isolated from the atmosphere. The tube is flushed through with gas or water for at least 30 minutes to remove air contamination before the copper tube was submerged and sealed using sealing nuts.

### 2.3.2. Analytical Methods

Water samples were collected from springs and geysers, during the 2006 and 2007 field season, for the analysis of  $\delta^{18}$ O,  ${}^{87}$ Sr/ ${}^{86}$ Sr,  ${}^{3}$ H, K<sup>+</sup>, Na<sup>+</sup>, Ca<sup>2+</sup>, Mg<sup>2+</sup>, Sr<sup>2+</sup>, Ba<sup>2+</sup>, Fe, Mn, Al<sup>3+</sup>, SiO<sub>2</sub>, Cl<sup>-</sup> and SO<sub>4</sub><sup>2-</sup> (Table 1, Appendix A). Time series samples through a large-scale eruption of Crystal Geyser were collected during the 2007 season. Dissolved inorganic carbon (DIC) was calculated from field alkalinity and pH using the computer code PHREEQC (Pankhurst and Appelo, 1999). Cation analyses were measured on acidified samples using a Varian Vista-PRO simultaneous inductively coupled plasma atomic emission spectrometer (ICP-AES) and anion concentrations were analysed on a Dionex Ion Chromatography System at the University of Oxford (2006 sample set) and the University of Cambridge (2007 sample set). Spring samples were diluted to fit the calibration range. For the 2006 data set all water samples were interspersed with standards SPSSW2 and T-167 which indicate accuracies better than ±5% for Na, K, Ca, Mg, Al, S and Si. For the 2007 data set multiple analysis of standard T-167 by AES again indicates accuracies of better than ±5% (2 $\sigma$ ).

Total dissolved inorganic carbon (DIC) was measured at the University of Cambridge.  $CO_2$  was released from 5–15 mL aliquots of spring water by acidification with >100 % H<sub>3</sub>PO<sub>4</sub> in vacuum.  $CO_2$  released on acidification in the reaction vessel was extracted while water was trapped at -80 °C. Total  $CO_2$  was measured manometrically before being converted to mmol L<sup>-1</sup>.

Analyses for <sup>87</sup>Sr/<sup>86</sup>Sr at the University of Cambridge follow Bickle *et al.* (2003) with analyses of NBS987 giving 0.710258  $\pm$  0.000008 (2 $\sigma$ , *n* = 11) over the period of the analyses (2006 data set).  $\delta^{13}$ C of dissolved inorganic carbon (DIC) and the  $\delta^{18}$ O of H<sub>2</sub>O were analysed in the Godwin Labs, University of Cambridge and are expressed in  $\delta\%_0$  deviation relative to Peedee Belemnite (PDB) and VSMOW standards with analytical precisions estimated at  $\pm$ 0.06 and  $\pm$ 0.08  $\%_0$  respectively. Analysis for  $\delta^{13}C_{CO2(g)}$  of the sampled gas where performed at the University of Cambridge using VG PRISM Mass Spectrometer.

Enriched <sup>3</sup>H was counted at Brigham Young University using a PerkinElmer Quantualus 1220 Liquid Scintillation Counter with a detection limit of  $\pm 0.8$  tritium units and a precision of about  $\pm 0.3$  TU.

 $\delta^{13}$ C of CO<sub>2</sub>(g) from collected gas samples are presented in Appendix A and detailed in figure 2.4-6. Major cation, anion and isotope analyses for the CO<sub>2</sub>-spring waters and for time-series fluid chemistry from Crystal Geyer are presented as data tables in Appendix A.
# 2.4. Discussion

# 2.4.1. CO<sub>2</sub>-Water-Rock Interactions

# 2.4.1.1 CO<sub>2</sub> Solubility and the Carbonate System

The theoretical aspects of carbonate equilibria are covered in great detail elsewhere (e.g. Drever, 1997; Garrels and Christ, 1965; Plummer *et al.*, 1979; Stumm and Morgan, 1981), and only a brief overview of the carbonate equilibria necessary for understanding  $CO_2$  dissolution and speciation,  $CO_2$  degassing and  $CO_2$  promoted fluid-rock interaction is discussed here. As is well known, dissolution of  $CO_2$ , and subsequent precipitation of calcite, is determined by the chemical exchange equilibria:

$$CO_2(g) \leftrightarrow CO_2(aq)$$
 (2.1)

$$CO_2(aq) + H_2O \leftrightarrow H_2CO_3 \tag{2.2}$$

$$H_2CO_3^* \leftrightarrow H^+ + HCO_3^- \tag{2.3}$$

$$HCO_{3}^{-} \leftrightarrow H^{+} + CO_{3}^{-} \tag{2.4}$$

$$Ca^{2+} + CO_3^- \leftrightarrow CaCO_3(s) \text{ at pH} > 8 \text{ or}$$
 (2.5)

$$Ca^{2+} + 2HCO_3^- \leftrightarrow CaCO_3(s) + H^+ + HCO_3^- \leftrightarrow CaCO_3 + CO_2(aq) + H_2O$$
  
at pH  $\leq 8$  (2.6)

where  $H_2CO_3^*$  represents  $H_2CO_3 + CO_2(aq)$  and the overall defining reaction for calcite precipitation may be written

$$Ca^{2+} + 2HCO_3^- \leftrightarrow CaCO_3(s) + CO_2(aq) + H_2O$$

$$(2.7)$$

Where the calcite saturation index (SI<sub>CC</sub>), the logarithm of the saturation state ( $\Omega$ ), is defined as

$$SI_{cc} = \log\left(IAP_{cc}/K_{sp}\right)$$
(2.8)

where

$$K_{sp} = \frac{a_{Ca^{2+}} \cdot a_{HCO_3^-}}{a_{H^+}} = \frac{\gamma_{Ca^{2+}} [Ca^{2+}] \cdot \gamma_{HCO_3^-} [HCO_3^-]}{\gamma_{H^+} [H^+]} , \qquad (2.9)$$

the activities at equilibrium, and

$$IAP_{cc} = \frac{a_{Ca^{2+}} \cdot a_{HCO_{3}^{-}}}{a_{H^{+}}} = \frac{\gamma_{Ca^{2+}}[Ca^{2+}] \cdot \gamma_{HCO_{3}^{-}}[HCO_{3}^{-}]}{\gamma_{H^{+}}[H^{+}]},$$
(2.10)

the activities in the water sample. Where *a* is activity, [] is concentration, and  $\gamma$  is an activity coefficient. *SI* = 0, if there is equilibrium between the mineral and the solution; SI < 0 reflects subsaturation, and *SI* > 0 supersaturation (see for example Appelo and Postma, 2005, Drever, 1997).

Initially,  $CO_2$  transfers across the gas-water interface to become an aqueous ion, a kinetically slow process [Eq. (2.1), (2.2)] (Dreybrodt, 1996). The solubility of  $CO_2$  increases with pressure, but decreases with temperature and salinity (Joyce and Holloway, 1993; Duan and Sun, 2003) (Fig. 2.4-1). At 25 °C and 1 bar, the solubility of  $CO_2$  in an aquifer fluid equivalent to a 3 M NaCl solution is approximately one-third its solubility in pure water. The dissolution of  $CO_2$  and subsequent speciation can be described by equations (2.1-2.4).

The removal of  $CO_2(g)$  from solution drives equation (2.1) to the left and equation (2.7) to the right, driving calcite precipitation in CO<sub>2</sub>-degassing springs and the formation of travertine. However, numerous studies (e.g. Dreybrodt *et al.*, 1992; Herman & Lorah, 1987, 1988; Lorah & Herman, 1988; White, 1997) show that calcite does not precipitate instantaneously at the point of saturation. Precipitation requires a finite supersaturation because of activation barriers to calcite nucleation and crystal growth (White, 1997). In most circumstances this implies a saturation index (*SI<sub>CC</sub>*) of +0.5, although Dreybrodt *et al.* (1992) suggest that saturation indices of at least +1.0 are required.



**Figure 2.4-1** CO<sub>2</sub> solubility (mol kg<sup>-1</sup>) as a function of temperature and various salinities at pressures of 1 and 100 bar. Calculations performed using the CO<sub>2</sub> solubility model of Duan *et al.*, 2006.



**Figure 2.4-2** Carbonate speciation for the system  $CO_2-H_2O$  and  $CaCO_3-CO_2-H_2O$  assuming open system equilibrium and externally fixed  $pCO_2$  (calculations performed in PHREEQC). (a) Speciation in the simple system  $CO_2-H_2O$  illustrates that  $H_2CO_3^*$  is the dominant species in solution at the  $pCO_2$  of the springs. (b) The addition of calcite to the  $CO_2-H_2O$  system greatly affects the speciation of carbon in solution. The most dramatic change is  $[H_2CO_3^*]$  becoming subordinate to  $[HCO_3^-]$ .  $HCO_3^-$  stability increases up to 4 orders of magnitude (compared to the  $CO_2-H_2O$  system) before  $[H_2CO_3^*]$  exceeds  $[HCO_3^-]$  at  $-\log pCO_2$  of 0.4.

## 2.4.1.2 Carbonate System Speciation

The simplest speciation system (after Garrels and Christ, 1965) is the dissociation of carbon dioxide in water and follows from equation (2.1-2.4). All the other controlling species are assumed devoid from water, and hence the electrical neutrality may be written

$$[H^+] = [OH^-] + [HCO_3^-] + 2[CO_3^{2-}]$$
(2.11)

Temperature has little effect on the speciation of the system (Garrels and Christ, 1965), with speciation being largely dependent on the pressure of the system (Fig. 2.4-2). As  $pCO_2$  goes to zero, the solution pH approaches 7, while increasing  $pCO_2$  causes the system to become more acidic. In this simple system the speciation of  $CO_2$  in the Green River springs would be dominated by  $H_2CO_3^*$ . Most  $H_2CO_3^*$  remains as  $CO_2(aq)$ ; only about 0.3% actually forms carbonic acid (Drever, 1997). Fluid chemistry in groundwater system however, involves interaction with additional components, most importantly  $Ca^{2+}$ , whose presence alters the electrical neutrality of the system and the subsequence carbonate speciation such that

$$2[Ca^{2+}] + [H^+] = [OH^-] + [HCO_3^-] + 2[CO_3^{2-}]$$
(2.12)

Addition of CaCO<sub>3</sub> to the system significantly affects the speciation. At 25 °C the shift in speciation between  $H_2CO_3^*$  and  $HCO_3^-$  implies an approximately even distribution of these two species in the CO<sub>2</sub>-charged groundwaters.

Upon dissolution of  $CO_2$ , the formation of bicarbonate ion,  $HCO_3^-$  and production of acidity by release of H<sup>+</sup> leads to a series of secondary reactions with complex feedbacks that buffer solution properties and mineral reactivity (Gunter *et al.*, 1993). In the absence of any fluid-mineral interaction the disassociation of this dissolved  $CO_2$  results in an acidic solution of pH 3.4 due to the dissociation of carbonic acid:

$$CO_2(g) + H_2O \leftrightarrow CO_2(aq) + H_2O \leftrightarrow H_2CO_3 \leftrightarrow H^+ + HCO_3^-$$
 (2.13)

A temperature-dependent dissociation constant K can be defined for Eq. (2.13):



Figure 2.4-3 Temperature dependent dissociation constant for H<sub>2</sub>CO<sub>3</sub> showing maxima at ~55°C

Calculations of log *K* (Eq. (2.14)) using SUPCRT92 (Johnson *et al.*, 1992) show a maximum of dissociation for reaction (2.13), occurring at about 55 °C above which log *K* decreases continuously with increasing temperature such that an initially weak acid becomes increasingly weaker at elevated temperature (Fig. 2.4-3). Thus, at low temperatures, the increased availability of H<sup>+</sup> might be expected to cause higher rates of mineral hydrolysis. Overall the larger relative solubility of CO<sub>2</sub> and the effective disassociation of H<sub>2</sub>CO<sub>3</sub>, means that even at very low temperatures CO<sub>2</sub>-charged fluids have a significant effect on the promotion of mineral-fluid reactions.

# 2.4.1.3 Alkalinity

Alkalinity [Alk] is a measure of the ability of a solution to neutralize acids to the equivalence point of carbonate or bicarbonate (Stumm and Morgan, 1981). It is equal to the stoichiometric sum of the bases in solution. In groundwater systems carbonate alkalinity tends to make up most of the total alkalinity due to the common occurrence and dissolution of carbonate minerals and the ubiquitous presence of dissolved  $CO_2$  (Drever, 1997). Other aqueous species that can contribute to alkalinity include  $BO_3^{3-}$ ,  $PO_4^{-3}$ ,  $SiO_2$  and  $NH_3$  although these have low concentrations in groundwaters (Drever, 1997). Alkalinity may be defined either as:

$$[Alk] = [HCO_3^-] + 2[CO_3^{-2}] + [OH^-] - [H^+]$$
(2.15)

or, the excess of positive charges over the anions of strong acids:

$$[Alk] = [Na^{+}] + [K^{+}] + 2[Ca^{2+}] + 2[Mg^{2+}] + \dots - [Cl^{-}] - 2[SO_{4}^{2-}] - [NO_{3}^{-}] - \dots$$
(2.16)

Removal or addition of  $CO_2$  modifies DIC and pH without changing [Alk] as the net reaction produces the same number of equivalents of positively contributing [H<sup>+</sup>] as negative contributing species [HCO<sub>3</sub><sup>-</sup> and/or CO<sub>3</sub><sup>2-</sup>]. This concept is typically illustrated in a capacity diagram (Deffeyes, 1965) which plots alkalinity against DIC to expediently show contours of pH. Accurate determination of pH, field alkalinity and DIC can be assessed by comparison of the measure values of [Alk], DIC and pH with the position of pH isopleths predicted from equilibrium conditions. If extensive CO<sub>2</sub> degassing had occurred prior to sampling the measured values of pH should be significantly large than those predicted by equilibrium considerations. Figure 2.4-4 shows the relation between measured DIC (mmol L<sup>-1</sup>), field alkalinity (mEq L<sup>-1</sup>) and pH for the Green River springs. Measured values of pH are close to or within error of values predicated by theoretical considerations suggesting that equilibration within the carbon system is largely maintained during ascent of fluid to the surface and sampling.

Addition of  $CO_2$  to a solution in contact with rock forming minerals can affect alkalinity. Hydrolysis of silicate, alumino-silicate and carbonate minerals consumes [H<sup>+</sup>] increasing [Alk], while releasing cations to solution which do not contribute to alkalinity. Precipitation of carbonate minerals consumes  $HCO_3^-$  and/or  $CO_3^{2-}$  buffering [Alk] towards lower values. Alkalinity is therefore an important measure of the degree of fluid-rock interaction in a groundwater system.  $CO_2$ -rich groundwater systems should evolve to higher alkalinity due to the progressive hydrolysis of rock forming minerals.



**Figure 2.4-4** Capacity (Deffeyes) diagrams for the CO<sub>2</sub>-springs. pH measurements made in the field are labeled next to each sample (2006 data). Data for the 2007 sampling program is included for reference. Constant pH isopleths are labeled about the margins of the diagrams for equilibrium at 25 °C. Change in temperature has negligible effect on the location of the important isopleths (between pH's of 6 and 9). Springs are invariably characterized by higher [Alk] than DIC when compared to corresponding pH isopleths. The deficiency in DIC is interpreted to represent CO<sub>2</sub>-degassing (which maintains [Alk]).

## 2.4.1.4 Fluid-Mineral Reactions

After introduction of  $CO_2$  into a geological reservoir, initial rapid carbonate, sulphate and oxide acid hydrolysis is expected to be followed by more sluggish ion-exchange reactions and then hydrolysis of silicate phases accompanied by re-precipitation of carbonate in excess of that dissolved. Upon consumption of these phases and as the fluid-mineral system moves towards saturation with respect to these minerals, kinetically slower and energetically less favourable reactions will begin to dominate the geochemical evolution of these fluids. The dissolution of silicate and phylosilicate minerals, which are typically undersaturated in near surface and shallow subsurface geological fluids (Brantley and White, 2003), will be enhanced by the reduction in pH afforded by the dissolution and speciation of  $CO_2$  and by the overall availability of H<sup>+</sup> (e.g. Casey and Bunker, 1990; Oelkers et al., 1994). A variety of secondary reactions (e.g. clays, silicates, carbonate, oxide, sulphates and salts) will be promoted by the availability of carbonate ions sourced from CO<sub>2</sub> and carbonate dissolution, cations sourced from mineral dissolution and exchange reactions and the relative increase in saturation of secondary phases as a result of solubilisation of primary minerals and increases in pH. Reactions involving H<sub>2</sub>CO<sub>3</sub><sup>\*</sup> with reservoir minerals are thus many and varied, depending on the chemical composition of the fluid and the mineralogy of the host rock.

Porosity volume in sedimentary basins is dominant by contributions from porous and permeable sandstone formations (e.g. Bethke, 1989). The mineralogy of terrestrial and marine sandstones is dominated by silicate minerals; including quartz and feldspars, and phyllosilicate minerals, including smectites, illites and chlorites (e.g. Cox and Lowe, 1995). Sandstones are

typically variably cemented by carbonate minerals including calcite, dolomite, siderite and ankerite (e.g. Cox and Lowe, 1995). Thus the dominant pH buffering reactions in mixed mineralogies are likely to vary with duration of reaction as the initial pH buffering will be dominated by minerals with fast dissolution kinetics;

Dolomite

$$MgCa(CO_3)_2 + 2H^+ \leftrightarrow Mg^{2+} + Ca^{2+} + 2HCO_3^-$$
 (2.17)

Followed by slower reaction of minerals with more complex frameworks, and lower solubilities, e.g.

Albite

$$NaAlSi_{3}O_{8} + 4H^{+} + 4H_{2}O \leftrightarrow Na^{+} + Al^{3+} + 3H_{4}SiO_{4}$$

$$(2.18)$$

At low temperatures, energy barriers prevent this reaction being reversible and these reactions are dominantly uni-directional. As a result, increases in porefluid  $[Al^{3+}]$ ,  $[H_4SiO_4]$  and mono- and divalent cations results in an increase in the solution saturation state of a range of phyllosilicate minerals whose formation is favoured by thermodynamic considerations, but whose composition and precipitation will be fundamentally controlled by chemical kinetics (Lasaga, 1995).

Dissolved bicarbonate species will form soluble complexes with dissolved cations sourced from fluid-rock reactions, e.g.

$$HCO_3^- + Ca^{2+} \leftrightarrow CaHCO_3^+ \tag{2.19}$$

which will ultimately increase the solubility of the dissolved  $CO_2$ . Dissolved  $HCO_3^-$  will then react with divalent cations, in solution, to form carbonate minerals (e.g. calcite, siderite, magnesite) which will form a sink of  $CO_2$  from the fluid following Eq. (2.6). Rates of these reactions are known to be fast, relative to the slow kinetics of  $CO_2$  dissolution and aqueous speciation, but have a complex dependence on reactant concentrations, in situ pH, temperature and fluid composition (e.g. Morse and Arvidson, 2002; Zuddas and Mucci 1998). Additionally, within porous media the growth of secondary precipitates may be ultimately limited by solute supply and solute transport, as apposed to true mineral surface reaction.

# 2.4.2. CO<sub>2</sub> Sources: Isotopic Constraints

Carbon isotopes aid in the elucidation of the carbon history of groundwaters and  $CO_2$  gases due to the large spread in isotopic composition of the various sources of geospherically derived carbon (Clark and Fritz, 1997). However, assessment of the degree of isotopic equilibration between sampled fluids and  $CO_2$  gas is important before the observed compositions can be considered characteristic of the original source carbon, due to the potential effects of  $CO_2$  degassing and nonequilibirum fraction as fluids ascend to the surface. To determine whether the waters and gases are in equilibrium with respect to carbon isotopes, calculations can be made to derive theoretical, predicted  $\delta^{13}C_{\text{DIC}}$  values based on the  $\delta^{13}C$  of exsolved  $CO_2$  gases.

#### 2.4.2.1 Stable Isotope Fractionation: Notation Review

The isotope fractionation factor between two substances A and B is defined as

$$\alpha_{A-B} = R_a / R_b \tag{2.20}$$

Where 
$$R_a = {}^{h}E / {}^{l}E$$
 (2.21)

The ratio of the heavy isotope over the light stable isotope in phase A, such as  ${}^{18}O/{}^{16}O$  or  ${}^{13}C/{}^{12}C$ . Rather than determining the absolute ratio of a substance it is easier and more precise to determine the relative difference between that substance and a reference such that

$$\delta_A = \frac{R_A - R_{std}}{R_{std}} \times 10^3 \tag{2.22}$$

where  $R_{std}$  is the absolute ratio in the standard. The relation between  $\delta$  values and fractionation factors (which are equilibrium constants that describe how isotopes are portioned between two phases) is

$$\alpha_{A-B} = \frac{1 + \delta_A / 1000}{1 + \delta_B / 1000} = \frac{\delta_A + 1000}{\delta_B + 1000}$$
(2.23)

Values of  $\alpha$  are commonly close to unity so that isotopic fractionation factors are expressed as per mil (% $_{o}$ ) fractionations, which can be approximated as

$$10^{3} \ln \alpha_{A-B} \approx \delta_{A} - \delta_{B} \tag{2.24}$$

#### 2.4.2.2 Carbon Isotopic Composition of DIC and $CO_2(g)$

The mass balance defining the contributions of  $H_2CO_3^*$  and  $HCO_3^-$  forming the total dissolved carbon pool at the pH range of interest can be defined as:

$$\delta^{13}C_{DIC} = X_{H_2CO_3^*} \delta^{13}C_{H_2CO_3^*} + X_{HCO_3^-} \delta^{13}C_{HCO_3^-}$$
(2.25)

Where  $X_{H2CO3*}$  and  $\delta^{13}C_{H2CO3*}$ , and  $X_{HCO3}$  and  $\delta^{13}C_{HCO3-}$  are the mole fractions of each component and their isotopic composition, respectively. Although  $H_2CO_3^*$  is composed of both  $CO_2(aq)$  and  $H_2CO_3$ , the contribution of  $H_2CO_3$  is small and for these calculations all  $H_2CO_3^*$  is assumed to be CO<sub>2</sub>(aq). The fractionation factor,  $\alpha$ , is related to  $\delta$  values for the species CO<sub>2</sub>(aq), HCO<sub>3</sub><sup>-</sup> and CO<sub>2</sub>(g) by (Clark and Fritz, 1997):

$$\alpha_{CO_2(aq)-CO_2(g)} = \left(\delta^{13}C_{CO_2(aq)} + 1000\right) / \left(\delta^{13}C_{CO_2(g)} + 1000\right)$$
(2.26)

$$\alpha_{HCO_{3}^{-}-CO_{2}(g)} = \left(\delta^{13}C_{HCO_{3}^{-}} + 1000\right) / \left(\delta^{13}C_{CO_{2}(g)} + 1000\right)$$
(2.27)

Where the temperature dependent fraction factors are determined using (Mook et al., 1974; Vogel et al., 1970):

$$10^{3} \ln \alpha_{CO_{2}(aa)-CO_{2}(a)} = -0.373 \times 10^{3} T^{-1} + 0.19$$
(2.28)

$$10^{3} \ln \alpha_{HCO_{3}^{-}-CO_{2}(g)} = 9.552 \times 10^{3} T^{-1} - 24.1$$
(2.29)

Which can be combined with the equation of mass balance to yield the isotopic composition of individual carbon species from the analysed  $\delta^{13}C_{CO2(g)}$  using the measured values of DIC, pH and the distribution of carbon species calculated using PHREEQC (Parkhurst and Appelo, 1999).



**Figure 2.4-5**  $\delta^{13}C_{DIC}$  measured versus that calculated from the  $\delta^{13}C$  of  $CO_2(g)$  using equilibrium fractionation factors and the distribution of HCO<sub>3</sub><sup>-</sup> and H<sub>2</sub>CO<sub>3</sub><sup>\*</sup> at the measured pH and DIC.



**Figure 2.4-6** Histogram of the  $\delta^{13}C_{CO2(g)}$  for the 2006 and 2007 sampling programs and from the analyses of Gilfillan (2006) and Heath (2004).  $\delta^{13}C_{CO2(g)}$  analyses show a relatively narrow range from -8.4 to -5.8 % and a skewed distribution towards isotopically light values.

The  $\delta^{13}C_{DIC}$  calculated from the  $\delta^{13}C_{CO2(g)}$  and the measured  $\delta^{13}C_{DIC}$  do not exhibit a 1:1 relationship (Fig. 2.4-5). During ascent to the surface spring waters degas CO<sub>2</sub> as a result of changes in the ambient pressure. The sampled CO<sub>2</sub> gas represents the weighted average of gas degassed over the whole degassing region, where as the sampled waters represent the cumulative fractionation effects up until the point of sampling at the surface.  $\delta^{13}C_{CO2(g)}$  for the CO<sub>2</sub>-springs exhibit a skewed distribution towards lower values (Fig. 2.4-6). This results from a Rayleigh type fractionation of the DIC pool as degassing takes place; with the bulk of the exsolved gas having more negative values, becoming increasingly negative as degassing progresses and occurs at shallower depths. The observed negative correlation in DIC and  $\delta^{13}C_{DIC}$  during a large-scale eruption of Crystal Geyser fits a Rayleigh fractionation model (of pure CO<sub>2</sub> degassing) to a first order (Assayag et al., 2009), but the narrow range of composition observed and lack of corresponding measurements on the gas phase does not put useful constraints on the initial undegassed fluid composition.

The apparent disequilibrium between DIC and  $CO_2$  maybe due to: 1) the large uncertainty in  $\delta^{13}C_{DIC(calculated)}$  due to uncertainty in measured pH and the resulting calculation of carbonate speciation; 2) kinetic fractionation resulting from diffusion into growing gas bubbles; 3) Bulk  $CO_2$  gas measurements representing a cumulative composition resulting from degassing over a degassing region as apposed to a true instantaneously degassed values. Constraints on the degree of degassing are important for the accurate characterisation of fluid chemistry and the calculation of mineral saturation state in the fluid.



**Figure 2.4-7** Profile of the instantaneous carbon isotopic composition of the DIC and of the  $CO_2$  versus depth. This illustrates how the equilibrium carbon isotopic fractionation between the instantaneous DIC and  $CO_2$  changes from a small positive value at greater than 100 m depth to increasingly larger values at depths shallower than 100m and b) that the observed large negative isotopic fractionations are dominated by the degassing processes at shallow depths. From Assayag *et al.*, (2009).

Analysis of carbon isotopic fractionation during ascent of the fluid by Assayag et al., (2009) concluded that degassing must occur at shallow depths <100m inferred from the magnitude of the overall fractionation between DIC and CO<sub>2</sub> gas (Fig. 2.4-7). The average of the fractionation between CO<sub>2</sub>(g) and DIC ( $\Delta_{CO2-DIC} = \delta^{13}C_{CO2} + \delta^{13}C_{DIC}$ ) for all springs and geyser ranges from -4.8 to -7.5 % with an average of ~ -6.4 %. Isotopic fractionation resulting from CO<sub>2</sub> degassing of a solution will be dominated by exchange in both the system  $H_2CO_3^*$ - $CO_2$  and  $HCO_3^-$ - $CO_2$ . Given that H<sub>2</sub>CO<sub>3</sub><sup>\*</sup> is largely CO<sub>2</sub>(aq) fractionation will be dominated by isotopic exchange in the system  $CO_2(aq)-CO_2(g)$ , at  $pCO_2 > 1$  atm and by  $HCO_3 - CO_2$  at  $pCO_2 < 1$  atm (Fig. 2.4-2). This means that the overall fractionation of a degassing solution will change with depth of degassing due to changes in the speciation and thus the magnitude of the observed fractionation is an approximate indication of the depth at which degassing started. The results suggest that in-situ values of  $\delta^{13}C_{CO2}$  and  $\delta^{13}C_{DIC}$  are between 3.0 to 4.0 % and 2.0 to 3.0 % more positive and more negative respectively, depending on the measured surface  $\delta^{13}C_{CO2(g)}$  and  $\delta^{13}C_{DIC}$ , and the depth of the host reservoir. Recalculated values of  $\delta^{13}C_{CO2(g)}$  are used for further discussion of the carbon dioxide source. This also indicates that variation in the  $\delta^{13}C_{DIC}$  is overprinted by degassing effects and is thus not an accurate constraint on fluid-rock reactions occurring in the host aquifer.

## 2.4.3. CO<sub>2</sub> Sources for Springs

Possible geological processes that may generate high concentrations of  $CO_2$  gas in crustal reservoirs include (Cappa and Rice, 1995): 1) gases derived from mantle or magmatic sources; 2) the degradation of organic matter; 3) diagenetic reactions involving clay and carbonate rocks; and 4) thermal decarbonation of carbonate rocks by metamorphic processes.

The  $\delta^{13}$ C values of the CO<sub>2</sub> gas phase emitted by the Green River springs show little spread, ranging from -6.61 to -7.55 ‰ (1 $\sigma$  = 0.29‰) (Table 1.). This suggests a common source for all the escaping CO<sub>2</sub>, and implies that the flux of the CO<sub>2</sub> gas phase to the surface is sufficient to suppress transport related fractionation of the gas isotopic composition. However, degassing effects during fluid ascent imply a 3 to 4 ‰ fractionation on the original values of  $\delta^{13}C_{CO2(g)}$ , implying in-situ values in the region ~ -3 to -5 ‰. The  $\delta^{13}$ C of CO<sub>2</sub> is within the compositional range of mantle-derived carbon (-3 to -8 ‰ V-PDB, Wycherley *et al.*, 1999), but is also largely within the range of bulk crustal carbon (-5 to -7 ‰ V-PDB).

Discriminating between magmatic, crustal and biogenic sources of CO<sub>2</sub> is not possible with stable isotopes alone, because the ranges of  $\delta^{13}$ C in magmatic and crustal CO<sub>2</sub> are non-unique (Sherwood Lollar *et al.*, 1997). In contrast, <sup>3</sup>He is an unambiguous tracer of magmatic volatiles (Oxburgh *et al.*, 1986), and <sup>4</sup>He which is derived from radioactive decay of U, Th and K, elements concentrated in the crust, is a tracer of crustal components. Because the rate of He diffusion is relatively low in magmatic/crustal fluids (Ballentine, 1997), magmatic <sup>3</sup>He must be carried, or advected, into shallow systems. The carrier fluid is inferred to be CO<sub>2</sub> (e.g. Sherwood Lollar *et al.*, 1997). Differences in their production mechanisms and diffusivities partition <sup>3</sup>He and <sup>4</sup>He into terrestrial reservoirs with different concentrations. Mantle helium is dominated by primordial <sup>3</sup>He, with a <sup>3</sup>He/<sup>4</sup>He ratio (R) of 1 to 3 x 10<sup>-25</sup> and R/R<sub>air</sub> of 3 to 30. Crustal He, dominated by <sup>4</sup>He from a decay of U and Th has a radiogenic <sup>3</sup>He/<sup>4</sup>He ratio of 1 to 3 x 10<sup>-28</sup> or R/R<sub>air</sub> of 0:007 to 0.04 (Andrews, 1987). The clearest indication of a mantle-derived fluid is therefore shown by the presence of <sup>3</sup>He (Ballentine, 1997).

Because He is lost from the atmosphere, with a residence time of approximately  $10^6$  years, the concentration of <sup>3</sup>He in air is two orders of magnitude smaller than in typical magmatic gases (Oxburgh *et al.*, 1986). Helium is present within the atmosphere at only low concentrations (5 x  $10^{-6}$  vol/vol at STP; Ballentine *et al.*, 2002). The production mechanisms of crustally sourced CO<sub>2</sub> do not typically introduce additional <sup>3</sup>He and as such crustally sourced CO<sub>2</sub> has high CO<sub>2</sub>/<sup>3</sup>He ratios. CO<sub>2</sub>-rich groundwaters therefore have CO<sub>2</sub>/<sup>3</sup>He ratios dominated by the CO<sub>2</sub> source, with crustally sourced CO<sub>2</sub> systems having CO<sub>2</sub>/<sup>3</sup>He elevated relative to MORB (CO<sub>2</sub>/<sup>3</sup>He = 1 to 2 x  $10^9$ ).



**Figure 2.4-8** The majority of the CO<sub>2</sub>-springs have  $CO_2/{}^{3}$ He ratios above the MORB range indicating a predominantly crustal CO<sub>2</sub>-source (Sherwood Lollar *et al.*, 1997; Ballentine *et al.*, 2002). Also plotted is the data range from the deep CO<sub>2</sub> reservoirs documented by Gilfillan et al., (2006), from McCallum Dome, Sheep Mountain, Bravo Dome, McElmo Dome, Doe Canyon and St John's Dome. All error bars are smaller than printed symbols. Drawn after Gilfillan (2004).

Figure 2.4-8 shows  $CO_2/^3$ He ratios plotted against  $CO_2$  concentration for all of the major  $CO_2$  gas fields of the Colorado Plateau and the Green River  $CO_2$ -springs (Gilfillan, 2004). All of the samples from the major gas fields have  $CO_2/^3$ He ratios around the MORB range, distinct from the elevated  $CO_2/^3$ He ratios of at Green River. Many of these samples have elevated  $^3$ He/ $^4$ He. This indicates that the  $CO_2$  within all the major  $CO_2$  fields of the Colorado Plateau is dominated by mantle derived  $CO_2$  but implies a predominantly crustal source for the  $CO_2$  at Green River.

 ${}^{3}$ He/<sup>4</sup>He ratios of Gilfillan (2004) for Green River show a small variation from 0.224 to 0.256 Ra and CO<sub>2</sub>/ ${}^{3}$ He ratios are significantly elevated relative to MORB. Despite the distinctly crustal CO<sub>2</sub>/ ${}^{3}$ He ratios, measured  ${}^{3}$ He/ ${}^{4}$ He values are well above the expected 0.02 Ra of pure crust. This indicates either a small contribution of mantle derived CO<sub>2</sub> (1-15 %; c.f. Wilkinson *et al.*, 2007) diluted by large crustal contributions or the entrainment of atmospherically derived noble gases in the groundwater system. The observed CO<sub>2</sub>/ ${}^{3}$ He and  ${}^{3}$ He/ ${}^{4}$ He imply a predominantly crustal source for this CO<sub>2</sub>.

Heath (2004) concluded that the  $CO_2$  was sourced in the uppermost Palaeozoic section. Drilling reports from petroleum exploration in the vicinity of Green River document small accumulations of  $CO_2$ -rich fluid throughout the stratigraphy, within formations that include the Jurassic Navajo Sandstone, Permian White Rim Sandstone, Honaker Trail Hermosa Formation and within multiple clastic units of the predominantly evaporitic Pennsylvanian Paradox Formation. Of the deeper formations, the Mississippian Leadville Limestone is the most likely  $CO_2$  source, as it possesses a suitable clay and carbonate mineralogy, petrographic evidence of replacement and breakdown of carbonate to produce a high secondary porosity (Chidsey *et al.*, 2005) and is known to contain accumulations of free phase  $CO_2$  in other regions of the Paradox Basin (Cappa and Rice, 1995). Nuccio and Condon (1996) infer that the Leadville Limestone was heated to ~ 170 °C between ~ 70 and 38 Ma, temperatures thought sufficient to drive decarbonation reactions (e.g. Hutcheon and Abercrombie, 1990).

# 2.4.4. Hydrology and Fluid Geochemistry

#### 2.4.4.1 Water Sources for CO<sub>2</sub>-Springs

Aquifers within the Phanerozoic sequence include the Jurassic Entrada Sandstone, the Jurassic 'N-aquifer' dominated by the Navajo Sandstone but including the Wingate Sandstone and the Kayenta Formation, the Permian White Rim Sandstone and a Palaeozoic aquifer comprising the Lower Pennsylvanian and Mississippian limestone and dolomite formations (Fig. 2.2-2) (Hanshaw and Hill, 1969).

The N-aquifer is the dominant local aquifer and the temperatures of waters in the CO<sub>2</sub>springs and geysers (Table 1) are consistent with their derivation from depths appropriate to the local depth of the Jurassic Navajo Sandstone, assuming a constant thermal gradient of 22.1 °C/km (estimated from local bottom hole temperature measurements) and no conductive cooling as fluids ascend to the surface. The flow rates estimated in Chapter 3 imply a thermal Peclet Number ~ 1 and therefore, that there is limited advection of heat within the Navajo Aquifer where it shallows in the anticline at Green River. Uncertainty on the local heat flow and thermal conductivities (Bodell and Chapman, 1982) and the magnitude of advective heat transport result in temperature estimates for the slightly shallower Entrada Sandstone which overlap those of the Navajo Sandstone. However, the deeper aquifers of the White Rim Sandstone and the Pennsylvanian formations would be significantly hotter (> 40 °C). The similarity of fluid chemistry and isotopic composition, and the constancy of the superposition of fluid temperature with reservoir depths appropriate for the Navajo Sandstone suggest a common source reservoir for all the springs.

#### 2.4.4.2 Reservoir Geology

The Navajo Sandstone, along with the Wingate Sandstone and Kayenta Formation, forms the regionally extensive Lower Jurassic 'N-aquifer', of which the Navajo Sandstone is the most productive unit.

The aeolian Navajo Sandstone in the northern Paradox Basin is fine grained (0.1 to 0.25 mm) and is dominated by quartz (72–86 wt%) and K-feldspar (7–11 wt%) with minor amounts of plagioclase (3–6 wt%) and trace heavy mineral fractions of tourmaline, apatite and rutile (<1 wt%) (Beitler *et al.*, 2005; Bowen, 2004; Cooley *et al.*, 1969; Harshbarger *et al.*, 1957; Parry *et* 

*al.*, 2004). Primary quartz and feldspar grains are rimmed with hematite and goethite (Chan *et al.*, 2000) and feldspar grains are altered to illite, smectite and kaolinite (Zhu *et al.*, 2005, 2006). Authigenic illite is disseminated across both feldspar and quartz surfaces. Portions of the feldspar surface are locally altered to kaolinite and a  $1-3 \mu$ m thick layer of authigenic smectite. Diagenetic pore fillings of kaolinite, illite and smectite occur predominantly in larger pore spaces. Interstitial dolomite and calcite, and quartz overgrowths are present as sporadic cements.

# 2.4.4.3 Local Hydrology and Fluid Flow Paths

The Mesozoic and Permian aquifers are recharged seasonally from precipitation principally in the San Rafael Swell (Hood and Patterson, 1984). The distribution of hydraulic head in wells penetrating the Navajo Sandstone delineates groundwater flow paths from zones of recharge in the San Rafael Swell, southeast towards the centre of the basin, where artesian conditions prevail (Fig. 2.4-9; 2.4-10). Groundwater is subsequently discharged into both the Green and Colorado Rivers (Hood and Patterson, 1984).

Individual flow paths, which map the source of fluid feeding each spring, are taken as down-slope on the potentiometric surface in the Navajo Sandstone from the potentiometric height of the Green River Airport Well, the upstream spring (Fig. 2.4-11). Spring solute chemistries show a progressive change along these flow paths attributed to fluid-mineral reactions (see section 2.5.7). Tritium abundances for measured springs (Table 1) exhibit values within error of zero, providing a minimum age constraint of >60 yrs for the groundwater samples. This precludes significant mixing with shallow, modern groundwater. Fluid flow rates estimated in Chapter 3. imply groundwater transit times between the most up-stream spring (Green River Airport Well) and the most down gradient spring (Chaffin Ranch Geyser) on the order of ~10,000 years.



**Figure 2.4-9** Map showing the location of  $CO_2$ -charged springs, local geological structure and the relative saturation of groundwater within the Navajo Sandstone. Arrows indicate the direction of groundwater flow within the Navajo Sandstone defined by the topology of the potentiometric surface. Modified from Hood and Patterson (1984).







**Figure 2.4-11** Map illustrating the relationship between local structure and the potentiometric surface within the Navajo Sandstone. The northerly plunging Green River anticline is transected by the approximately east-west trending Little Grand Wash and Salt Wash fault systems. Flow paths are deflected by the normal faults where throws exceed ~100m. Structure contours are of the top surface of the Navajo Sandstone. Redrawn after Doelling (2002) & Dockrill (2005).

Flow is assumed to be homogeneous and springs are projected up to 6km laterally onto the  $\sim$  30 km flow path from the upstream Green River Airport Well (Fig. 2.4-11 & 2.4-17). Dockrill (2005) assessed sealing mechanisms on the Little Grand Wash Fault and northern fault of the Salt Wash Graben and concluded that cross-fault flow should occur at low throws (<100m), towards the fault tips but that the faults were sealed at higher throws (>100m), towards the axis of the Green River anticline, due to reservoir–non-reservoir juxtaposition and development of a

continuous clay smear. It is probable that the flow path through Crystal Geyser is deflected along the Little Grand Wash Fault and that flow paths are deflected along the northern margin of the Salt Wash Graben. Flow paths to Tumble Weed and Chaffin Ranch geysers pass through the fault tips of the Salt Wash Graben and, on the basis of the analysis of Dockrill (2005), should not be deflected. Below we show that data from the geysers on the north side of the Salt Wash Graben, as well as Ten Mile, Tumble Weed and Chaffin Ranch Geysers can be modelled as a continuous geochemical sequence although the extent to which this results from comparable hydrologies remains untested.

# 2.4.5. Fluid Geochemistry

## 2.4.5.1 Origin of the Fluid Isotopic Composition

The consistent  $\delta^{18}$ O and  ${}^{87}$ Sr/ ${}^{86}$ Sr ratios of the Green River spring waters suggest a common source for all ten springs (Table 1, Appendix A). The spring waters are initially of the Ca<sup>2+</sup>– Mg<sup>2+</sup>–HCO<sub>3</sub><sup>-</sup> type, where they flow from the recharge zone to the westerly limb of the Green River anticline (Fig. 2.4-12). The waters then evolve to Na<sup>+</sup>–HCO<sub>3</sub><sup>-</sup>–Cl<sup>-</sup> type as they ascend and cool in the anticline and mix with deeply derived brines.

Regionally, chloride concentrations in the Navajo Sandstone are low (0.1-1mmol/l) (Zhu, 2000), being derived from atmospheric inputs in recharge waters. Halite is not present in the Navajo Sandstone and is thus not a potential source of Cl<sup>-</sup> (Zhu, 2005). Elevated chloride concentrations in the Green River springs are attributed to input of basinal brines most probably associated with the inputs of CO<sub>2</sub>.

Heath (2004) shows that the spring waters lie close to the global meteoric water line on a plot of D/H versus  $\delta^{18}$ O, and attributed these fluids to a purely meteoric source. We interpret  $\delta^{18}$ O values ~ 2‰ more positive than local Green River surface waters (Mayo *et al.*, 2003) as resulting from mixing between the meteoric source and isotopically heavy brine (Fig. 2.4-13a), (c.f. Wilkinson *et al.*, 2008).

<sup>87</sup>Sr/<sup>86</sup>Sr ratios (Table 1.) in the Green River spring waters are elevated compared with formation waters from the Navajo Sandstone elsewhere (0.70976 1 $\sigma$  = 0.0007) (Spangler *et al.*, 1996). Strontium concentration versus <sup>87</sup>Sr/<sup>86</sup>Sr data (Fig. 2.4-13b) fall along a two component mixing hyperbola between Paradox Formation waters (Spangler *et al.*, 1996), with values close to that of Pennsylvanian seawater (0.7081 to 0.7087, Burke *et al.*, 1982), and a radiogenic end-member comprising silicate minerals in the host aquifer.



**Figure 2.4-12** Piper diagrams for the CO<sub>2</sub>-springs and basinal brine from the Paradox formation and Paleozoic Aquifers. Concentrations in mEq  $L^{-1}$ .

Assuming that chloride behaves conservatively and is derived solely from brine, the solute chemistry in each spring can be corrected for the brine input:

$$k_{c} = k_{s} - \left[\frac{\left(Cl_{s} / Cl_{B}\right) \cdot k_{B}}{1 - \left(Cl_{s} / Cl_{B}\right)}\right]$$
(2.27)

where  $k_c$ ,  $k_s$  and  $k_B$  are the corrected, spring and brine concentrations (mmol/l) of the *k*th element, respectively.  $Cl_s$  and  $Cl_B$  are the chloride concentrations in the spring and the formation brine. This is equivalent to treating brine inputs as an additional phase and allows the quantification of solutes derived from fluid-rock interaction alone (Fig. 2.4-17). Compilations of regional brine analyses are present in Appendix A.



**Figure 2.4-13** (a) Cross plot of oxygen and hydrogen stable isotopic compositions of the Green River springs (Heath, 2004), local surface waters (Mayo *et al.*, 2003) and Paradox Formation brine (Spangler *et al.*, 1996). The isotopic composition of the  $CO_2$ -charged springs is explained by mixing between isotopically light meteorically derived fluids with a small component of isotopically heavy basinal brine from the Paradox Formation. (b) <sup>87</sup>Sr/<sup>86</sup>Sr versus Sr<sup>2+</sup> concentration for the CO<sub>2</sub>-charged springs and Paradox Formation brine (Spangler *et al.*, 1996), showing mixing of strontium derived from brine with a composition close to that of Pennsylvanian seawater (Burke *et al.*, 1982) and a radiogenic end-member attributed to strontium derived from silicates in the host aquifer (Truini and Longsworth, 2003).

## 2.4.5.2 CO<sub>2</sub> Solubility and transport

Figure 2.4-14 depicts the maximum dissolved  $CO_2$  concentration in pore fluid through the stratigraphy of the Paradox Basin, in the vicinity of Green River. This model assumes a constant porewater temperature from the surface to where this intersects the geothermal gradient at the reservoir top. The local geothermal gradient is calculated as 21.2 °C/km based on bottom-hole temperature measurements from exploration well Pan American 1#, Salt Wash. Fluid salinities are based on measured values for the Navajo Aquifer system (Crystal Geyser water) and on a compilation of published analyses for fluids of the White Rim, Paradox Formation (Spangler *et al.*, 1996) and Paleozoic Aquifer systems. The solubility of  $CO_2$  was determined using the P, T and salinity dependent expressions of Duan *et al.*, (2006). Because of the interplay of increasing

temperature and pressure deeper into the subsurface, the solubility of  $CO_2$  in porefluid has a minimum at the surface and a maximum at between 500 and 900 m depending on the thermal profile and fluid salinities. Below this depth solubility decreases sharply at the transition from dilute meteoric aquifers to brine-rich aquifers with high salinities, due to the salting out effect (Duan *et al.*, 2006) and then continues to decrease slowly due to the effects of temperature. The transport of deeply derived  $CO_2$  in solution from the Paleozoic Aquifer to the shallow White Rim and Navajo Aquifers will be limited by the solubility of  $CO_2$  within the saline Paradox Formation brine – a maximum concentration of ca. 0.8 mol L<sup>-1</sup> can be expected in the brine rich formations and ca. 1.6 mol L<sup>-1</sup> in the shallower Navajo and White Rim Aquifers. If  $CO_2$  is transported in solution from the Paleozoic Aquifer, exsolution of a free phase is unlikely due to the increased solubility in the shallow aquifers due to salinity, temperature and pressure effects.



**Figure 2.4-14**  $CO_2$  solubility versus depth for a typical profile through the Green River anticline, and for different thermal profiles. See text for method of derivation and details of fluid compositions in the different aquifer systems.

## 2.4.5.3 Fluid Rock Reaction: Evolution of the Fluid Chemistry

Fluid chemistries of groundwater systems are controlled largely by the hydrolysis of rock forming silicate, aluminosilicate and carbonate minerals and to a lesser extent by the dissolution of halides and sulphates (Drever, 1997). Fluid-rock reactions in groundwater systems are driven by the dissolution and redistribution of  $CO_2$  which promotes mineral dissolution via the production and dissociation of carbonic acid. Shallow and/or young groundwater systems are dominated by reactions involving carbonate minerals, when present, due to the high solubility and rapid dissolution kinetics of these minerals. When there are no carbonates present, or saturation with respect to carbonate phases is reached, the ion chemistry will be controlled by the dissolution of silicate minerals. Determination of groundwater saturation state using PHREEQC (Parkhurst and Appello, 1999) indicates that groundwaters are undersaturated with respect to the predominant silicate minerals in the host aquifer; K-feldspar, albite and anorthite, and are oversaturated with respect to typical weathering product aluminosilicate minerals kaolinite, smectite and illite. Groundwaters are oversaturated with calcite and dolomite.

Silicate mineral dissolution reactions consume  $CO_2$  and increase the dissolved cation and bicarbonate concentrations. Alkalinity is therefore frequently invoked as a variable which reflects the extent of fluid-rock interaction (Plummer *et al.*, 1983) because it can increase concurrently with the base cations (Ca, Mg, Na, K) that are released during mineral dissolution. The stoichiometry of typical mineral dissolution reactions implies that alkalinity should show a 1:1 relation with respect to Ca + Mg + Na + K in equivalent when the water chemistry is regulated by the weathering of silicate and/or carbonates. Dissolution of halide and sulphate minerals does not affect alkalinity observed in the fluid chemistry of the CO<sub>2</sub> springs (Fig. 2.4-15) indicates that the dissolved solutes, in excess of those derived from brine inputs, are sourced predominantly from the dissolution of silicate and/or carbonates.

The fluid chemistry exhibits a systematic increase in Na<sup>+</sup>, K<sup>+</sup>, Ca<sup>2+</sup>, Sr<sup>2+</sup>, Al<sup>3+</sup> and <sup>87</sup>Sr/<sup>86</sup>Sr along the flow path attributed to feldspar dissolution (Fig. 2.4-17). In general, DIC and alkalinity increase down stream from Green River Airport Well due to the progressive addition of  $CO_2$  to the fluid along flow and the consumption of  $CO_2$  and H<sup>+</sup> during silicate hydrolysis.



Figure 2.4-15 Cross plot of field alkalinity versus the sum of the base cations corrected for brine derived  $N^+$  and  $K^+$  by subtraction of Cl<sup>-</sup>.

<sup>87</sup>Sr/<sup>86</sup>Sr is highest for the most up gradient spring, Green River Airport Well, which is devoid of brine inputs. <sup>87</sup>Sr/<sup>86</sup>Sr decreases to Crystal Geyser and Small Bubbling Spring reflecting brine inputs close to the site of these springs. <sup>87</sup>Sr/<sup>86</sup>Sr and Sr<sup>2+</sup> then increase progressively down stream reflecting increased proportions of silicate derived Sr<sup>2+</sup> in the fluid. This trend mirrors that observed for other silicate derived components. Tenmile Geyser lies off this trend in both <sup>87</sup>Sr/<sup>86</sup>Sr and Sr<sup>2+</sup> reflecting the high proportion of Sr<sup>2+</sup> rich, low <sup>87</sup>Sr/<sup>86</sup>Sr brine in this spring. On a plot of 1/Sr versus <sup>87</sup>Sr/<sup>86</sup>Sr the spring waters down stream of Small Bubbling Spring form an array reflecting increasing quantities of silicate derived Sr<sup>2+</sup> with increasing groundwater age and degree of fluid rock interaction (Fig. 2.4-16).



**Figure 2.4-16** Cross plot of 1/Sr versus <sup>87</sup>Sr/<sup>86</sup>Sr illustrating the effects of both fluid mixing and fluid-rock reaction on the composition of the groundwater.



**Figure 2.4-17** Solute chemistry versus distance along the modelled flow path. Little Grand Fault and the northern fault of Salt Wash Graben are located approximately 8 and 14 km along the flow path, respectively. Trends in the data are discussed in the text. Concentrations of  $N^+$  and  $K^+$  are corrected for brine additions. Na<sup>+</sup> and K<sup>+</sup> error bars are uncertainty after correction for brine inputs (Appendix A) and analytical uncertainties for all other solutes. For cations and <sup>87</sup>Sr/<sup>86</sup>Sr both 2006 and 2007 data sets are presented. Values are generally within the measured uncertainties adding validity to the trends and suggest spring chemistries are temporally invariant. (DIC = Dissolved Inorganic Carbon, [Alk] = Alkalinity (mEq/l).

The primary Mg<sup>2+</sup> source is diagenetically early dolomite cement ubiquitous to aeolian Jurassic sediments of the Paradox Basin (Desborough and Poole, 1992). Mg<sup>2+</sup> initially increases during the earliest portions of the flow path, interpreted to reflect dissolution of dolomite. Increases in Mg<sup>2+</sup> along various portions of the flow path are match by relative increases in Sr<sup>2+</sup> and decreases in <sup>87</sup>Sr/<sup>86</sup>Sr, which reflect Mg<sup>2+</sup> liberation from dolomite dissolution. Further along flow Mg<sup>2+</sup> concentrations are variable suggesting its concentration is largely regulated by precipitation of secondary weathering products.

The SiO<sub>2</sub> content decreases sharply as fluid flows from the Green River Airport Well, which samples deeper, warmer  $(27 \,^{\circ}\text{C})$ , fluids on the NE limb of the Green River anticline, to springs along the crest of the anticline which consistently sample cooler fluids  $(16-18 \,^{\circ}\text{C})$ . On the projected profile (Fig. 2.4-17), pH shows a minimum at Green River Airport Well and increases to Crystal Geyser, decreases to Small Bubbling Spring and then increases at a decreasing rate in geysers downstream of Small Bubbling Spring. This is interpreted to reflect injection of CO<sub>2</sub> at, or upstream, of Green River Airport Well and near Small Bubbling Spring on the northern margin of the Salt Wash Graben. The downstream increase in pH is interpreted to reflect progressive neutralization of this acidity by dissolution of silicate minerals.

# 2.4.5.4 CO<sub>2</sub> Degassing: In-situ DIC and pH

The measured pH and DIC may not directly reflect the in-situ values of these quantities if extensive CO2 degassing has taken place as fluids ascend to the surface. Elucidation of the true in-situ values of these quantities is important for the interpretation of the fluid-rock interaction histories of these groundwaters and for the correct determination of mineral saturation state. Without direct measurement of the fluid and gas flux in each spring or isotopic constraints on the degassing process (from for example an inert tracer such as noble gases) it is impossible to precisely constrain the degree of CO2 degassing in individual springs. As has previously been discussed (section 2.4.2.2) stable isotopic constraints imply degassing takes place in the shallower portions of each spring. This implies that saturation with respect to CO2 in the ascending fluid is not reached until some finite depth (unless fluid velocities are very fast relative to the critical overstep in saturation required for bubble nucleation and growth) and that fluids are not saturated with CO2 at reservoir conditions. However, the in-situ solubility of CO2 at the site of each spring is a readily calculable quantity and provides a maximum constraint on the degree of CO2 degassing experienced by each spring.

Calculation of the maximum in-situ  $CO_2$  solubility for each spring was made using the model of Duan *et al.*, (2006) and analyzed fluid chemistries, at reservoir depths estimated from the fluid emanation temperature or from well constraints, where available. In-situ pH,  $SI_{cc}$  and  $pCO_2$  were then calculated in PHREEQC (Parkhurst and Appello, 1999) using the modeled DIC,

analyzed water compositions and field alkalinity (Fig. 2.4-18). Measured values of alkalinity provide an important constraint on in-situ pH and calcite saturation, being unaffected by the degassing process. If alkalinity of the groundwaters was controlled purely by equilibria in the carbonate system (i.e. by equilibrium between  $CO_2(aq)$ ,  $HCO_3^-$  and calcite) the decrease in the modeled  $CO_2$  solubility with distance along the flow path would impose a decrease in alkalinity also. This is not observed in the field measurements and thus alkalinity, and subsequently pH, must be elevated by progressive fluid-rock reaction along the flow path. The trends in in-situ DIC and pH with distance along the flow path mirror those observed in the measured values of these quantities. These calculated  $CO_2$  solubilities are a maximum for individual springs. Whilst the actual in-situ  $CO_2$  concentrations maybe somewhere close to, or below saturation this provides an upper limit on the degree of  $CO_2$  degassing experience by each spring (Table. 2.4-1) and a minimum possible value for in-situ pH. Importantly, elevated  $CO_2$  concentrations at the measured values of alkalinity lower mineral saturation in the fluid through a reduction in pH (Fig. 2.4-18). However, absolute changes in in-situ pH remain a result of progressive fluid-rock reaction and pH neutralization through hydrolysis reactions.



**Figure 2.4-18** In-situ DIC, pH and  $pCO_2$  and the resulting  $SI_{cc}$  calculated using the Duan *et al.*, (2006)  $CO_2$  solubility model and PHREEQC.

Well	Modelled DIC	Measured DIC	% Degassed
	mmol L <sup>-1</sup>		
Crystal Geyser	1334	107	92
Torreys Spring	411	112	73
Tenmile Geyser	1079	83	92
Pseudo-Tenmile Geyser	617	93	85
Chaffin Ranch Geyser	239	100	58
Green River Airport Well	1537	76	95
Big Bubbling Spring	1215	116	90
Small Bubbling Spring	1298	119	91
Side Seen Big Bubbling	1288	119	91

**Table 2.4-1** Measured DIC versus DIC calculated for  $CO_2$ -saturation at reservoir depth, and the implied degree of CO2 loss through degassing.

737

98

87



Figure 2.4-19 Calcite and plagioclase saturation indices for the measured spring compositions (black squares) and the compositions recalculated for  $CO_2$  saturation in the host reservoir (open symbols).

# 2.4.6. Thermodynamic Constraints on Fluid-Rock Reaction

**Tumble Weed Geyser** 

Although a weathering process must be regarded as a nonequilibrium process, a common approach to obtain information on the regulation of natural water composition is through equilibrium calculations. In principle this approach is valid since an irreversible pathway as a whole may be seen as a series of consecutive reactions each of which is in equilibrium with the next (Wernberg, 1998). Besides their relative simplicity, the equilibrium models always show the direction towards which the system is striving.

One of the most common applications of equilibrium models is to relate analysed concentrations of different species to stability diagrams of some selected minerals. If the analysed species are approximately located along the boundary of two different phases, these phases are interpreted as concentration controlling. In order to define the different equilibrium model

systems (Figs. 2.4-20 to 2.4-23) a certain number of chemical species, i.e., components, were chosen (see Ingri, 1978). These components,  $H^+$ -SiO<sub>2</sub>(aq)-Al<sup>3+</sup>-Na<sup>+</sup>-K<sup>+</sup>-Mg<sup>2+</sup>-Ca<sup>2+</sup>-H<sub>2</sub>CO<sub>3</sub>, are the minimum number of chemical species required to describe the composition of all phases and solute species (after Marini, 2007). H<sub>2</sub>O is not considered since its activity is set to unity in the calculations. The anions Cl<sup>-</sup> and SO<sub>4</sub><sup>2-</sup> are not considered since they are not included in the silicate minerals.

It should be noted that the application of equilibrium constants of silicate minerals to natural water model systems is associated with some difficult problems. First, the equilibrium constants are usually not experimentally obtained but extrapolated using data (e.g. heat capacities, entropies) from elevated temperatures. In some cases even the thermodynamic data at elevated temperatures are estimated. Secondly, the silicate phases occurring in nature are not idealized pure phases, but instead solid solutions are ubiquitous. Thus inferences about controlling reactions in groundwater systems based on activity diagrams are a general guide at best. The superposition of groundwater composition outwith a specific mineral field does not always imply that that mineral may not form or be an important buffer of composition.

The concentration of dissolved silica, derived from the dissolution of silicate minerals, is controlled by equilibrium with an amorphous silica phase in the majority of springs (Figs. 2.4-20). Theoretically dissolved silica may be either controlled by kinetic factors during the dissolution of silicate minerals or by precipitation of secondary minerals. It has been noted in several studies (e.g. Barnes and Hem, 1973; Paces 1978) that secondary silica formation in low temperature groundwaters typically involves amorphous forms of silica, with variable solubilities (between chalcedony and true amorphous silica), rather than direct precipitation of quartz. Although, tentatively the dissolved silica may be controlled by a more soluble silica phase or by the transformation of K-feldspar and smectite to illite at higher temperatures (Aagaard and Helgeson, 1983).



**Figure 2.4-20** The  $aSiO_2(aq)$  as a function of temperature showing the superposition of measured values with the stability boundaries for chalcedony (for the low temperature springs) and for the reaction of K-feldspar and smectite to illite for Green River Airport Well.

Kaolinite and Ca-smectite are the dominant stable clay minerals (Fig. 2.4-21 to 2.4-23). Equilibrium with the aforementioned silica phases maintains most groundwater samples within the kaolinite stability field.  $Al^{3+}$  concentrations are essentially independent of pH suggesting a non equilibrium control on this species. Because  $aSiO_2(aq)$  is fixed by the precipitation of an amorphous silica phase, kaolinite will not regulate the dissolved  $Al^{3+}$  concentration (Deutsch, 1997) and its concentration will be regulated by the dissolution of silicate minerals.

Groundwater composition trajectories are from the stability field of smectite as waters at moderate temperature flow from depth up the NW-limb of the Green River anticline (Fig. 2.4-21). Accumulation of base cations and attenuation of pH as the fluids ascend induces trajectories towards the stability field of the dissolving silicate minerals (K-feldspar and plagioclase). Cooling of the fluid results in a decrease in solubility of the silica phase and results in a decrease in  $aSiO_2(aq)$ , moving the fluids into the stability field of kaolinite.

A second introduction of CO<sub>2</sub> further along the flow path suppresses silicate saturation in the fluid and they transpose vertically in  $aK^+/aH^+$ ,  $aNa^+/aH^+$ ,  $aCa^{2+}/(aH^+)^2$ ,  $aMg^{2+}/(aH^+)^2$ compositional space. Further dissolution of silicate minerals drives compositions back towards the silicate mineral stability fields. The groundwaters are oversaturated with respect to calcite and therefore secondary calcite formation is thermodynamically favourable (Fig. 2.4-24). However, numerous studies (e.g. Dreybrodt et al., 1992; Herman and Lorah, 1987, 1988; Lorah and Herman, 1988; Michaelis et al., 1985; Segnit et al., 1962; White, 1997) show that calcite does not precipitate instantaneously at the point of saturation. Precipitation requires a finite supersaturation because of activation barriers to calcite nucleation and crystal growth (White, 1997). Activation barriers may be accentuated by calcite inhibitor ions, e.g. Mg (Berner, 1975; Bischoff, 1968; Pytkowicz, 1965), or the presence of organic matter (Berner, 1975; Raiswell & Fisher, 2004). In most circumstances this implies a saturation index ( $SI_{CC}$ ) of +0.5, although Dreybrodt et al. (1992) suggest that saturation indices of at least +1.0 are required. The measured spring compositions fall within this +0.5 to +1.0 range.  $pCO_2$  recalculated for reservoir CO<sub>2</sub> saturation (section 2.4.5.4) displaces  $SI_{CC}$  to values of undersaturation in the upper portions of the flow path, moving to saturated to moderately saturated in the later portions of flow.



**Figure 2.4-21** Activity-activity diagrams for Na<sup>+</sup>, Ca<sup>2+</sup> and K<sup>+</sup> at 25 °C for the CO<sub>2</sub>-springs (modified after Helgeson *et al.*, 1969), showing generalized mineral stability boundaries aassuming that the *activity* of aqueous SiO<sub>2</sub> is fixed by equilibrium with chalcedony. Blue path is the generalized trajectory for the evolution of the fluid along the length of the flow path. Lower in-situ pH would depress data points to lower values of log(aX/aH<sup>+</sup>).



**Figure 2.4-22** Alumino-silicate phase stability diagrams for Na<sup>+</sup>, Ca<sup>2+</sup> and Mg<sup>2+</sup> at 25 °C. Approximately linear correlations with slopes of 1:1 and 2:1 are characteristic of groundwater systems where Na<sup>+</sup>, Ca<sup>2+</sup> and Mg<sup>2+</sup> aqueous activities are regulated by silicate dissolution reactions (Helgeson, 1969, 1970; Norton, 1974). Kaolinite and a Ca-rich smectite are the most thermodynamically favored reaction products.



**Figure 2.4-23** Alumino-silicate phase stability diagrams at 25 °C for all the potential low temperature reaction products (modified after Marini, 2007).



**Figure 2.4-24** Calcite saturation index as a function of  $pCO_2$  for measured  $CO_2$ -spring water analyses (black squares) and for the modelled in-situ values (open symbols). The solid horizontal line at  $SI_{cc} = 0$  describes water in equilibrium with calcite, while the dashed horizontal lines indicate kinetic thresholds for dissolution and precipitation (White, 1997). Vertical lines labeled 'atmosphere' represent  $pCO_2$  at sea level (1 atm total pressure).

## 2.4.7. Redox Conditions

Groundwaters typically contain Fe concentrations in the region of 5  $\mu$ mol L<sup>-1</sup> (Drever, 1997) but values as high as 2000  $\mu$ mol L<sup>-1</sup> have been reported in reducing groundwater systems (Deutsch, 1997) due to the increased solubility of Fe phases in reduced and acidic fluids (e.g. Welham et al., 2000). Analysed spring waters have Fe concentrations in the range 60 to 270  $\mu$ mol L<sup>-1</sup> and Mn concentrations in the range 2 to 30  $\mu$ mol L<sup>-1</sup>.

Measured Eh values for spring waters are in the range 6 to  $-42 \pm 3$  mV, indicating that the groundwater system is in a reduced state and that Fe and Mn are predominantly present in 2+ oxidation state (Fig. 2.4-25a). Superposition of measured Eh, pH and aFe<sup>2+</sup> indicate that dissolved iron concentrations are largely controlled by equilibrium with an iron oxide phase (Fig. 2.4-25b) with a solubility close to that of hematite or goethite (see Appendix C for a complete discussion) via the reductive dissolution reaction at acidic pH:

or

$$Fe_2O_3 + 6H^+ + 2e^- \leftrightarrow 2Fe^{2+} + 3H_2O \tag{2.28}$$

$$FeOOH + 3H^+ + e^- \leftrightarrow Fe^{2+} + 2H_2O \tag{2.29}$$

It should be noted that various authors suggest caution in using Eh to quantify redox condition (e.g. Lindberg and Runnells, 1984). The difficulty in interpreting redox from Eh measurements results from using an equilibrium approach to describe a highly dynamic system (James and Bartlett, 2000). Eh is a simple measure, but it gives at best only qualitative assessment of water redox conditions because the Pt electrode may not respond to many important redox couples

(Lovely and Goodwin, 1998). Thus, a wide range of Eh has been observed for the same redox couple and, as a result, several redox reactions may be relevant within the same Eh range (Lovely and Goodwin, 1998).

In the absence of soluble phase redox couples such as  $SO_4^{2-}H_2S$  or  $CO_2-CH_4$  groundwater redox reaction potential is largely a function of the oxygen fugacity of the fluid (Drever, 1997).

Equilibrium redox potentials for the  $SO_4^{2-}H_2S$  and  $CO_2-CH_4$  redox couples are in the region of 0 to -200 mV and -200 to -500mV, respectively (Drever, 1997). Dissolved oxygen concentrations typically decrease within increasing depth and groundwater age (e.g. Edmunds, Miles and Cook, 1984; Lin-Hua and Atkinson, 1985). This is largely due to the interaction of the groundwater with organic rich sediments, reduced mineral phases and bacterial activity in the subsurface (Drever, 1997). Gas compositional analyses of Heath (2004) suggest that these groundwaters are largely free of dissolved  $CH_4$  or  $H_2S$ . However, circumstantial evidence in the form of a detectible odour of  $H_2S$  during large-scale eruptions of Crystal Geyser suggests that dissolved  $H_2S$  at least, may be present in small quantities in these groundwaters. This suggests that the groundwater redox reaction potential is largely controlled by the dissolved oxygen content of the fluid (and possibly by the presence of trace  $H_2S$ ), whilst the measured redox potential is determined by the  $Fe^{3+}/Fe^{2+}$  redox couple.

Effused spring water interacts with the atmosphere accumulating dissolved oxygen such that Fe moves from the ferrous to ferric state and as a result of the change in relative solubility is removed from solution:

or

$$4Fe^{2+} + 3O_2 + 6H_2O \rightarrow 4Fe^{3+} + 12OH^- \rightarrow 4Fe(OH)_3 + 4H_2O$$
(2.30)

$$4Fe^{2+} + 3O_2 + 6H_2O \to 4Fe^{3+} + 12OH^- \to 2Fe_2O_3 + 6H_2O$$
(2.31)

Fe is precipitated as goethite or hematite. Reprecipitated Fe imparts a distinctive ochre colour to the precipitated carbonate in travertines.



**Figure 2.4-25** a) Equilibrium phase diagram, calculated using CHNOSZ (Dick, 2008), for iron oxidehydroxides and sulphides in the system FeCSOH and MnCSOH at  $18^{\circ}$ C;  $aCO_2 = -1.4$ ,  $aS_{TOT} = -2.4$  and  $aFe_{TOT}$  at -3 and -7. b) As above but including equilibrium boundaries for Mn-oxides and aqueous species, and data points for the measured values of Eh and pH for each spring. Some scatter in the data is attributed to CO<sub>2</sub> degassing and the incorporation of atmospheric O<sub>2</sub> in the surface layers of the spring waters.

# 2.4.8. Time Series Fluid Chemistry: Crystal Geyser

Modern eruptions of Crystal Geyer exhibit a bimodal pattern of size and frequency with short duration (~20 minutes), low flux (~0.17 kg/sec CO<sub>2</sub>) eruptions occurring approximately every 8 hours and large explosive eruptions (~4.2 kg/sec CO<sub>2</sub>) occurring every 22 hours, lasting on average 115 minutes (Gouveia and Friedmann, 2006).

Time series fluid chemistry from Crystal Geyser exhibits two distinct compositional patterns which are related to changes in the style of fluid and gas effusion (Fig. 2.4-26). During the build-up period to a large-scale eruption small-scale 'bubbling events' occur periodically (five small scale 'bubbling events' occurred during the sampling period, at regular 25 minute intervals) and fluid chemistry evolves towards increasing Na-K-Cl-SO<sub>4</sub> rich and Ca-Mg-Sr-Fe-Mn poor compositions. During a large-scale eruption this trend reverses and the fluid chemistry then changes systemically through the course of the eruption (with the sampled eruption lasting two hour and ten minutes).

The major changes in solute chemistry during this period are a systematic decrease in the Na<sup>+</sup>, K<sup>+</sup>, Cl<sup>-</sup>, SO<sub>4</sub><sup>2-</sup>,  $\delta^{18}$ O, DIC, <sup>87</sup>Sr/<sup>86</sup>Sr and an increase in Ca<sup>2+</sup>, Mg<sup>2+</sup>, Sr<sup>2+</sup>, Fe<sup>2+</sup>, Mn<sup>2+</sup> and  $\delta^{13}$ C<sub>DIC</sub>. Systematic changes in Cl<sup>-</sup> and  $\delta^{18}$ O through both portions of the geyser cycle are interpreted to reflect two-component end-member mixing between a saline, isotopically heavy Na-K-Cl-SO<sub>4</sub> type fluid (representing the 'typical' groundwater previously discussed; a mixture of meteorically derived formation fluid and deeply derived Paradox Formation brine) and an isotopically light, dilute Ca-Mg-Sr-Fe-Mn type fluid (representing 'typical' groundwater without addition of brine, similar to that of the fluid expelled from the Green River Airport Well further up the flow path) (Fig. 2.4-17). Cl<sup>-</sup> versus  $\delta^{18}$ O defines a hyperbolic mixing line (Langmuir *et al.,* 1978).This hyperbola lies as a mixing curve between an isotopically light, dilute meteoric end-member and an earlier mixture of dilute meteoric fluid and isotopically heavy, saline brine. Thus, the chemistry changes observed in Crystal Geysers largely represent the dilution of metaorie.

Cross plots of major cations and anions versus Cl<sup>-</sup> define approximately linear trends. Linear trends of decreasing Na<sup>+</sup>, K<sup>+</sup> and SO<sub>4</sub><sup>2-</sup> with decreasing Cl<sup>-</sup> reflect dilution of a high Na/Cl, K/Cl and SO<sub>4</sub>/Cl fluid with increasing proportions of a dilute, isotopically light, Mg-Ca-HCO<sub>3</sub><sup>-</sup> end-member. Approximately linear trends of increasing divalent cation (Ca<sup>2+</sup>, Mg<sup>2+</sup>, Sr<sup>2+</sup>, Fe<sup>2+</sup>, Mn<sup>2+</sup>) concentrations with decreasing Cl<sup>-</sup> reflect dilution of the pre-eruption water with increasing proportions of the Ca-Mg-HCO<sub>3</sub> end-member. Increase in these cation concentrations reflects that fact that the divalent cation/Cl of the Ca-Mg-HCO<sub>3</sub> end-member are greater than that of the Na-K-Cl type pre-eruption waters.


degassing process. c) Schematic diagram of Crystal Geyser and Little Grand Fault showing the hypothesised view of groundwater mixing as a result of

fluid ejection during geysering.

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**Figure 2.4-27** Times series solute and isotope geochemistry for the time series samples of Crystal Geyser. Dashed line is the eruption height (m), solid line are the solute or isotope values.



**Figure 2.4-28**  $\delta^{18}$ O versus Cl<sup>-</sup> for all the CO<sub>2</sub>-springs (blue squares) and for the time series samples of Crystal geyser (red squares) showing the least squares hyperbolic fit to the data (Langmuir *et al.*, 1978). The figure demonstrates the mixing between two end-member fluids: a saline brine with high Cl<sup>-</sup> and heavy  $\delta^{18}$ O; and dilute meteoric fluid with low Cl<sup>-</sup> and light  $\delta^{18}$ O. The Crystal geyser samples are a further dilution of a mixture already formed from these end-members, with a third lighter meteoric end-member. Differences in the  $\delta^{18}$ O of the meteoric end-members is interpreted as reflecting variability in the  $\delta^{18}$ O of rainwater through the Holocene (c.f. Zhu, 2000)



Figure 2.4-29 Cl<sup>-</sup> versus major solute chemistry for the time series samples of Crystal Geyser.



**Figure 2.4-30** Cross plots of Sr<sup>2+</sup> and <sup>87</sup>Sr/<sup>86</sup>Sr versus Mg/Ca illustrating the derivation of low <sup>87</sup>Sr/<sup>86</sup>Sr Sr, Ca and Mg from dolomite dissolution.

The magnitude of the variation in <sup>87</sup>Sr/<sup>86</sup>Sr observed in the time series samples (0.712524 to 0.712729, n = 17) is small compare to the observed range in <sup>87</sup>Sr/<sup>86</sup>Sr observed between all samples (0.711755 to 0.713327, n = 10). <sup>87</sup>Sr/<sup>86</sup>Sr decreases 1) through the course of an eruption, 2) with decreasing Cl<sup>-</sup> and 3) with increasing Sr<sup>2+</sup> concentration. The hyperbolic mixing trends between <sup>87</sup>Sr/<sup>86</sup>Sr and various cations implies; a) the pre-eruption fluid has <sup>87</sup>Sr/<sup>86</sup>Sr higher than the Ca-Mg-HCO<sub>3</sub> end-member. b) trends in <sup>87</sup>Sr/<sup>86</sup>Sr versus major cations reflect mixing between the two fluid end-members and the dilution effects previously discussed. C) <sup>87</sup>Sr/<sup>86</sup>Sr decreases with increasing Sr<sup>2+</sup>. The lower <sup>87</sup>Sr/<sup>87</sup>Sr and higher Sr, Ca and Mg of the Ca-Mg-HCO<sub>3</sub> end-member are attributed to a higher proportion of carbonate derived from dissolution of dolomite in the host aquifer, in the earlier portions of the flow path (Fig. 2.4-30).

Temperature measurements of Gouveia and Friedmann, (2006) using rugged thermistors record systemic variations in temperature of the effused fluid during the build up to an eruption, and through the course of an eruption, which are generally consistent with our measurements of temperature variation. Time series measurements reveal a gradual but systematic increase in temperature of ~ 1.5 °C from 17 °C to 18.5 °C at the onset of eruption. During the course of an eruption temperature decreases systematically from the pre-eruptive maximum (18.7 °C) to close to the pre-eruptive minimum (16.6 °C), at the end of the eruption. These systematic temperature variation may thus be related to mixing of two distinct water bodies of different temperature, and from different depths. This temperature variation is equivalent to a ~ 85 m variation in the depth of the source fluid. The Navajo Sandstone is ~ 95 m thick in the vicinity of Crystal Geyser (Green River Unit 1#). Differences in the densities of the fluid end-members may impart differences in the hydrodynamics of these fluids and stratification within the host reservoir. It can thus be

inferred that the Na-Cl type end-member is sourced from deeper portions of the formation and the  $Mg-Ca-HCO_3^{-1}$  from shallower (Fig. 2.4-26).

This variation in fluid chemistry and temperature is interpreted to reflect the drawing in and mixing of distinct water types within the near wellbore region, within the host aquifer. It seems likely that these fluid mixing processes are in part stimulated by the excess (e.g. a fluid flux greater than that driven by hydraulic head) of fluid withdrawn from the aquifer during geysering. This rapid fluid effusion is driven by the buoyant uplift and explosive ejection of fluid from the well by rising CO<sub>2</sub> bubbles (Lu et al., 2005; 2006; Pruess, 2006, 2008). This results in a rapid decline in the height of the column of fluid sitting in the well, causing a pressure perturbation in the reservoir itself, which must impose increased fluid velocities in the subsurface. The observed pattern of fluid mixing implies that CO<sub>2</sub>-charged brines influx into the Navajo Aquifer in close proximity to Crystal Geyer, on the timescale of the geysering events. It suggests that the geysering processes itself acts as an active groundwater pump, stimulating the vertical migration of fluid between reservoir and leakage to the surface.

The presence of an active flux of  $CO_2$ -charged brine from a reservoir deeper than the Navajo Aquifer can be assessed from information on the effusion of  $CO_2$  and fluid from Crystal Geyser. The rate of  $CO_2$  effusion from Crystal Geyser has been measure as ~11,000 t/a (tones per annum) (Gouveia *et al.*, 2005; Gouveia and Friedmann, 2006). The presence of a continuous free gas phase close to the site of Crystal Geyser is improbable as this well is close to the apex of the anticline and would thus be likely to directly penetrate any buoyantly accumulated gas cap. However, the exsolution of small volumes of  $CO_2$  within the host aquifer may occur due to the depression of  $CO_2$  solubility as fluids ascend the anticline.

If the reservoir fluid was close to  $CO_2$  saturation (as it would likely be if an exsolved phase could be maintained) fluid entering the bottom of the Crystal Geyser well would degas instantaneously upon rising a short distance vertically. The geysering processes intrinsically requires that the point of gas exsolution be mobile and able to rise and fall vertically through the well (Fi.g 2.4-26), thus regulating the development of periodic, large-scale degassing events which drive large eruptions. A  $CO_2$ -saturated reservoir would degas continuously from the well base, producing a continuous violent gas stream and would not exhibit periodicity in eruption style or strength.



**Figure 2.4-31** Schematic diagram illustrating the accumulation of  $CO_2$ -charged brine at the intersection of the Little Grand Fault with the apex of the Green River anticline. Free phase  $CO_2$  may accumulate as isolated, capillary trapped bubbles due to the change in solubility as fluids ascend the anticline.

Measurement of the recovery rate of fluid within the well following a large eruption allows calculation of the fluid velocity (1.03 x  $10^{-4}$  m/sec) and volumetric fluid flux (1.17 m<sup>3</sup>/day). This value match closely with that expected for a pressure head driven fluid flux calculated using the equations of Bernoulli, and is equivalent to the artesian fluid flux. Additional fluid is expelled from the well during large eruptions due to the buoyant uplift of water by large, rising gas bubbles. The rate of water flux from Crystal Geyser during large-scale eruptions was measured in the early 1970's (although the method was not specified) and was reported by Baer and Rigby (1978) as 27.5  $\pm 2$  m<sup>3</sup>/hr, with eruptions lasting on average 4.25 hours. However, anecdotal evidence suggests that the modern flux has decreased since this measurement (Waltham, 2001; Fig. 2.2-6), possibly due to reduction in local hydraulic head as a result of fluid and pressure depletion in the surrounding reservoir, or depletion of a CO<sub>2</sub>-charged fluid reservoir. Scaled to the duration of a modern eruption these flux estimates imply that in the course of an eruption  $60 \pm 3$  $m^3$  of fluid (or a 527m x 38cm column) is emptied from the well; equivalent to the entire well volume. Assuming that this flux was similar over the period prior to the flux measurements this implies that for the given reservoir thickness (95 m) and porosity (20%) a  $3.2 \pm 0.8$  km radius around the geyser was emptied of fluid prior to the 1970's and  $5.5 \pm 1.4$  km radius over the 74 year life of the geyser (scaling for the decrease in eruption length since the 1970's). This large volume of fluid effusion is most likely balanced by influx of fluid from aquifers below the Navajo Aquifer and from increase in the fluid velocity within the aquifer itself.

From eruption frequency data and the estimates of fluid and gas expulsion during eruptions and the background fluid and gas flux during periods of quiescence, annual estimates of the CO<sub>2</sub> and water discharge, and the yearly, average CO<sub>2</sub> concentration can be made. Average annual CO<sub>2</sub> emissions range from 5694  $\pm$  1708 t/a to 12702  $\pm$  3810 t/a using upper and lower limits for the CO<sub>2</sub> flux observed in individual, large eruptions and uncertainty estimates in the sampling method (Gouveia *et al.*, 2005). Estimates of fluid flux during periods of eruption and quiescence yield 2.7x10<sup>4</sup> m<sup>3</sup>/a and 368 m<sup>3</sup>/a, respectively. This results in average CO<sub>2</sub> concentrations of ~4 to 10 mol L<sup>-1</sup>, greatly exceeding the maximum solubility of CO<sub>2</sub> in the Navajo Aquifer. This strongly implies that CO<sub>2</sub> must be added to the Navajo Aquifer close to the site of Crystal Geyser.

## **2.5.** Conclusions

Crustally sourced CO<sub>2</sub>, produced from diagenetic reactions in the Leadville Limestone, at depth within the Paradox Basin, migrates vertically through the stratigraphy mixing with and dissolving into basinal brines of the Paradox Formation. These CO<sub>2</sub>-charged brines migrate along the Little Grand and Salt Wash fault systems into the shallow White Rim and Navajo Aquifers where they mix with meteorically derived groundwaters, flowing along hydraulic gradients from zones of recharge in the San Rafael Swell to zones of discharge near the confluence of the Green and Colorado Rivers. This passive migration of CO<sub>2</sub> is analogous to leakage of a deep geological CO<sub>2</sub> reservoir into shallower aquifer systems. CO<sub>2</sub> entering the shallow groundwater systems suppresses pH and mineral saturation in the fluid promoting dissolution of silicate and carbonate minerals in the host aquifer. The introduction of this high partial pressure  $CO_2$  gas increases the capacity to accept dissolved solids by lowering the pH and the saturation state of the groundwater, enhancing mineral dissolution. As a result, the CO<sub>2</sub>-rich groundwaters can evolve towards very high solute concentrations after prolonged water-rock interaction. In geological  $CO_2$ storage sites this processes will ultimately enhance the fluids capacity to accept dissolved CO<sub>2</sub>, through ionic complexing, thereby enhancing solubility trapping. With progressive flow through the aquifer the hydrolysis of plagioclase and K-feldspar consume H<sup>+</sup>, releases solutes and alkalinity to the solution driving the groundwaters towards saturation with respect to these phases. pH attenuation and elevation in mineral saturation will ultimately reduce the reactively of migrating CO<sub>2</sub>-charged fluids reducing the rate of corrosion of caprocks and fault seals encountered by the migrating plume. Thermodynamic constraints imply that the dominant reaction products are smectite, kaolinite and chalcedony. Importantly equilibrium with chalcedony fixes  $aSiO_2(aq)$ , maintains groundwater compositions in the stability field of kaolinite and prevents kaolinite equilibrium from regulating  $Al^{3+}$ .

The CO<sub>2</sub>-charged groundwaters contain high quantities of dissolved  $Fe^{2+}$  and  $Mn^{2+}$ . Superposition of Eh, pH and  $aFe^{2+}$  suggests that the redox sate of the fluid is controlled by low oxygen fugacity and fixed by the  $\text{Fe}^{3+/}\text{Fe}^{2+}$  redox couple through equilibration with hematite. This has important implications for the mobilization and transport of metals in CO<sub>2</sub> storage sites and is analogues to iron mobilization processes recently observed at the Frio test CO<sub>2</sub>-injection site (Hovorka *et al.*, 2006; Karaka *et al.*, 2006; Smyth *et al.*, 2009). This suggests that, even in the absence of an additional reductant, deep O<sub>2</sub> depleted groundwaters in CO<sub>2</sub> storage sites will derive high metal concentrations from the pH suppression induced by large quantities of dissolved CO<sub>2</sub>.

Cold water geysering of Crystal Geyser, driven by  $CO_2$ -degassing, causes pressure depletion in the Navajo Aquifer. This stimulates influx of  $CO_2$ -charged brines from deeper formations, on the time-scale of the geysering events, which mix with chemically distinct fluids in the host aquifer. The physical process of  $CO_2$  gas-driven geysering is therefore an important mechanism for the stimulation of vertical fluid and gas migration in the subsurface and will be important for prolonging effusion from leaking wells in  $CO_2$  storage sites.

## **Chapter 3 Silicate Mineral Dissolution Kinetics**

## **3.1. Introduction**

The majority of estimates of field-based mineral dissolution rates have previously been determined by mass balance techniques in soil profiles and watersheds (reviewed in Drever and Clow, 1995; White and Brantley, 1995; White and Brantley, 2003), at surface pressure and temperature conditions. A smaller number of studies have focused on understanding reaction rates in natural porous media (e.g. Brantley *et al.*, 2001; Hereford *et al.*, 2007; Keating and Bahr, 1998; Kenoyer and Bowser, 1992a, 1992b; Kim, 2002; Maher *et al.*, 2006; Malmstrom *et al.*, 2002; Rowe and Brantley, 1993; Zhu, 2000, 2005). Few attempts have been made to determine field scale reaction rates in clastic reservoirs with high  $pCO_2$  (Matter *et al.*, 2007).

In this chapter the groundwater chemistry, thermodynamic and hydrological modelling described in Chapter 2 is used, in conjunction with petrological observations and a compilation of published porosity and hydraulic conductivity measurements, to estimate rates of the controlling fluid-mineral reactions in the  $CO_2$ -charged groundwaters. The main results of this work were published by Kampman et al., (2009) and this chapter builds on this work. Emphasis is placed on the feldspar dissolution reactions, as they are likely to be the slowest and hence the most important in controlling reaction progress. Prior to this the most relevant aspects of the experiment studies of feldspar dissolution are reviewed with emphasis on aspects of fluid chemistry and the dissolution mechanisms relevant to the conditions expected in natural  $CO_2$ -charged groundwaters.

## **3.2. Review of Experimental Studies on Feldspar** Dissolution Kinetics

Dissolution rate experiments on feldspars have been conducted in three ways: 1) batch experiments (Amrhein & Suarez, 1992; Casey et al., 1991; Hamilton et al., 2001); 2) flow-through experiments (Berg & Banwart, 2000; Hellmann, 1994; Knauss & Wolery, 1986; Oxburgh et al., 1994); or, 3) surface titration experiments (Blum and Lasaga, 1991; Oxburgh et al., 1994). Fluid samples and effluents of the former two experimental methods were analysed for various elements, e.g. Al, Si, Na and Ca and, using this data, dissolution rates were calculated by mass

balance techniques. The latter was mainly used to derive reaction rate equations as a function of surface charge.

In general feldspar dissolution rates can be divided into three different pH-dependent regions (Fig 3.2-1) (Blum and Lasaga, 1991; Hamilton et al., 2001; Knauss and Wolery, 1986; Oxburgh et al., 1994): 1) low pH region (pH < 5): the dissolution rate decreases with increasing pH; 2) near-neutral pH region (pH 5 to 8): the dissolution rate shows no dependence on pH; 3) high pH region (pH > 8): the dissolution rate increases with increasing pH, though this pH dependence is less pronounced than for the "low pH" region. As temperature increases, the dissolution rates become more pH dependent in the acid and alkaline pH regions. The activation energy required for dissolution is also higher (~ 80 kJ/mol) in more acid and alkaline environments, than in the near-neutral pH region (~ 65 kJ/mol).



Figure 3.2-1 Laboratory dissolution rates for feldspars of different composition at various pH.

#### **3.2.1.** Dissolution Mechanism

The dissolution mechanism of the feldspar mineral surface has been a point of debate among various authors. Essentially, there are three main contentious aspects: 1) the surface-controlled dissolution reaction; important aspects of which include a) the reactive site density (Amrhein and Suarez, 1992; Holdren Jr. and Speyer, 1987), which in turn is related to the "reactive surface area", though not in a proportional manner; b) the formation of surface complexes (Brady and Walther, 1992; Hellmann, 1999; Oxburgh et al., 1994) c) mineral heterogeneities, e.g. more rapid dissolution of Ca-rich phases than Na- or K-rich phases (Casey et al., 1991; Inskeep et al., 1991); and 2) formation of a leached or altered layer at the mineral-solution interface (Amrhein and Suarez, 1992; Hellmann et al., 2003; Muir et al., 1990; Muir and Nesbitt, 1991; Nesbitt and Muir, 1988); and 3) formation of protective coatings at the crystal surface (Amrhein and Suarez, 1992; Berner and Holdren Jr., 1977; Nugent et al., 1998).

#### 3.1.1.1. Surface Controlled Reaction

Knauss and Wolery (1986), as well as Hamilton et al. (2001) and Berner and Holdren (1977), suggest that dissolution was controlled by the reactive site density due to non-uniform attack at the surface, preferentially at high energy crystal defects, along twin boundaries or at dislocations, which intersect the surface. However, Amrhein and Suarez (1992) have shown that the relation between dissolution rate and specific surface area is not a simple one, and though the density of reactive surface sites per unit area varies systematically with grain size, it does not do so in a linear way (Holdren Jr. & Speyer, 1985). Laboratory estimates of mineral surface areas are typically measured using the BET technique which relates the adsorption of a measured volume of inert gas (usually  $N_2$ ) to the mineral surface area (e.g. Gregg and Sing, 1982). Geometric estimates, considering idealized sediment grains, typically underestimate mineral surface areas by orders of magnitude, when compared to BET measurements, due to the effects of surface roughness and topology (e.g. Brantley *et al.*, 2000, White *et al.*, 1996). In naturally weathered materials surface roughness and thus total mineral surface area increases with the duration of weathering (White *et al.*, 2003) but how this relates to the total reactive surface area of the mineral is still uncertain.

Further complexity surrounds the formation of surface complexes on the mineral surface, prior to detachment and dissolution of the grain, which relate the surface dissolution mechanism to the solution pH. At low pH values the feldspar surface is positively charged due to the formation of  $\equiv$ Al-OH<sub>2</sub><sup>+</sup> surface complexes, and at high pH values  $\equiv$ Si-O<sup>-</sup> surface complexes are dominant, resulting in a negative surface charge. As a result of the formation of these surface complexes, at acid pH dissolution will be mainly concentrated at the Al-surface site, while, at alkaline pH, dissolution focuses on the Si-surface sites (Brady and Walther, 1989; Hellmann, 1999; Oxburgh et al., 1994). At near-neutral pH, however, the dissolution rate is independent of surface charge, as it is mainly occupied by neutral  $\equiv$ Si-OH and  $\equiv$ Al-OH surface complexes. Oxburgh et al. (1994) suggested that, at near-neutral pH, reaction occurs at neutral Al-surface sites, due to the fact that an Al-O-Si bond is weaker than a Si-O-Si bond (Hamilton et al., 2001).

Further, the role of compositional heterogeneity may introduce variable dissolution rates across the mineral surface. In general, it is suggested that the dissolution rate of feldspars increases with anorthite content (Casey et al., 1991; Oxburgh et al., 1994). This is related to the higher solubility of more Ca-rich feldspar compared to Na-rich feldspar. TEM imaging of a zoned labradorite by Inskeep et al. (1991) has shown that the more Ca-rich lamellae were dissolved preferentially over the more Na-rich ones. These mineralogical heterogeneities influence the measured dissolution rate significantly.

Hamilton et al. (2001) and Oxburgh et al. (1994) showed that the Al/Si ratio also affects the dissolution rate. For feldspars with varying Al content it is seen that the dissolution rate

increases with increasing Al/Si ratio (Hamilton et al., 2001). In addition, Hamilton et al. (2001) and Oxburgh et al. (1994) both concluded that variations in Al content among feldspars could explain the observed increase in dissolution rate going from albite to anorthite. This difference is explained by the difference in feldspar structure, which is related to the interconnection between AlO<sub>4</sub> and SiO<sub>4</sub> tetrahedra (Hellmann, 1999). Increasing the Al/Si ratio means replacement of Si atoms by Al atoms, which results in an increase in Si-O-Al bond length (Hamilton et al., 2001). As a result of this bond length increase AlO<sub>4</sub> tetrahedra are preferentially removed from the feldspar framework. Albite contains SiO<sub>4</sub> tetrahedra that are interconnected, and therefore the loss of AlO<sub>4</sub> tetrahedra will not affect the kinetics of surface SiO<sub>4</sub> tetrahedra detachment, i.e.  $\equiv$ Si-OH complexes, in albite. This is in contrast to anorthite, which contains completely isolated SiO<sub>4</sub> tetrahedra, and therefore anorthite dissolution requires only the breaking of, weaker, Al-O-Si bonds, instead of both Al-O-Si and Si-O-Si bonds, as is the case for albite dissolution (Hellmann, 1999).

#### 3.1.1.2. Leached Layer

The mineral surface dissolution of feldspar is also influenced by the formation of leached layers and precipitates. Coating of the feldspar grains by these layers is assumed to change the dissolution mechanism from transport-controlled to diffusion-controlled, as released ions must now first diffuse through the coating before being released to solution. Leached layers are the result of non-stoichiometric dissolution and near-surface alteration at acid to neutral pH, and are not generally observed at basic pH (Casey et al., 1988, 1991; Hellmann et al., 2003). Depth profiles of these altered zones typically show depletion in interstitial cations, i.e. Na, K, Ca, and framework elements, i.e. Al, retention of Si and O (Hellmann et al., 2003; Muir et al., 1990), and enrichment in aqueous species, i.e. H (Casey et al., 1988).

There is a significant difference between naturally formed leached layers and laboratory produced layers: naturally formed leached layers are Al-rich (Nesbitt and Muir, 1988), while laboratory produced layers are Si-rich (Hellmann et al., 2003; Inskeep et al., 1991; Muir et al., 1990). These altered layers usually have a thickness of several hundreds of angstroms, and this thickness may also vary with feldspar composition (Muir et al., 1990), increasing with increasing Al content. The mechanism of leached layer formation is thought to involve three consecutive steps (Chou and Wollast, 1985; Muir et al., 1990): 1) rapid replacement of Ca<sup>2+</sup> and Na<sup>+</sup> by H<sup>+</sup> or H<sub>3</sub>O<sup>+</sup>; 2) hydrolysis reactions, resulting in the breaking of Si-O-Al and Si-O-Si bonds preferentially and the depolymerisation of the silicate structure, eventually resulting in a Al-depleted layer; 3) slow dissolution of the residual layer at the solid-solution interface, together with diffusion of ions from the fresh feldspar surface, leading to steady state dissolution. This results in the formation of a layer composed of Si, O and H, most likely a hydrated silica gel, overlying the fresh feldspar mineral (Chou and Wollast, 1985; Hellmann et al., 2003; Muir et al.,

1990). The effect of this layer on inhibiting dissolution remains uncertain. Additionally, the presence of a cation depleted surface layer in highly weathered natural minerals may adversely influence BET or geometric estimates of the reactive mineral surface area, resulting in overestimation of the reactive surface of natural feldspars.

#### 3.1.1.3. Secondary mineral precipitation

Part of the discrepancy between laboratory and field-scale reaction rates may be explained by the presence of surface coatings formed by the precipitation of secondary minerals, which may influence the dissolution rates. Weathered minerals in nature are often coated by clays (Berner & Holdren Jr., 1977; Nugent et al., 1998; Zhu; 2005), organic material and oxyhydroxides of Al, Fe, and Mn. This coating can either be discontinuous (Berner & Holdren Jr., 1977; Nugent et al., 1998), or continuous. Even if the coating is discontinuous, as a result of its porosity or patchy distribution, it may affect the dissolution of the mineral where this is in contact with the coating rather than with the solution (Hodson, 2003).

Investigation of natural mineral coatings on feldspars (Berner & Holdren Jr., 1977; Nugent et al., 1998; Zhu, 2005) has shown that the weathering of feldspar minerals indeed results in the formation of a patchy hydrous coating consisting of aluminosilicates, e.g. kaolinite or other clay minerals. In spite of the presence of this clay-like coating the underlying feldspar showed the same textural features as laboratory weathered feldspar without a coating. Therefore, Berner and Holdren Jr. (1977) concluded that it is unlikely that the presence of this coating inhibited dissolution. However, they did not take into account the possibility that the observed dissolution textures, e.g. etch pits, could either have developed before the precipitation of the coating, or just developed more slowly below the coating (Hodson, 2003).

To investigate the effect of coatings on the dissolution rate of feldspar under conditions where effect of solution saturation state can be discounted Hodson (2003) studied the dissolution behaviour on anorthite in the presence of a, laboratory produced, Fe-rich coating. He concluded that the formed coating was porous, containing both meso- and micropores, and that this porous coating of secondary minerals did not inhibit the dissolution of the feldspar mineral, as the obtained dissolution rates were in the same order of magnitude as those for uncoated minerals. This also means that the presence of porous surface coatings on minerals does not explain the observed discrepancy between mineral dissolution rates obtained in the field and those in the laboratory.

A similar study was performed on anorthite (Murakami et al., 1998), but with different secondary mineral precipitates; boehmite, "modified" boehmite, and kaolinite, which are reaction products derived from the dissolving feldspar. Though their obtained dissolution rates were in the same order of magnitude as those for uncoated minerals, they concluded, on the basis of

calculated Gibbs free energies for anorthite dissolution, that the precipitation of secondary minerals promoted dissolution. They stated that, even though the dissolution rate decreased as a result of precipitation, the formation of the coating required elements present in solution, thereby reducing the saturation state of the fluid, and hence, promoting more dissolution of the feldspar.

#### **3.2.2.** Solution Composition

Other factors affecting the dissolution rate of feldspars are: 1) solution saturation state (Aagaard and Helgeson, 1977, 1982; Lasaga, 1981; Oeklers et al., 1994); 2) cations in solution, e.g. aqueous Al (Amrhein and Suarez, 1992; Muir and Nesbitt, 1991); and 3) ligand absorption, e.g. oxalate (Berg and Banwart, 2000; Blake and Walter, 1999), citrate (Blake & Walter, 1999), or carbonate (Berg & Banwart, 2000);

#### 3.1.1.4. Solution Saturation State

Within the framework of transition state theory (TST) (Lasaga, 1981), the rate of an elementary reaction is proportional to the concentration of the activated complex (or the energy maximum that the reactants should pass to be converted into products) and to the concentration of the surface species precursor of the activated complex (precursor complex) (Wieland et al., 1998). Although feldspar dissolution likely involves several elementary reactions, TST can still be applied to the overall rate if it is controlled by a single elementary rate-limiting step (Lasaga, 1981). Within this context, silicate dissolution rates can be described using (Lasaga, 1981):

$$r = k^{+} \prod a_{i}^{-ni} \left\{ 1 - \exp(\Delta G_{r} / \sigma RT) \right\}$$
(3.1)

where *r* defines the net reaction rate,  $k^+$  denotes a dissolution rate constant, *a* corresponds to the activity of the *i*<sup>th</sup> aqueous species,  $n_i$  signifies the reaction coefficient of the *i*<sup>th</sup> species in the reaction forming the precursor complex,  $\sigma$  refers to the reaction order,  $\Delta G_r$  denotes the change in free energy for the overall reaction, *T* stands for absolute temperature, and *R* represents the gas constant. The product  $\Pi a_i^{-ni}$  describes the effect on the overall rate of the activities of the aqueous species involved in precursor complex formation. The terms within the brackets describe the effect of solution saturation state. For highly undersaturated solutions,  $\Delta G_r$  has a large negative value and the term within the brackets is equal to 1. At these conditions the dissolution rate is independent of bulk solution saturation of the precursor complex. For small deviations from equilibrium (i.e. when  $\Delta G_r / \sigma < RT$ ), the rate becomes linearly related to chemical affinity.

When applying Eq. (3.1) to silicate dissolution rates, it has commonly been assumed that 1)  $H^+$ ,  $OH^-$  and  $H_2O$  are the only aqueous species involved in precursor complex formation, 2) a

single reaction mechanism controls the overall rate at all  $\Delta G_r$ , and 3)  $\sigma = 1$ . These assumptions lead to the following rate equation (Lasaga, 1981):

$$r = k_{+}^{'} (a_{H+})^{n} H^{+} \{ 1 - \exp(\Delta G_{r} / RT) \}$$
(3.2)

where k'<sub>+</sub> refers to the dissolution rate constant for the hydrolytic process. This rate law has been used extensively to model fluid-rock interactions. However, the functional form of the dissolution rate: $\Delta G_r$  dependence is not well established and published expressions include simple exponentially decreasing rates as  $\Delta G_r$  tends to zero (e.g. Aagaard and Helgeson, 1977, 1982; Lasaga, 1981) as well as combinations of two or more exponential terms attributed to multiple dissolution mechanisms such as the development of etch pits as saturation states deviate further from equilibrium (e.g. Hellman and Tisserand, 2006; Taylor *et al.*, 2000).

#### 3.1.1.5. Cation Effects

The addition of cations to solution could affect the dissolution rate of feldspars, though not all cations have this effect (Amrhein & Suarez, 1992; Muir & Nesbitt, 1991). Addition of "feldspar building" ions, e.g. Ca, Na, Si, and Al, to solution resulted in different effects on the dissolution rate. In general, Ca, Na, and Si ions appeared to have no effect on the dissolution rates of labradorite (Muir & Nesbitt, 1991), and anorthite (Amrhein & Suarez, 1992) in acid solutions. This is in contrast to Al, which significantly inhibited dissolution at pH 3.6 to 6.0 at 25 °C (Amrhein & Suarez, 1992; Muir & Nesbitt, 1991), though not at pH 3.0 (Amrhein & Suarez, 1992), and only at concentrations above ca 0.5 mM. Inhibition of dissolution to the surface by aqueous aluminium. As the release of Al from the silicate surface to solution depends on the concentration gradient between the solid and solution, addition of aluminium to solution decreases this gradient and therefore slows down the release of Al from the solid, and hence the dissolution rate (Muir & Nesbitt, 1991).

#### 3.1.1.6. Ligand Complexation

The addition of ligands to solution also affects the dissolution rate, as they tend to form surface complexes. Carbonate is believed to form  $\equiv$ Al-CO<sub>3</sub><sup>-</sup> surface complexes with positively charged Al-surface groups (Berg & Banwart, 2000). A similar process is applicable to organic acids (Blake & Walter, 1999). Blake and Walther (1999) have studied the effect of citric and oxalic acid on the dissolution rate of albite, labradorite, and orthoclase. They concluded that there is a similarity in dissolution behaviour of alkali feldspars with similar Al content, i.e. albite and orthoclase, and a greater solubility of the more Al-rich feldspar, labradorite, in the presence of organic acids.

## **3.3. Methodology: Calculating Reaction Rates**

#### 3.3.1. Introduction

The rate of individual mineral-fluid reactions occurring in the Navajo Sandstone, have been determined by the solution of the mass balance equations which relate changes in fluid chemistry between a single initial spring (Green River Airport Well) and down-gradient springs (Fig. 2.4-17), to addition or subtraction of specific mineral phases. Fluid compositions sampled at each  $CO_2$  spring are corrected for the addition of brine entrained in the  $CO_2$  stream. Reaction progress  $(M_j)$  is then calculated by difference from a single initial well. The flow path and its length (z) are estimated from potentiometric surface measurements. Fluid velocity is calculated from a compilation of published porosity, hydraulic conductivities and local hydraulic head measurements for the Navajo Sandstone (Appendix B). Mineral proportions and surface areas are estimated from physical, chemical and petrological measurements on Navajo Sandstone samples locally, and from sites elsewhere in the Paradox Basin. The extent of mineral-fluid thermodynamic disequilibrium ( $\Delta G_r$ ) is calculated from the fluid chemistry, uncorrected for the brine additions

#### **3.3.2.** Mass Balance

Reaction progress, the net transfer of a mineral j to the fluid,  $M_j$  (negative for precipitation, positive for dissolution), was calculated from the evolution of solute chemistry between springs. Mineral mole transfers,  $M_j$ , in units of moles per m<sup>3</sup> of fluid, were calculated between the brine corrected chemistry of the upstream spring, Green River Airport Well, and the brine corrected chemistry of all down-gradient springs. Positive  $M_j$  denotes dissolution, negative  $M_j$  denotes precipitation. The chemical evolution of component k (concentration  $m_k$  moles/l), in the water between two points along the flow path is given by

$$\Delta m_{k} = \sum_{j=1}^{J} M_{j} b_{j,k}$$
(3.3)

where  $\Delta m_{T,k} = m_{k_{jnul}} - m_{k_{initial}}$  and  $b_{j,k}$  are the stoichiometric mole fraction of component k in mineral phase j (c.f. Plummer *et al.*, 1990). The solute flux mass balance model is non-unique to the extent that there may be phases additional to the ten (including brine) constrained by the ten components (including CI) modelled here. The possible reacting phases are defined by petrographic observations of outcrop samples of fresh unaltered Navajo Sandstone obtained from the San Rafael Swell, and core chips from petroleum exploration wells that penetrate the Navajo Sandstone along the Green River anticline, as well as published petrography of the Navajo Sandstone (Harshbarger *et al.*, 1957; Zhu *et al.*, 2006). Primary and secondary mineral compositions were analysed by electron microprobe, average compositions are presented bellow (see Appendix B for tabulated probe data). The following mineral compositions were used to constrain the mass balance model

K-feldspar:	$K_{0.95} Na_{0.05} Al_{1.00} Si_{3.00} O_8$	
Plagioclase:	$Na_{0.62}Ca_{0.38}Al_{1.38}Si_{2.62}O_8$	
Smectite:	$K_{0.26}Na_{0.03} [Mg_{0.35}Fe_{0.13}Al]$	$_{1.52}][Si_{3.51}Al_{0.49}]O_{10}(OH)_{2}$
Kaolinite:	$Al_2Si_2O_5(OH)_4$ *	
Dolomite:	$Ca_{1.06}Mg_{0.93}(CO_3)_2$	
Calcite:	$CaCO_{3}*$	
Quartz:	SiO <sub>2</sub> *	
Gypsum:	$CaSO_4 \cdot 2H_2O*$	(*ideal composition used)

Nine components (Na<sup>+</sup>, K<sup>+</sup>, Ca<sup>2+</sup>, Mg<sup>2+</sup>, Al<sup>3+</sup>, SiO<sub>2</sub>, SO<sub>4</sub><sup>2-</sup>, C and alkalinity), and nine phases (plagioclase (An38), K-feldspar, silica, kaolinite, smectite, calcite, gypsum, dolomite and CO<sub>2</sub>(g)) were considered, giving:

(i) solute mass balance

$$\Delta m_{T,Na} = 0.62M_{plagioclase} + 0.05M_{K-feldspar} + 0.03M_{smectite}$$
(3.4)

$$\Delta m_{T,K} = 0.95M_{K-feldspar} + 0.26M_{smectite}$$
(3.5)

$$\Delta m_{T,Mg} = 0.35M_{smectite} + 0.93M_{dolomite} \tag{3.6}$$

$$\Delta m_{T,Si} = M_{silica} + 2.62M_{plagioclase} + 3M_{K-feldspar} + 2M_{kaolinite} + 3.51M_{smectite}$$
(3.7)

$$\Delta m_{T,Al} = 1.38M_{plagioclase} + M_{K-feldspar} + 2M_{kaolinite} + 2.01M_{smectile}$$
(3.8)

$$\Delta m_{T,Ca} = M_{calcite} + M_{gypsum} + 0.38M_{plagioclase} + 1.06M_{dolomite}$$
(3.9)  
$$\Delta m_{T,Ca} = M_{calcite} + M_{gypsum} + M_{gypsum} + M_{dolomite}$$
(3.9)

$$\Delta m_{T,C} = M_{calcite} + M_{dolomite} + M_{CO_2}$$
(3.10)

$$\Delta m_{T,S} = M_{gypsum} \tag{3.11}$$

(ii) alkalinity mass balance

$$\Delta m_{T,Alkalinity} = 2M_{calcite} + 4M_{dolomite} + 2M_{kaolinite} + 5.94M_{smectite} + 2.76M_{plagioclase} + 2M_{k-feldspar}$$
(3.12)

where 
$$Alkalinity = \left[HCO_3^{-}\right] + 2\left[CO_3^{2-}\right] + \left[OH^{-}\right] - \left[H^{+}\right]$$
 (3.13)

In addition to the solute mass balance equations mineral mass transfers are further constrained by the solution of an alkalinity mass balance. The stoichiometric coefficients constraining individual mineral mole transfers in equation 3.12 are the number of equivalents (mEq/l) of alkalinity produced or consumed per mole of phase dissolved or precipitated. Silicate dissolution and clay precipitation reactions modify local alkalinity by consuming or releasing protons, respectively. Reactions involving carbonate minerals modify alkalinity through the consumption or release of protons and bicarbonate ions. The dissolution and dissociation of  $CO_2$  has no net effect on alkalinity as it produces both  $HCO_3^-$  and  $H^+$  ions via the dissociation reaction  $CO_2 + H_2O \rightarrow HCO_3^- + H^+$ .

The mole transfers for plagioclase can be independently constrained by separate solution of the mass balance equations for Sr and  ${}^{87}$ Sr/ ${}^{86}$ Sr (Eq. 3.14 to 3.16), assuming all Sr, corrected for brine additions, is derived from the dissolution of plagioclase and dolomite, and  $M_{dolomite}$  is derived from the solute mass balance model:

$$\Delta Sr = Sr_{final} - Sr_{initial} \tag{3.14}$$

$$\Delta^{87} Sr / {}^{86} Sr \cdot Sr = ({}^{87} Sr / {}^{86} Sr \cdot Sr)_{final} - ({}^{87} Sr / {}^{86} Sr \cdot Sr)_{initial}$$
(3.15)

$$\Delta^{87} Sr/^{86} Sr \cdot Sr = ({}^{87} Sr/^{86} Sr \cdot Sr)_{plagioclase} \cdot M_{plagioclase} + ({}^{87} Sr/^{86} Sr \cdot Sr)_{dolomite} \cdot M_{dolomite}$$
(3.16)

The average Sr concentration in analysed plagioclase and dolomite are ~ 320 ppm and 205 ppm, respectively.  ${}^{87}\text{Sr}/{}^{86}\text{Sr}_{\text{plag}}$  (0.724102) is taken to be the average  ${}^{87}\text{Sr}/{}^{86}\text{Sr}$  reported for whole rock analyses of Truini and Longsworth, (2003).  ${}^{87}\text{Sr}/{}^{86}\text{Sr}_{\text{dolomite}}$  is taken as the average  ${}^{87}\text{Sr}/{}^{86}\text{Sr}$  for early dolomite cements (0.71030) reported by Goldstein *et al.*, (2008).

Whilst illite clays are present as altered products of feldspar they are thought to represent the products of higher temperature diagenetic reactions during burial and are not thought to participate in these reactions either as dissolving phases due to their relative super-saturation or as precipitates due to the presence of other, thermodynamically more stable phases.

The solutions of equations 3.4 to 3.12 for the changes of brine-corrected water compositions between the Green River Airport Well and the nine downstream wells are consistent with: 1) dissolution of plagioclase, K-feldspar, dolomite and gypsum, 2) precipitation of calcite, kaolinite, smectite and quartz, and 3) consumption of  $CO_2$ . The proportions of the phases are consistent with the stoichiometry of the reaction

$$plag + Kspar + gypsum + dolomite + H^{+} + HCO_{3}^{-} \rightarrow$$

$$kaolinite + smectite + calcite + quartz$$
(3.17)

#### 3.3.3. Calculation of Reaction Rates

Feldspar dissolution rates in mole·m<sup>-2</sup>·s<sup>-1</sup> were calculated from 1) the gradient of the mineral modes in the fluid with distance along the flow path, 2) the fluid flux and 3) mineral surface areas within the aquifer. Porosity and hydraulic conductivity data are compiled in Appendix B. Mineral mode against distance plots show an inflection where there is a drop in pH (Figs. 2.4-17 & 3.4-1) and we model the best constrained part of the profile downstream of this point. The rate of change of mineral mode with distance was calculated by modelling the variation of mineral modes ( $M_j$ ) with distance (z), by a least-squares fit to the empirical expression

$$M_i = A \cdot (1 - \exp^{-B_z}) \tag{3.18}$$

which was then differentiated to obtain the rate of change of the slope,  $dM_i/dz$ .

$$\frac{dM_j}{dz} = AB \cdot \exp^{-Bz} \tag{3.19}$$

The differential equation describing the variation in moles of a reacted phase in the fluid phase with time may be approximated by

$$\varphi \frac{\partial M_j}{\partial t} = R_j \cdot S_j - \omega_o \varphi \frac{\partial M_j}{\partial z}$$
(3.20)

where  $\omega_o$  is the fluid velocity (ms<sup>-1</sup>),  $\phi$  is the porosity,  $R_j$  is the reaction rate for phase *j* (mole.m<sup>-2</sup>.s<sup>-1</sup>) and  $S_j$  is the surface area of mineral *j* (m<sup>2</sup>/m<sup>3</sup>). For flow systems where  $S_j$  varies slowly, the quasi stationary state approximation (Lichtner 1988),  $\partial M_j/\partial t = 0$ , simplifies equation (3.20) to

$$\frac{\partial M_j}{\partial z} = \frac{R_j S_j}{\omega_o \varphi}$$
(3.21)

The fluid flux  $(\omega_o \phi)$  was calculated from the gradient in hydraulic head dh/dz, and the mean of a compilation of laboratory derived hydraulic conductivity values from the Navajo Sandstone, K (ms<sup>-1</sup>) (Hood and Patterson, 1984; Weigel, 1986), where

$$\omega_o \varphi = K \cdot \frac{dh}{dz} \tag{3.22}$$

Reaction rate  $R_j$  for the *j*th mineral phase, was then calculated as

$$R_{j} = \frac{\partial M_{x}}{\partial z} \frac{\omega_{o} \varphi}{S_{j}}.$$
(3.23)

 $S_j$ , the surface area of the *j*th mineral (m<sup>2</sup>/m<sup>3</sup>) is calculated from the whole rock specific surface area, ( $s_j = 0.7 \text{ m}^2/\text{g}$  from BET measurements on Navajo Sandstone by Zhu (2005) assuming that individual mineral surface areas are proportional to their volume fractions and allowing for the mean porosity of the Navajo ( $\phi = 0.20 \pm 0.04 \text{ 1} \sigma$ , from Navajo Sandstone samples collected from the northern Paradox Basin, (Cooley *et al.*, 1969; Freethy, 1988; Hood and Patterson, 1984; Weigel, 1986) as

$$S_{i} = s_{i} \cdot v_{i} \cdot (1 - \varphi) \cdot \rho \tag{3.24}$$

Mineral volumetric abundances,  $v_j$ , were determined from normative mineral abundances calculated using the mineral compositional data obtained in this study and a compilation of whole rock chemical analyses of Navajo Sandstone from this study (Appendix B) and Bowen (2004). Modal mineralogy was calculated from least squares mixing of mineral proportions to match whole rock compositions using the program MINSQ (Hermann & Berry, 2002). Calculated mineral surface areas for plagioclase and K-feldspar are  $51 \times 10^3 \pm 6 \times 10^3 \text{ m}^2/\text{m}^3$  and  $112 \times 10^3 \pm 10 \times 10^3 \text{ m}^2/\text{m}^3$  respectively.

### 3.4. Results and Discussion

#### 3.4.1. Reaction Rates

Reaction progress in terms of net dissolution of plagioclase and K-feldspar and precipitation of kaolinite, smectite and calcite calculated relative to Green River Airport Well (Table 3.4-1) show an inflection after Crystal Geyser but then increase at an exponentially decreasing rate downstream (Fig. 2.4-17). These rate changes are attributed to progressive neutralization of pH downstream from the sites of  $CO_2$  injection and the approach to mineral-fluid equilibrium. The inflexion in gradient after Crystal Geyser is consistent with the drop in pH and increase in  $CO_2$  consumed (Fig. 2.4-17) at Small Bubbling Spring attributed to additional  $CO_2$  injection.

We therefore fit the empirical equation 3.18 to the change in mineral modes against distance for springs downstream of Small Bubbling Spring (Fig. 3.3-1). These fits include the down stream Ten Mile, Tumble Weed and Chaffin Ranch Geysers which have a more tenuous hydrological connection with the upstream wells. Excluding these springs from the fits makes only a ~ 25% difference to the gradient except where it is poorly defined towards the ends of the flow paths. The rates of mineral dissolution are calculated from the gradients in molar transfer with distance (equation 3.18) and from the steady state solution to the transport equation 3.21. The rates of plagioclase and K-feldspar dissolution are in the ranges  $2x10^{-14}$  to  $2x10^{-19}$  and  $4x10^{-16}$  to  $4x10^{-18}$  mol·m<sup>-2</sup>·s<sup>-1</sup> respectively, within the range observed for other field studies at near-neutral pHs but slower than most laboratory studies (Fig. 3.4-2).



**Figure 3.4-1** Calculated changes in the feldspar mineral modes with distance along the flow path. The rate of change of mineral mode with distance was calculated by a least-squares fit to the variation of mineral modes  $(M_j)$  with distance (z) over the well-constrained portion of the flow path, downstream of Small Bubbling Spring. Error bars are the propagated errors derived from analytical uncertainty, uncertainty associated with the brine correction and mass balance modeling (see Appendix A of detials).



**Figure 3.4-2** Variation in feldspar dissolution rate versus pH for a compilation of laboratory (White and Brantley, 2003) and in-situ dissolution rates (Hereford et al., 2007; Malstrom et al., 2004; White and Brantley, 2003), feldspar dissolution rates in the Navajo Sandstone at Black Mesa (Zhu, 2005) and the rates calculated at Green River.

	Plag	Kspar	Kao	Smc	Cc	Si	Gyp	Dol	CO <sub>2</sub>
Spring					mmol/l				
Crystal Geyser	40.18	2.53	-28.38	-3.80	-14.06	-58.46	3.03	2.58	40.68
Small Bubbling	55.85	3.26	-35.50	-8.00	-26.17	-73.25	2.05	4.01	61.44
Big Bubbling	73.30	4.25	-47.97	-10.13	-32.75	-98.56	0.14	4.46	64.58
SS Big Bubbling	81.99	5.27	-51.01	-13.63	-38.47	-106.14	1.75	5.89	69.88
Pseudo Tenmile	99.86	6.01	-61.98	-16.26	-46.50	-127.72	1.18	6.27	51.72
Torreys	117.80	7.97	-73.25	-19.66	-48.41	-151.66	3.64	7.38	69.70
Tenmile	103.50	7.63	-49.01	-32.05	-35.09	-110.67	18.77	13.67	15.35
Tumble	98.87	7.45	-55.00	-21.46	-40.16	-117.34	9.87	9.10	44.30
Chaffin	112.68	8.96	-58.32	-28.54	-36.90	-127.03	15.10	12.70	16.59

Table 3.4-1 Mineral mol transfers (mmol/l) calculated using the mass balance model detail in section 3.3.2.

Error propagation analyses, using Gaussian error propagation, give uncertainties of approximately 20-25% of the calculated rates (the formulation of error analysis is detailed in Appendix A). Error propagation takes into account the errors associated with mass transfer calculations arising from analytical uncertainty, the uncertainties in correction for brine inputs taken as the standard error of brine compositions compiled from Spangler *et al.*, (1996) and Breit (2002), the scatter in BET specific surface area measurements, mineral abundances and porosity. Calculation of plagioclase mole transfers depends primarily on changes in fluid Na concentrations which have relatively large uncertainty due to the scatter in brine Na/Cl ratios. If the brine inputs in the Green River system are of relatively homogeneous compositions then plagioclase exhibits smooth changes in mole transfer with distance comparable with the better constrained K-feldspar mole transfers (Figs. 3.4-1). However the magnitude of plagioclase mole transfers and resultant inferred reaction rates are sensitive to the assumed brine Na/Cl ratio. If this is varied over the full range observed (0.73 to 0.99), then average calculated plagioclase dissolution rates decrease from ~  $3x10^{-14}$  to ~  $8x10^{-15}$  mol·m<sup>-2</sup>·s<sup>-1</sup>.

Plagioclase dissolution rates determined independently with  ${}^{87}$ Sr/ ${}^{86}$ Sr and Sr mass balance vary from  $4x10^{-14}$  to  $1x10^{-25}$  mol·m<sup>-2</sup>·s<sup>-1</sup> in good agreement with rates derived from solute mass balance. However, uncertainties associated with rates derived from Sr are on the order of 50% of the calculated rates, given the compounding effects of the large variation in  ${}^{87}$ Sr/ ${}^{86}$ Sr<sub>plag</sub>, Sr<sub>plag</sub>,  ${}^{87}$ Sr/ ${}^{86}$ Sr<sub>dol</sub>, Sr<sub>dol</sub>,  ${}^{87}$ Sr/ ${}^{86}$ Sr<sub>brine</sub> and Sr<sub>brine</sub>. Depressed Sr and  ${}^{87}$ Sr/ ${}^{86}$ Sr for Torreys Spring and Big Bubbling side seep are probably due to the addition of a low  ${}^{87}$ Sr/ ${}^{86}$ Sr Sr source not accounted for in the model, variability in the brine  ${}^{87}$ Sr/ ${}^{86}$ Sr and Sr concentration or to heterogeneity in mineral  ${}^{87}$ Sr/ ${}^{86}$ Sr and Sr concentrations at the aquifer scale.



**Figure 3.4-3** (A) Calculated changes in the plagioclase mineral modes with distance along the flow path, using Sr mass balance. (B) Least squares fitting of equation 3.18 yields mole transfers and calculated rates that are of the same order of magnitude as those derived from solute mass balance. Torrey's spring and Big Bubbling side seep are discounted from the fit as they have negative mole transfers, suggesting that the model does not accurately account for their measured fluid composition.

#### **3.4.2.** Approach to Equilibrium - $\Delta G_r$

Reaction rates decrease as minerals approach equilibrium with co-existing fluids (e.g. Lasaga, 1998). We have therefore calculated the degree of solution saturation state for each spring with respect to the individual feldspar dissolution reactions. The deviation from equilibrium is expressed in terms of the Gibbs free energy of reaction,  $\Delta G_r$  (kJ mol<sup>-1</sup>),

$$\Delta G_r = RT \ln \left[ \frac{IAP}{K_{eq}} \right]$$
(3.25)

where *R* is the gas constant (kJ.K<sup>-1</sup>.mol<sup>-1</sup>), *T* is the absolute temperature (K), *IAP* is the ion activity product and  $K_{eq}$  is the equilibrium constant. The general reaction for the dissolution of plagioclase feldspar in water can be described as (Arnórsson and Stefánsson, 1999):

$$Na_{x}Ca_{(1-x)}Si_{(2+x)}Al_{(2-x)}O_{8} + 8H_{2}O \leftrightarrow$$

$$xNa^{+} + (1-x)Ca^{2+} + (2-x)Al(OH)_{4}^{-} + (2+x)H_{4}SiO_{4}$$
(3.26)

In general, feldspars dissolve congruently at acid and alkaline pH, and incongruently at neutral pH. Studies of mineral saturation in aqueous solutions involve two steps: (1) derivation of equilibrium constants ( $K_{eq}$ ) for mineral hydrolysis from thermodynamic data taking into account the effects of variable composition of the minerals and ordering, as appropriate; and, (2) calculation of individual aqueous species activities from analytical data on the waters to retrieve values for the respective activity product (*IAP*). Comparison between the two allows evaluation of saturation states of waters with respect to feldspars as a function of their composition and Al-Si ordering (Arnórsson & Stefánsson, 1999).

The distribution of aqueous species and their activities were calculated using the geochemical computer code PHREEQC (Parkhurst and Appelo, 1999).  $\Delta G_{f, \text{Tr, Pr}}^{\circ}$ ,  $V^{\circ}$ ,  $S^{\circ}$ , Cp of feldspar solid solutions were calculated after Arnórsson and Stefánsson, (1999). Equilibrium constants ( $K_{eq}$ ) for the reactions considered where calculated using the SUPCRT92 code (Johnson *et al.*, 1992) modified with the thermodynamic data for Al species of Tagirov and Schott (2001).

 $\Delta G_r$  values for the feldspar dissolution reactions were computed from equation 3.25. Values of the ion activity product, *IAP* in equation 3.25, for the congruent dissolution of plagioclase and K-feldspar, consistent with the reactions

$$Na_{0.62}Ca_{0.38}Al_{1.38}Si_{2.62}O_8 + 2.76H^+ + 5.24H_2O \longleftrightarrow$$

$$0.62Na^+ + 0.38Ca^{2+} + 1.38Al(OH)_2^+ + 2.62H_4SiO_4$$

$$(3.27)$$

$$K_{0.95}Na_{0.05}Al_{1.00}Si_{3.00}O_8 + 6H_2O + 2H^+ \longleftrightarrow$$

$$0.95K^+ + 0.05Na^+ + Al(OH)_2^+ + 3H_4SiO_4$$
(3.28)

were computed using

$$IAP_{plag} = \frac{a_{Na^{+}}^{0.62} \cdot a_{Ca^{2^{+}}}^{0.38} \cdot a_{Al(OH)_{2}^{+}}^{1.38} \cdot a_{H_{4}SiO_{4}}^{2.62}}{a_{H^{+}}^{2.76}}$$
(3.29)

$$IAP_{Kspar} = \frac{a_{K^+}^{0.95} \cdot a_{Na^+}^{0.05} \cdot a_{Al(OH)_2^+} \cdot a_{H_4SiO_4}^3}{a_{H^+}^2}$$
(3.30)

The modelled plagioclase and K-feldspar reactions exhibit a strong inverse relationship between dissolution rate and mineral-fluid free energy difference over a -10 to -2kJ mol<sup>-1</sup> and a -6 to 0 kJ mol<sup>-1</sup> transition region, respectively (Fig. 3.4-3). These free energies lie close to equilibrium in the very low  $\Delta G_r$ , low dissolution rate region that is characterized by a strong functional dependence of the dissolution rate on  $\Delta G_r$ . Laboratory studies on feldspars (Beig and Lüttge, 2006; Burch *et al.*, 1993; Hellman *et al.*, 2006; Hellmann and Tisserand, 2006; Taylor *et al.*, 2000) and other silicate minerals (e.g. Nagy & Lasaga, 1992) confirm theoretical predictions that dissolution rates are independent of saturation state far from equilibrium (but see Oeklers *et al.*, 1994) and decrease in a transition region as equilibrium is approached. However, the functional form of the dissolution rate: $\Delta G_r$  dependence is not well established and published expressions include simple exponentially decreasing rates as  $\Delta G_r$  tends to zero (e.g. Aagaard and Helgeson, 1977, 1982; Lasaga, 1981) as well as combinations of two or more exponential terms attributed to multiple dissolution mechanisms such as the development of etch pits as saturation states deviate further from equilibrium (e.g. Hellman and Tisserand, 2006; Taylor *et al.*, 2000).

The results here for plagioclase and K-feldspar dissolution rates (Fig. 3.4-3), suggest that at  $\Delta G_r > -10$  kJ/mol rates decrease exponentially over 5 orders of magnitude as equilibrium is approached. This is the most difficult region to investigate in laboratory experiments because of the very slow reaction rates, and field results, such as those here which reflect reactions over the ~ 1000 year time scales for water flow between the springs, offer an alternative approach.



**Figure 3.4-4** The variation in feldspar dissolution rate with  $\Delta G_r$  at Green River, illustrating the strong dependence of rate on degree of under-saturation, the wide range of rates observed and the overall proximity of the system to equilibrium. Error bars are the propagated uncertainty in dissolution rate and  $\Delta G_r$  detailed in Appendix A.

#### 3.4.3. Uncertainties in Reaction Rates and Solution Saturation States

The uncertainties in the reaction rates recovered from the field measurements should not be underestimated. However several of the most significant of these may cause systematic uncertainty in the absolute magnitude of the reaction rates but not the form of the functional dependence on  $\Delta G_r$ . A major uncertainty is that the BET method may over-estimate mineral surface areas. However, it is unlikely that mineral surface areas will vary significantly along the



**Figure 3.4-5** The variation in plagioclase dissolution rate with  $\Delta G_r$  comparing estimates of  $\Delta G_r$  from measured pH and *p*CO<sub>2</sub> to those derived from recalculation of in-situ *p*CO<sub>2</sub> and pH described in Chapter 2.

flow path and any systematic error in surface areas will result in a corresponding systematic error in the absolute values of dissolution rates but not their functional dependence on  $\Delta G_r$ . K-feldspar and plagioclase geometric surface areas, are 27% and 41% less than BET determined surface areas, respectively, and would imply calculated rates that are faster than BET normalized rates by the same factors, with peak K-feldspar and plagioclase rates of  $4.5 \times 10^{-16}$  and  $4.5 \times 10^{-14}$  mol·m<sup>-2</sup>·s<sup>-1</sup>. Complications in the hydrology could invalidate the calculation of reaction rates but the results from closely spaced springs are consistent. Again, systematic errors in estimating flow rates would not change the form of the relationship with  $\Delta G_r$ .

Uncertainties in the calculation of  $\Delta G_r$  are more difficult to estimate because confidence limits on the thermodynamic data are not available for the fluid species. In addition there are two further potential sources of uncertainty: 1) the filtration of water samples through 0.2 µm filters may not remove all particulate Al, although the consistency of the results suggest that this is not a serious problem in these relatively clean spring waters: 2) fluid pH and alkalinity measurements are taken from samples collected after degassing during ascent in the spring. Modelling of the carbon isotope versus pH changes during the degassing process (Assayag *et al.*, 2009) suggests that degassing must be a relatively shallow process and even so the observed CO<sub>2</sub>-gas to DIC  $\delta^{13}$ C fractionations need to include an extra ~ 1 ‰ kinetic fractionation. Precise estimates of the uncertainty in DIC and pH are therefore difficult to ascertain. Depth-dependent degassing may result in over-estimates of local fluid pH which would introduce systematic uncertainty in  $\Delta G_r$ and erroneously high  $\Delta G_r$  estimates for each spring. Recalculation of in-situ pH and *p*CO2 (Chapter 2, section 2.4.5.4) for the plagioclase dissolution reaction results in ~ -10 kJ/mol lower estimates of  $\Delta G_r$  for the springs closest to the site of CO<sub>2</sub> injection, decreasing to between -5 and 0 kJ/mol for the springs furthest along the flow path (Fig. 3.4-5). Evan at the maximum in-situ pH  $\Delta G_r$  estimates are still close to or within the experimentally determined close to equilibrium region, where rates are predicted to exhibit strong  $\Delta G_r$  dependence.

#### 3.4.4. Comparison of Reaction Rates with Laboratory and Field Estimates

The observed proximity of Green River Navajo Sandstone fluids to plagioclase and K-feldspar equilibrium and the dependence of feldspar dissolution rates on deviation from these equilibria may explain a significant part of the apparent discrepancy with comparable laboratory-derived rates, which typically characterize systems far from equilibrium.

For example, the experiments of Taylor *et al.*, (2000) on plagioclase (An61) dissolution at 25°C and pH 3 (Fig. 3.4-6) imply that plagioclase (An61) dissolution rates at  $\Delta G_r = -10$  kJ/mol are about 18% of those measured at far from equilibrium (Fig. 3.4-6). If so, the calculated rates at low  $\Delta G_r$  of ~ 2x10<sup>-14</sup> mol·m<sup>-2</sup>·s<sup>-1</sup> would be compatible with far-from-equilibrium rates of ~1x10<sup>-13</sup> mol·m<sup>-2</sup>·s<sup>-1</sup> as observed in some experimental studies (e.g. Amrhein and Suarez, 1992; White and Brantley, 2003). If geometric surface area normalized rates are considered, close to equilibrium rates derived here imply far from equilibrium rates of ~3x10<sup>-13</sup> mol·m<sup>-2</sup>·s<sup>-1</sup> within error, of the mean of circum-neutral pH laboratory derived plagioclase dissolution rates (~4.6x10<sup>-13</sup> mol·m<sup>-2</sup>·s<sup>-1</sup>) (White and Brantley, 2003).

The effect of inhibiting ions, namely Al and  $CO_3^{2-}$  are difficult to assess in any natural system due to the competing and interdependent effects of pH,  $\Delta G_r$ , and ion activities. Al concentrations are on the order of 3 to 6  $\mu$ mol L<sup>-1</sup> significantly lower than the 500  $\mu$ mol L<sup>-1</sup> required for significant Al inhibition at 25 °C reported by Amrhein and Suarez, (1992). Amrhein and Suarez, (1992) report a 31% decrease in anorthite dissolution rate at 25 °C and pH 6 in the presence of Al concentrations of 4  $\mu$ mol L<sup>-1</sup>. Correction of the calculated rates for this magnitude of Al inhibition makes a negligible difference to the peak plagioclase dissolution rates, which become 2.4x10<sup>-14</sup> mol·m<sup>-2</sup>·s<sup>-1</sup>. Oeklers et al., (1994) reported a ~16% decreasing in albite dissolution rates at 150°C and pH 9 in the presence of 1000 µmol L<sup>-1</sup> Al. A ~10% decrease in Kfeldspar dissolution rate at 150°C and pH 2 was reported by Gautier et al., (1994) for similar Al concentrations. Whilst the presence of dissolved Al may have a small effect on suppressing the overall magnitude of the dissolution rates in this system, its effect is probably small and cannot explain the overall variation in the magnitude of rates observed. However without experimental studies at the relevant feldspar compositions, temperature and pH this is difficult to assess quantitatively. No applicable experimental work has been conducted on  $CO_3^{2-}$  at the relevant temperature and  $pCO_2$  and as  $CO_3^{2-}$  surface complexation is likely to increase solubility, its effect on retarding dissolution rate can be negated.



**Figure 3.4-6** Variation in plagioclase dissolution rate with  $\Delta G_r$  at Green River compared to experimentally determined rates at similar pH and temperature (after Taylor *et al.*, 2000). Green River rates have been normalized to 25°C using the Arrhenius equation and an activation energy of 80 kJ/mol from Blum and Stillings (1995). Line fit to the experimental data is the dissolution rate law of Taylor *et al.*, (2000). The figure illustrates the main  $\Delta G_r$  regions over which free energy-rate dependence and independence is observed in experimental studies. It should be noted that differences in the magnitude of our rates compared to the predicted rates at  $\Delta G_r > -10$  kJ/mol of Taylor *et al.*, (2000) are attributed to differences in An content and pH between their experiment and the groundwater system, but this is the only study of  $\Delta G_r$  dependence at a 'comparable' plagioclase composition and at low temperature.

Differences in feldspar dissolution rates observed between surface weathering environments and aquifer systems (White and Brantley, 2003) are attributed to the difference in proximity of these two systems to equilibrium. The difference in proximity to equilibrium found here as compared to the lower  $\Delta G_r$  values (-30 to -50 kJ mol<sup>-1</sup>) for feldspar dissolution observed in surface weathering environments (Velbel, 1989) with high percolation velocities suggests that slow flow velocities and long solution-mineral contact times in aquifers maybe important in holding silicate weathering reactions close to thermodynamic equilibrium. It should be noted that the slow rate of fluid percolation through the Navajo Sandstone favours mineral surface control, as apposed to transport control on fluid-mineral reaction rate.

Additionally the apparent pH dependence observed in compilations of field-scale dissolution rates at circum-neutral pH (Fig. 3.4-2) is attributable to the combined effects of a) their proximity to equilibrium and b) the strong variation in  $\Delta G_r$  observed over a small change in pH between pH 6 and 7.

## **3.5.** Conclusions

In-situ feldspar dissolution rates under conditions of high pCO<sub>2</sub>, within the saturated Navajo Sandstone at Green River, Utah have been determined in this chapter. The close to equilibrium plagioclase dissolution rates derived from mass balance and hydrological modelling range from  $10^{-13.74 \pm 0.11/0.15}$  mol·m<sup>-2</sup>·s<sup>-1</sup> to  $10^{-18.63 \pm 0.6/1.5}$  mol·m<sup>-2</sup>·s<sup>-1</sup>. K-feldspar dissolution rates range from  $10^{-13.74 \pm 0.11/0.15}$  mol·m<sup>-2</sup>·s<sup>-1</sup> to  $10^{-17.42 - 0.27/0.81}$  mol·m<sup>-2</sup>·s<sup>-1</sup>. K-feldspar dissolution rates range from  $10^{-15.45 \pm 0.08/0.09}$  mol·m<sup>-2</sup>·s<sup>-1</sup> to  $10^{-17.42 - 0.27/0.81}$  mol·m<sup>-2</sup>·s<sup>-1</sup>. These rates are 1 to 3 orders of magnitude slower than rates determined by laboratory experiments at similar temperatures and pH, and 1 to 3 orders of magnitude faster than rates determined in the same aquifer under alkaline groundwater conditions. The enhancement of feldspar dissolution rates in this study area, relative to those determined by Zhu (2005) for alkaline groundwater, is attributed to the introduction of CO<sub>2</sub> which depresses silicate mineral saturation in the fluids. The finding that the Green River system is close to thermodynamic saturation adds to the evidence that the 2–5 orders of magnitude discrepancy between laboratory and field rates may, in part, be explained by differences in the thermodynamic state of experimental and natural fluids (c.f. Burch *et al.*, 1993; White and Brantley, 2003).

The range of rates and the rate: $\Delta G_r$  dependence observed at Green River suggest that feldspar dissolution rate laws should include exponentially declining rates close to equilibrium ( $\Delta G_r <-10$ kJ/mol), over a wider range (and slower absolute values) of dissolution rate than previously suggested by experimental studies. These findings suggest that mineral-fluid reactions in CO<sub>2</sub> hosting reservoirs will be promoted by the state of disequilibrium induced by the introduction of CO<sub>2</sub> and highlight the importance of including a rate: $\Delta G_r$  dependence in the geochemical modelling of the long term interactions of CO<sub>2</sub>-fluid-rock in geological storage reservoirs. This suggests that in the earliest stages of CO<sub>2</sub> injection in storage sites systems can be expected to be highly undersaturated with respect to minerals comprising the host reservoir and reaction rates will be fast, occurring at low  $\Delta G_r$ . The continued study of fluid-rock interactions in natural settings may help further elucidate the relationship between rate and  $\Delta G_r$  for a range of mineral phases, in the close-to-equilibrium region which is so difficult to assess experimentally.

These results must be tempered with the understanding that large uncertainties exist in the quantification of modelling parameters in natural settings, especially reactive mineral surface area, indirect sampling of reservoir fluids and the hydro-geological setting. The long duration of reaction accessible in natural studies, whilst allowing access to controlling factors of real mineral weathering such as near equilibrium rate dependence, also introduces uncertainty as many model parameters may change through the duration of the 'experiment'. The change in porosity and reacting mineral surface through the duration of the natural experiment cannot easily be factored into the calculation of the controlling rates. Heterogeneity in reservoir hydraulic properties, mineralogy and fluid chemistry also lead to uncertainty in the calculation of rates.

# Chapter 4 Geochemistry of an Ancient CO<sub>2</sub>-Leaking Groundwater System, Green River, Utah

## 4.1. Introduction

Surface travertine deposits, and carbonate cementation and veining within Jurassic sandstones within the footwall of Little Grand Fault (LGF) and Salt Wash Graben (SWG) record a history of CO<sub>2</sub> leakage from the Green River anticline. The origin and evolution of fluids responsible for surface travertine formation, shallow subsurface carbonate veining and host rock alteration may be delineated from petrographic observations, and from the chemical and isotopic composition of mineral products. Further, processes important for controlling the leakage of  $CO_2$  from the fault systems, and the coupling of physical and geochemical processes during subsurface CO<sub>2</sub> leakage, can be investigated through the analysis of chemical and isotopic systems. Understanding the evolution of leakage behaviour in fault systems both in time and space, and under conditions of differing fluid infiltration, mineral-fluid reactions, fault architecture and lithological properties is of great importance for predicting the potential leakage behaviour of geological  $CO_2$  storage sites. Physical and geochemical observations from naturally leaking faults allows prediction to be made about the interplay of structural and chemical processes in controlling leakage sites and rates, the role of fluid-mineral interactions in generating and closing leakage pathways and their relation to geochemical processes in the host aquifer, such as the volume of the CO<sub>2</sub>-charge, and subsequent in-situ  $pCO_2$ , and the dissolved mineral load.

The petrology and mineral chemistry of altered host rock, carbonate cements and veins from fracture networks in the fault damage zone and in travertine feeder systems provide constraints on the pathways and rates of  $CO_2$ -promoted fluid-mineral reactions. Minor and trace element contents of carbonate cements reflect pore water chemistries prevailing during carbonate precipitation (Veizer, 1983) and with knowledge of the relevant mineral-fluid partition coefficients can be used to reconstruct the chemistry of the parent fluid. In addition, if the composition of the parent fluid is known, a posteriori, mineral and fluid chemistry can be used to constrain the magnitude of this partitioning. For some trace elements, experimental studies have shown that the magnitude of the parent structure. Thus, if past fluids associated with ancient

travertine formation were compositionally similar to the modern  $CO_2$ -charged fluids, this fluid composition, in conjunction with measured carbonate cement compositions can be used to estimate the rate of carbonate mineral precipitation. Information on the rates of carbonate cementation in fault zones, and their geochemical controls, is of great importance in predicting the sealing behaviour of faults and fracture zones as a result of the passage of  $CO_2$ -charged fluids. This will allow prediction of the time required for leaking faults in geological carbon storage sites to self seal through carbonate mineral precipitation.

#### 4.1.1. Diagenetic Bleaching of Jurassic Sandstones, Paradox Basin

The aeolian Lower to Middle Jurassic sandstones of the Paradox Basin are typically characterized by a uniform red color that results from thin hematite coatings on sand grains, formed during early diagenesis (Walker, 1975). Across the Paradox Basin, adjacent to faults and preferentially in coarser grained sandstone units, these reddish sandstones are frequently bleached pale-yellow or white where hematite grain coatings have been dissolved by the passage of diagenetic fluids (Foxford et al., 1996; Garden et al., 1997, 2001). The nature of the fluid(s) responsible for this bleaching are still highly debated as many volatile species are capable of altering the Eh-pH conditions of subsurface fluids, facilitating dissolution of minerals such as hematite, which are otherwise relatively insoluble in typical, low temperature groundwater systems. These extraformational fluids may include hydrocarbon liquids, carbon dioxide, organic acids, methane, hydrogen sulphide (Chan et al., 2000; Eichhubl et al., 2009; Garden et al., 2001; Surdam et al., 1993) and de-oxygenated fluids. Previous studies of bleaching in the Paradox Basin have mainly attributed the bleaching fluid directly to hydrocarbons (Beitler et al., 2003; Bowen, 2004; Chan et al., 2000; Garden et al., 2001; Hansley, 1995; Parry et al., 2004) or fluids directly associated with them (Eichhubl et al., 2009). Although alternative volatile phases, such as  $CO_2 + H_2S$ , have been proposed (Haszeldine et al., 2005). What ever the mechanism, such extensive dissolution of hematite must involve reductive hydrolysis via the reaction;  $Fe_2O_3 + 2e + 6H^+ \leftrightarrow 2Fe^{2+} +$  $3H_2O$ , given the very low solubility of Fe<sup>3+</sup> in typical groundwaters.

At Green River bleaching of Jurassic sandstones occurs to varying degrees in the footwalls of both Little Grand Fault (Curtis Formation) and Salt Wash Graben (Entrada Sandstone) (Dockrill, 2005). The distribution of bleaching in the footwalls of both faults is focused at the intersection of the faults and the fold axis of the Green River anticline. Two distinct generations of sandstone bleaching are observable in the field. The first is large-scale bleaching which is m's thick and 10's to 1000's m in lateral extent, separated from unbleached rock by a sharp contact and constrained to the lower portions of individual formations. This bleaching is associated with calcite cementation and gypsum and calcite veining. The second is small-scale bleaching which is confined to the base of ancient travertine deposits. This occurs as:

a) thin, 10's cm thick bleached sandstone beds which extend laterally 10's meters from the alteration zone; b) as halos, mm's-cm's thick, around fractures within the alteration zone and; c) as diffuse bleaching in zones of complex alteration, and calcite and aragonite cementation and veining. The origin of both bleaching events, and their relationship to each other, is uncertain but the localization of bleaching in travertine feeder zones implies at least some relation between this geochemical processes and the passage of  $CO_2$ -charged fluids.

This chapter discusses the petrology, isotope geochemistry and mineralogy of bleaching associated with ancient travertine feeder zones, within the Entrada Sandstone, Salt Wash Graben. In this chapter mineral composition from calcite cements associated with bleaching below travertine mounds are used to constrain the Eh-pH conditions prevailing in the ancient CO<sub>2</sub>-system. The petrology and isotope geochemistry of the large-scale bleached zones is discussed in Chapter 5, where observations from fluid inclusions are used to constrain the volatile phase responsible for bleaching in each system.

## 4.2. Objectives

Carbonate cemented host rock and carbonate veins from the Entrada Sandstone, in the footwall of Salt Wash Graben, were collected for geochemical, petrological and isotopic analysis. Samples collected during the 2007 field season were supplemented with chips of U-Th dated carbonate veins from both Little Grand Fault and Salt Wash Graben provided by Neil Burnside, University of Glasgow. Isotopic analysis of their <sup>87</sup>Sr/<sup>86</sup>Sr,  $\delta^{18}$ O and  $\delta^{13}$ C performed at the University of Cambridge allows a reconstruction of the evolution of the isotopic composition of CO<sub>2</sub>-charged groundwaters, sourced from the Navajo Aquifer, over the ca 413 ka year leakage history (Burnside, 2009) recorded in these deposits.

Detailed petrology, cathodoluminescence and SEM mapping of thin sections, and EDS, XRD and XRF were used to characterize the mineralogy of the original host rock and the mineralogical products of interaction with CO<sub>2</sub>-charged fluids. Detailed compositional analysis of the carbonate minerals can be used to constrain the chemistry of the parent fluid, Eh-pH conditions prevailing during its deposition and to asses the role of kinetic processes in controlling carbonate formation and to quantify their precipitation rates. A petrological and isotopic study of carbonate mineral products within the fault zones was carried out in order to investigate the following:

1) What was the nature and origin of the fluid associated with ancient travertine deposition and did that fluid vary compositionally with time (i.e. modification of major chemistry through fluid-mineral reactions; degassing or carbonate precipitation modification of the  $\delta^{13}C_{DIC}$ ? Was it compositionally similar to the active CO<sub>2</sub> system?

- 2) What were the Eh-pH conditions prevailing in the ancient CO<sub>2</sub>-charged groundwaters? Were the groundwaters sufficiently reduced, due to low dissolved oxygen content, that pH suppression due to high concentrations of dissolved CO<sub>2</sub>, was sufficient to dissolved hematite grain coatings?
- 3) What geochemical factors control the mineralogy, chemistry and rates of carbonate cementation in travertine feeder zones? Can carbonate chemistry be used to infer carbonate precipitation rates and if so how do these rates compare to predictions from experimental studies on surface controlled mineral precipitation rates? What geochemical factors, such as the presence of inhibiting ions, the state of saturation with respect to carbonate and the degree of CO<sub>2</sub>-degassing, are most important in controlling precipitation rates?
- 4) What are the timescales of active  $CO_2$  injection, from deeper formations, into the Navajo Aquifer? Does surface leakage occur immediately upon injection of  $CO_2$  into the Navajo Aquifer or is there a delay reflecting the time required for physical and geochemical interactions to occur, facilitating leakage? How long does this  $CO_2$ -charge take to dissipate? Is there a coupling between  $CO_2$  injection, surface leakage and the rate of mineral- and gas-fluid reactions?
- 5) What controls the spatial and temporal distribution of leakage sites? Do these sites vary as a result of geochemical processes, such as the plugging of leakage pathways by carbonate deposition? Are overall properties of the fault lithologies, fault architecture and local hydrology important in controlling rates of leakage?

## 4.3. Methodology

#### 4.3.1. Isotopic Systems and Fluid Rock Interaction

When information is desired regarding the past properties of a hydrological system information recorded in minerals deposited in past regimes is of great value (e.g. Bottomley and Veizer, 1992; Hendry and Marshall, 1991; Marshall *et al.*, 1992, Paces *et al.*, 1994; Whelan and Stuckless, 1992). The stable-isotope geochemistry of carbonate phases can be analyzed to help constrain pore-water evolution. The isotope ratios of O and C record the isotope ratios of the parent fluid, modified by temperature-dependent fractionations. Oxygen isotopic signatures may provide information about fluid flow, fluid sources and fluid–rock interaction (e.g. Burkhard and Kerrich, 1988; Burkhard *et al.*, 1992; Janssen *et al.*, 1997, 1998). Commonly pore waters can be attributed to end-member compositions (e.g. meteoric, seawater, basinal brine) or to mixing lines between these end member compositions (e.g. Lee and Krothe, 2001).

The carbon isotopic signature of carbonate can be used to study the origin and evolution of the pore water carbon reservoir from which inferences about the nature of the original carbon source can be made, if precipitation temperature can be independently estimated. Further, the stable isotopic composition of the parent fluid may be fractionated by reactions resulting from
physical processes, such as volatile loss and mineral precipitation, important for understanding the physical and geochemical controls on fluid chemistry and the evolution of pore fluid chemistry and mineral products as a result of these processes.

The isotope ratios of Sr and other 'nonfractionating' elements in solution deposited minerals are always equal to those of the parent water; thus these isotope ratios directly record water conditions prevailing at the time of precipitation, with possible alteration due to subsequent cation exchange. The <sup>87</sup>Sr/<sup>86</sup>Sr ratios in groundwater reflect the water-rock reaction histories and flow pathways of the waters and the mixing of distinct water sources. Several studies have used <sup>87</sup>Sr/<sup>86</sup>Sr as a natural tracer of groundwater flow and fluid-rock interaction (e.g., Blum *et al.*, 1993; Bullen *et al.*, 1997; Clow *et al.*, 1997; Johnson and DePaolo, 1994; Katz and Bullen, 1996; Musgrove and Banner, 1993). <sup>87</sup>Sr/<sup>86</sup>Sr in groundwater evolve toward the ratio of Sr acquired from the host rock, primarily from silicate minerals (e.g. plagioclase, K-feldspar, mica). Although <sup>87</sup>Sr is radiogenic the roughly forty seven billion year half life of the decay process is so long that on the timescale of groundwater evolution, <sup>87</sup>Sr/<sup>86</sup>Sr of Sr sources is essentially stable.

### 4.3.2. Faults and CO<sub>2</sub> Leakage

Fluid infiltration into faults and the resulting fluid–rock interaction influence the chemical and mechanical behaviour of faults (Hubbert and Rubey, 1959). In particular, elevated pore fluid pressures, which reduce the effective confining stress and allow frictional slip at low fault stress, have been invoked to explain the remarkable weakness of major fault zones (Chester *et al.*, 1993; Chester and Logan, 1986; Lachenbruch and Sass, 1980; Miller *et al.*, 1996). Since areas of CO<sub>2</sub> discharge globally coincide with regions of seismic activity, CO<sub>2</sub> exsolution may increase pore fluid pressures within fault zones (e.g. Barnes *et al.*, 1978; Irwin and Barnes, 1975), and corrode minerals comprising the fault surface, inducing fault weakening (Kennedy *et al.*, 1997). Recent detailed studies on fault zones have revealed that faults act both as important fluid conduits during fault-related deformation and as barriers to fluid flow (Caine *et al.*, 1996). This conduit-barrier behaviour of faults varies in space and time during the active fault stages (Goddard and Evans, 1995; Logan and Decker, 1994). Structural and geochemical studies have been used to characterize fault-related alteration processes both along and across major fault zones (e.g. Chester, 1994; Cox, 1995; Hadizadeh, 1994)

### **4.3.3.** Isotopes: Equilibrium versus kinetic fractionation

### 4.3.3.1. Carbon Isotopes

Various mechanisms can lead to the precipitation of calcium carbonate from groundwaters. Precipitation of calcite can precede either by slow reactions close to equilibrium or by rapid irreversible reactions. In the first forward and backward reaction rates are almost equal. The products formed escape from the solution and do not interact with it again. Under such conditions the products are in carbon and oxygen isotopic equilibrium with the solution, when they are generated. This, however, requires slow deposition rates, whereby the Ca-concentration at the surface of the solid must be close to saturation with respect to calcite. The fractionation factors  $\alpha_{eq}$  in this case are the corresponding equilibrium values. For the carbonate system, in the pH range of interest, they can be defined from experimental studies (Clark and Fritz, 1997; Deines *et al.*, 1974; Romanek, 1992) as:

$$10^{3} \ln \alpha_{CO_{2}(aq)-CO_{2}(g)} = -0.373 \times 10^{3} T^{-1} + 0.19$$
(4.1)

$$10^{3} \ln \alpha_{H_{2}CO_{3}-CO_{2}(g)} = \left(-0.91 + 0.0063 \times 10^{6}\right) / T^{2}$$
(4.2)

$$10^{3} \ln \alpha_{HCO_{1}^{-}-CO_{1}(g)} = 9.552 \times 10^{3} T^{-1} - 24.1$$
(4.3)

$$10^{3} \ln \alpha_{cc-CO_{2}(g)} = 2.988 \times 10^{6} T^{-2} - 7.6663 \times 10^{3} T^{-1} + 2.4612$$
(4.4)

$$10^{3} \ln \alpha_{arag-CO,(g)} = 13.88 - 0.13 \times T \tag{4.5}$$

$$\delta^{13}C_{dol} - \delta^{13}C_{HCO3^{-}} = 38.832 - \frac{31.506 \times 10^3}{T} + \frac{7.698 \times 10^6}{T^2} - \frac{0.388 \times 10^9}{T^3}$$
(4.6)

Where

$$\alpha_{CO_2(aq)-CO_2(g)} = \left(\delta^{13}C_{CO_2(aq)} + 1000\right) / \left(\delta^{13}C_{CO_2(g)} + 1000\right)$$
(4.7)

$$\alpha_{H_2CO_3 - CO_2(g)} = \left(\delta^{13}C_{H_2CO_3} + 1000\right) / \left(\delta^{13}C_{CO_2(g)} + 1000\right)$$
(4.8)

$$\alpha_{HCO_{3}^{-}-CO_{2}(g)} = \left(\delta^{13}C_{HCO_{3}^{-}} + 1000\right) / \left(\delta^{13}C_{CO_{2}(g)} + 1000\right)$$
(4.9)

$$\alpha_{CaCO_3 - CO_2(g)} = \left(\delta^{13}C_{CaCO_3} + 1000\right) / \left(\delta^{13}C_{CO_2(g)} + 1000\right)$$
(4.10)

can be employed to yield the individual equilibrium fractionation factors between all of the various carbonate species and from which the isotopic composition of  $HCO_3^-$  in equilibrium with measured values of calcium carbonate  $\delta^{13}C$  can be estimated.

For non-equilibrium fractionation the other extreme is irreversible fast precipitation as a consequently of rapid changes in solution composition which produce and maintain an elevated saturation state of calcium carbonate ( $\Omega_{cc}$ ). Such processes include very rapid changes in pH via H<sup>+</sup> consuming mineral dissolution reactions with fast kinetics and CO<sub>2</sub> degassing. Three

processes determine the value of the rate constant of calcium carbonate precipitation: (a) the precipitation kinetics at the surface of the mineral. (b) Mass transport of the reacting species from and towards this surface, respectively. (c) The slow conversion of  $HCO_3^-$  to  $CO_2$  and the chemical reactions of carbonate chemistry (Buhmann and Dreybrodt, 1985; Dreybrodt, 1988, Dreybrodt *et al.*, 1996). Such irreversible processes result in kinetic fractionation with different fractionation factors  $\alpha_{kin}$ , caused by the different reaction rates of the light and the heavy molecules (Zeebe and Wolf-Gladrow, 2001). However, the magnitude of these fractionations is largely unknown.

### 4.3.3.2. Oxygen Isotopes

During calcium carbonate precipitation, in contrast to carbon where all atoms are contained in  $HCO_3^-$  and  $CO_2(aq)$  molecules and to a negligible amount in  $CO_3^{2^-}$ , the oxygen atoms are exchanged not only within the carbonate species but also with the huge amount of oxygen atoms in the water. These represent a large reservoir with about  $10^4$  times more atoms than contained in the carbonate species.

The oxygen isotopic composition of water in equilibrium with calcite, aragonite and dolomite can be derived from (Kim and O'Neil, 1997, 2007; Zhou and Zheng, 2003):

$$10^{3} \ln \alpha_{cal-H_{2}0} = 18.03 \times 10^{3} T^{-1} - 32.42$$
(4.11)

$$10^{3} \ln \alpha_{arag-H_{2}O} = 20.44 \times 10^{3} / T^{-1} - 41.48$$
(4.12)

$$10^{3} \ln \alpha_{dol-H,0} = 2.73 \times 10^{6} T^{-2} + 0.26 \tag{4.13}$$

Equilibrium isotopic fractionation between  $HCO_3^-$  and  $H_2O$  can be assumed in instances where the precipitation rate of carbonate is sufficiently slow to allow equilibration of  $HCO_3^-$  in solution with  $H_2O$ . Since the slowest of the reactions taking place in solution during the precipitation of calcium carbonate is the dehydration of bicarbonate ions, and the hydration of aqueous carbon dioxide (Williams, 1983) and since this is the only step in which isotopic exchange can take place between the oxygen of the water and the oxygen of the carbon compounds in solution, equilibrium between these species is necessary for the carbonate to be precipitated in oxygen isotopic equilibrium with the water. Positively correlated  $\delta^{18}O$  versus  $\delta^{13}C$  with a slope that deviates from that expected for changes in fractionation due to temperature variations is a general indication that kinetic processes may ultimately govern  $\delta^{18}O_{CaCO3}$ .

### **4.3.4.** Carbonate Precipitation in CO<sub>2</sub>-rich Fluids

Dissolved  $CO_2$  will react with divalent cations, in solution, to form carbonate minerals (e.g. calcite, siderite, magnesite) which will form a sink of  $CO_2$  from the fluid. Overall reaction

stoichiometries show that calcite precipitation consumes bicarbonate ion while either increasing acidity in a closed system or liberating  $CO_2(g)$  in a system open to  $CO_2$  loss (i.e.  $CO_2$  degassing):

$$Ca^{2+} + 2HCO_3^- \leftrightarrow CaCO_3(s) + H^+ + HCO_3^-$$

$$(4.14)$$

$$Ca^{2+} + 2HCO_3^- \leftrightarrow CaCO_3(s) + H_2O + CO_2(g)$$

$$(4.15)$$

Increase in  $HCO_3^-$  concentrations,  $Ca^{2+}$  liberation and  $H^+$  consumption through mineral dissolution, or  $CO_2$  loss through degassing, drives overall equations (4.14) and (4.15) to the right, resulting in the precipitation of calcite.

Rates of these reactions are known to be fast, relative to the slow kinetics of  $CO_2$  dissolution and aqueous speciation, but have a complex dependence on reactant concentrations, in situ pH, temperature and fluid composition (e.g. Morse 1986; Mucci and Morse, 1983. 1984; Zuddas and Mucci 1998). Additionally, carbonate precipitation rates may be ultimately limited by solute supply and solute transport, as apposed to true mineral surface reaction (e.g. Given and Wilkinson, 1985; Lee *et al.*, 1996; Wilkinson and Dampier, 1990).

Surface controlled mineral precipitation and dissolution rates have most often been expressed in terms of a disequilibrium functional dependence. Since the net growth rate of calcium carbonate is, a priori, a function of calcium and bicarbonate concentrations, rate data has been commonly fitted to the following rate equation (Arvidson and Mackenzie, 2000; Berner and Morse, 1974; Gledhill and Morse, 2006; Morse and Arvidson, 2002; Nancollas and Reddy, 1971):

$$R = k(\Omega_{cc} - 1)^n \tag{4.16}$$

or its logarithmic form:

$$\log R = \log k + n \log \left(\Omega_{cc} - 1\right) \tag{4.17}$$

where *R* is the precipitation rate normalized to the reacting surface area (mol m<sup>-2</sup> s<sup>-1</sup>), *k* is the rate constant, *n* is the order of the overall reaction (Lee and Morse, 1999; Morse, 1987; Mucci and Morse, 1984; Nancollas and Reddy, 1971) and  $\Omega_{cc}$  is the saturation state defined as

$$\Omega_{cc} = \frac{\left[HCO_{3}^{-}\right] \cdot \left[Ca^{2+}\right]}{K_{cc}^{*} \cdot \left[H^{+}\right]}$$
(4.18)

where  $K_{cc}^{*}$  is the calcite stoichiometric solubility constant at a given temperature, and [HCO<sub>3</sub><sup>-</sup>] and [Ca<sup>2+</sup>] are the bicarbonate and calcium ion concentrations, respectively. This model is commonly adopted for precipitation from aqueous solutions of minerals such as calcite and

involves alternating incorporation of cations and anions (Ca<sup>2+</sup> and CO<sub>3</sub><sup>2-</sup>) into the lattice. In this case, the growth rate also depends on the relative abundance of the cations and anions in solutions in addition to  $\Omega_{cc}$ .

Within porefluids at, or close to saturation with  $CO_2$  the  $[HCO_3^-] \gg [Ca^{2+}]$  and the macroscopic variation in carbonate precipitation rates will be partly limited by the availability of  $Ca^{2+}$  and other divalent ions. Given the order of magnitude differences between  $[HCO_3^-]$  and  $[Ca^{2+}]$  in typical porefluids the microscopic variability in precipitation rate will be governed by variation in  $\Omega_{cc}$  due to variable activities of  $[HCO_3^-]$  and  $[H^+]$ . Variation in  $[HCO_3^-]$  and  $[H^+]$  will primarily be caused by changes in  $pCO_2$ , the extent of reaction and the degree of pH buffering.

Numerous studies (e.g. Dreybrodt *et al.*, 1992; Herman & Lorah, 1987, 1988; Lorah & Herman, 1988; White, 1997) show that calcite does not precipitate instantaneously at the point of saturation. Precipitation requires a finite supersaturation because of activation barriers to calcite nucleation and crystal growth (White, 1997). Activation barriers may also be accompanied by calcite inhibitor ions, e.g. Mg (Arvidson *et al.*, 2006; Berner, 1975; Bischoff, 1968; Pytkowicz, 1965), or the presence of organic matter (Berner, 1975; Raiswell & Fisher, 2004). In most circumstances this implies a saturation index ( $SI_{cc}$ ) of +0.5, although Dreybrodt *et al.*, (1992) suggest that saturation indices of at least +1.0 are required.

The rate of calcite growth in porefluids is strongly influenced by its relative supersaturation, the  $pCO_2$ , the concentration of inhibitor ions and organic molecules and the trace ion/Ca<sup>2+</sup> of the parent fluid (Arvidson et al., 2003; Busenberg and Plummer, 1986; House et al., 1981; Inskeep and Bloom, 1985; Morse, 1983; Nancollas and Reddy, 1971; Reddy et al., 1981; Shiraki and Brantley, 1995; Zhong and Mucci, 1993; Zuddas and Mucci, 1994). It is expected that, in fluids with complex chemistry calcite precipitation will be suppressed by a decrease in the density of active growing sites due to the blocking of growth steps and kink sites by the adsorption of divalent ions such as Fe<sup>2+</sup>, Mn<sup>2+</sup> and Mg<sup>2+</sup> (Chen et al., 2006; Dromgoole and Walter, 1990b; Gutjahr et al., 1996; Katz et al., 1993; Meyer, 1984; Reddy and Wang 1980). This effect decreases with increasing super-saturation due to higher intrinsic growth rates and the rapid 'burial' of the absorbed ion. The ratio of trace ion (Tr) concentrations of components forming solid solutions with that of the pure endmember,  $Tr^{2+}/Ca^{2+}$ , (e.g.  $Mg^{2+}$ ,  $Mn^{2+}$ ,  $Fe^{2+}$ ) have been shown to lower calcite precipitation rates where the concentration of the trace ion in the parent fluid is high and where the solubility of the  $TrCO_3$  endmember is greater than that of pure calcite (Berner, 1975, Dromgoole & Walter, 1990b; Meyer, 1984; Mucci, 1988). This may be especially important in diagenetic systems where  $Fe^{2+}$  and  $Mn^{2+}$  concentrations in pore fluids can be large. Additionally the precipitation kinetics of calcite increase with increasing  $pCO_2$  at (constant supersaturation) due to an increase in the activity of the component carbonate species in solution. Water soluble organic ligands and ions such as  $PO_4^{3-}$  and  $SO_4^{2-}$  have been known to act as precipitation inhibitors by blocking crystal growth sites (Katz *et al.*, 1993; Kitano and Hood, 1965; Paquette *et al.*, 1996; Reddy, 1977)

### 4.3.5. Carbonate Cement Compositions

Interpreting the mode and environment of formation of secondary carbonates deposited from  $CO_2$ -charged fluids is best achieved by examination of the chemical and isotopic composition of the secondary phases themselves. Minor and trace element contents (Mg, Fe, Mn, Sr, Ba, Na, K) of carbonate cements reflect pore water chemistries prevailing during carbonate precipitation (e.g. Rimstidt, 1998; Veizer, 1983). The systematic dependence of the coprecipitation of these 'foreign' ions in calcite, dolomite and aragonite with various physical and chemical processes provides an important tool in understanding paleo-fluid chemistry and the pathways by which fluid-mineral reactions have occurred. Numerous studies have focused on the measurement and application of partition coefficients, which relate the composition of the carbonate mineral to that of the solution from which it predicated (e.g. Brand and Veizer, 1980; Budd et al., 1993; Fairchild et al., 2000; Oomori et al., 1987). For instance, the temperature dependence of  $Mg^{2+}$ incorporation into the calcite lattice makes it an important tool in interpreting paleo-temperatures (e.g. Morse *et al.*, 1997). Efforts have been made to use the Na<sup>+</sup> contents of carbonates as indicators of paleosalinities and salinity (e.g. Veizer et al., 1977; Ishkawa and Ichikumi, 1984) but Na probably occupies interstitial positions in the calcite structure and its incorporation is thus partly dependent on the number of surface defect sites (see Busenberg and Plummer, 1984).

Concentrations of the redox sensitive elements Fe and Mn in calcite have been used, in conjunction with cathodoluminescence (CL) microscopy, to interpret paleo-redox conditions of pore waters prevailing during diagenesis (see Barnaby and Rimstidt, 1989 for a thorough review). Variation in CL brightness is primarily a function of Fe<sup>2+</sup> and Mn<sup>2+</sup> content, with Fe<sup>2+</sup> the main quencher and Mn<sup>2+</sup> the main activator of luminescence (Sommer, 1972; Fairchild, 1983; Machel, 1985; Mason, 1987). Natural calcite cements may contain 1000's of ppm Fe or Mn, and a minimum of ~ 10 ppm Mn is necessary to activate CL (Ten Have and Heijnen, 1965). Variations in CL brightness may record changes in Fe<sup>2+</sup> and Mn<sup>2+</sup> concentrations which reflect changes in the Eh-pH conditions of the parent fluids (e.g., Frank *et al.*, 1982).

The equilibrium partitioning of a component between two phases can be represented as a simple chemical reaction:

$$X_{phaseA} \leftrightarrow X_{phaseB} \tag{4.19}$$

With an equilibrium constant (K) for the reaction of:

$$K = a_{X_{phaseA}} / a_{X_{phaseB}} \tag{4.20}$$

Where  $a_X$  is activity and the equilibrium constant *K* is equivalent to a distribution coefficient of *X* between the two phases. This equilibrium constant can only be equal to the concentration ratio of *X* in the two phases when the activity coefficient of X in both phases is unity (or the same). Given the difficulty in determining activities and the non-equilibrium state of many experimental and natural systems the concentration of a trace component (*Tr*) is typically related to a carrier component (*Cr*) in the solid (*S*) and liquid (*L*) phases (e.g. Ca<sup>2+</sup>) by the non-thermodynamic partition coefficient, *D*, where:

$$D = \frac{\left(Tr / Cr\right)_{s}}{\left(Tr / Cr\right)_{L}}$$
(4.21)

*D* can be theoretically related to a true thermodynamic equilibrium constant by solid ( $f_i$ ) and liquid ( $\gamma_i$ ) activity coefficients (after Morse and Bender, 1990). Using the exchange reaction for a hypothetical trace component (*Tr*) in calcite as an example, we have:

$$Tr^{2+} + CaCO_3 \leftrightarrow Ca^{2+} + TrCO_3 \tag{4.22}$$

$$K_{d} = \frac{a_{Ca^{2*}}a_{TrCO_{3}}}{a_{Tr^{2*}}a_{CaCO_{3}}}$$
(4.23)

$$=\frac{\left(a_{T_{rCO_{3}}}/a_{CaCO_{3}}\right)}{\left(a_{T_{r}^{2^{*}}}/a_{Ca^{2^{*}}}\right)}$$
(4.24)

$$=\frac{\left(f_{T_{TCO_{3}}}m_{T_{TCO_{3}}}/f_{CaCO_{3}}m_{CaCO_{3}}\right)}{\left(\gamma_{T_{r^{2*}}}m_{T^{2*}}/\gamma_{Ca^{2*}}m_{Ca^{2*}}\right)}$$
(4.25)

and

$$D = \frac{\left(\frac{m_{Tr}}{m_{Ca}}\right)_{calcite}}{\left(\frac{m_{Tr}}{m_{Ca}}\right)_{L}}$$
(4.26)

Since the molar ratios of Tr to Ca in the solid phase and TrCO<sub>3</sub> to calcite are the same, D is related to  $K_d$  as:

$$D = K_d \left[ \frac{\left( \gamma_{Tr^{2+}} / \gamma_{Ca^{2+}} \right)}{\left( f_{TrCO_3} / f_{CaCO_3} \right)} \right]$$
(4.27)

Taking the activities of the solid phases as unity and substituting (4.26) into (4.27) we have:

$$\left(m_{Tr}/m_{Ca}\right)_{calcite} = K_d \left(\gamma_{Tr^{2+}}/\gamma_{Ca^{2+}}\right) \cdot \left(m_{Tr}/m_{Ca}\right)_L$$

$$(4.28)$$

The dependence of partition coefficients on both the crucial thermodynamic properties of pressure, temperature and composition and the kinetics of carbonate precipitation have been determined for a number of minor and trace elements in calcite: Mg and Sr (Gascoyne, 1982; Huang and Fairchild, 2001; Lorens, 1980; Mucci and Morse, 1982; Oomori et al., 1987; Pingitore and Eastman, 1986; Tesoriero and Pankow, 1996); Mn and Fe (Böttcher, 1998; Dromgoole and Walter, 1990a; Lorens, 1978, 1981; Mucci, 1988, Pingitore et al., 1988); Ba (Tesoriero and Pankow, 1996; Tunusoglu, 2007); Na (Busenberg and Plummer, 1986; Ishkawa and Ichikumi, 1984); and some trace elements (Zhong and Mucci, 1989, 1995). Experimentally determined partition coefficients for minor and trace element incorporation in dolomite and aragonite (Busenberg and Plummer, 1984; Gaetani and Cohen, 2006; Kinsman and Holland, 1969; Zhong and Mucci, 1989), are less ubiquitous or are absent and as such values must be determined from theoretical thermodynamic calculations (e.g. Curti, 1999, Wang and Xu, 2001). However, given its easy substitution for Ca, Sr incorporation in aragonite (Kinsman and Holland, 1968; Gabitov et al., 2008; Gaetani and Cohen, 2006) and dolomite (Baker and Burns 1985; Vahrenkamp and Swart, 1990) is reasonably well constrained. The application of experimentally determined  $(K_{d})$ values or those based on thermodynamic calculations of mineral solubilities are complicated by the fact that true thermodynamic equilibrium is rarely attained in low temperature experimental or natural systems.

Kinetic processes effecting the distribution of trace elements within precipitating carbonate crystals include the tendencies of Ca and *Tr* to attach at kink sites on the growth steps of an actively growing crystal (Watson and Liang, 1995, Rakovan and Reeder 1996). This is due to differences in the surface energies of different absorption sites in the crystal. This process results in heterogeneous trace element distributions and sector and intersectoral zoning in carbonate crystals due to the low rates of diffusion of trace elements in the solid phases relative to the rates of crystal growth (Rakovan and Reeder 1996).



**Figure 4.3-1** The dependence of  $D_{Sr}$  on the precipitation rate of calcite at various fluid Mg/Ca. Compiled from Mucci (1986) and Mucci and Morse (1983).

The second process is related to surface-solution boundary processes which result in the incorporation of Tr into the growing crystal at a different rate to the incorporation of Ca, so that (mTr/mCa) ratio is either large or smaller than the contacting solution. This differential incorporation is dependent on the rate of transport of the ions from the solution to the mineral surface (Lasaga, 1981; 1982).

Experimental distribution coefficient show a systematic pattern of behaviour that differs from that expected if the distribution were controlled by equilibrium thermodynamics alone (Rimstidt *et al.*, 1998), suggesting that experiments are effected by kinetic processes. As such calculations of pore fluid chemistry from carbonate cement composition using equilibrium distribution coefficients can predict general trends but they must be tempered with an understanding of the kinetic processes affecting the specific system of interest. This does however allow the Tr/Ca of calcite to be used to infer precipitation rates where the original fluid Tr/Ca value is know and the dependence of  $D_{Tr}$  on precipitation rate is experimentally well constrained.

In the case of calcite, the value of trace element partition coefficients varies with increasing rate of precipitation in a systematic manner (Beck *et al.*, 1992; Kinsman and Holland, 1969; Lorens, 1981; Morse and Bender, 1990; Mucci, 1986; Pingitore and Eastman, 1986). Mucci (1986) precipitated magnesian calcites at room temperature from solutions of various  $[Mg^{2+}]/[Ca^{2+}]$  and at  $\Omega_{cc}$  values ranging from 2.0 to 14.4. The results, combined with those of Mucci and Morse (1983) (Fig. 4.3-1) were used to obtain the empirical relationship

$$D_{\rm sr} = 0.65973 + 0.06591 \cdot \log R \tag{4.29}$$

where *R* is the precipitation rate in mol/m<sup>2</sup>/sec,  $D_{Sr}$  is the Sr/Ca<sup>cc</sup> partition coefficient, at a  $[Mg^{2+}]/[Ca^{2+}]$  of 1.0. It is noted that the exact nature of this rate-dependence is not clear, nor are the effects of Mg and *p*CO<sub>2</sub> rigorously known. Eq. (4.29) is the result of a least square fit with a correlation coefficient of 0.60. Beck *et al.*, (1992) in agreement with the results of Mucci and Morse (1983, 1990) and Jacobson and Usdowski (1976), reported no significant effect on  $D_{Sr}$  due to increase in pressure. These workers observed only a slight increase in  $D_{Sr}$  value with increasing temperature in experiments carried out to 400°C and 10 MPa.

### 4.3.6. Redox

Various studies (Carpenter and Oglesby, 1976; Grover and Read, 1983; Niemann and Read 1988; Oglesby, 1976) have suggested that progressive changes in Fe and Mn contents reflect variation in porewater pH and Eh during diagenesis. Implicit in this geochemical model is the assumption that the Mn<sup>2+</sup> and Fe<sup>2+</sup> concentrations in the fluid were governed by equilibrium reactions with Mn- and Fe-bearing mineral phases whose solubilities were controlled by the pH and Eh conditions of the groundwater and that these minerals were present in the system during the precipitation of carbonate. The Mn and Fe content of this pore water is determined by the Mn/Ca and Fe/Ca ratios of the calcite precipitate and the corresponding distribution coefficients  $D_{Mn}$  and  $D_{Fe}$ . Application of Eq. (4.27) requires knowledge of the  $aCa^{2+}$  in pore waters and activity coefficients for  $Ca^{2+}$ ,  $Mn^{2+}$  and  $Fe^{2+}$ . Given the apparent similarity of chemistry of modern  $CO_2$ charged fluids and those responsible for calcite deposition (see section 4.4.3) Ca concentration and activity coefficients from the modern fluid have been used in the calculation of element distributions in calcite cements. The distribution coefficients for Mn and Fe in calcite are influenced by precipitation rate (Dromgoole and Walter, 1990a; Lorens, 1981; Mucci, 1988) and temperature (Bodine et al., 1965). Lorens (1981) indicated that  $D_{Mn}$  varies from 5 at rapid precipitation rates to almost 70 at very slow rates of precipitation. A similar behaviour is observed for  $D_{Fe}$  (Lorens, 1981). In subsequent calculations values of  $D_{Mn} = 7$  and  $D_{Fe} = 3$  were used. If the effective distribution coefficients for Mn and Fe during calcite precipitation varied by even an order of magnitude from these values due to rate effects, the estimated solution Eh and pH would be in error by only 0.06 volts and 0.25 pH units, respectively. This would not significantly effect the conclusions about approximate Eh & pH ranges of paleo-CO<sub>2</sub>-charged fluid. Temperature is not of a significant concern given the narrow range of temperatures observed in modern CO<sub>2</sub>-charged fluids and the lack of a significant variation in  $D_{Mn}$  and  $D_{Fe}$  at temperatures lower than 100°C (Bodine et al., 1965)

### 4.3.7. Eh-pH Diagrams

The redox couples of interest  $Fe^{2+}/Fe_2O_3$  and  $Mn^{2+}/MnO_2$  more closely approximate equilibrium with respect to measured Eh than to Eh computed from other parameters such as dissolved  $O_2$ (Lindberg and Runnells, 1984). It is thus reasonable to conclude that Pt electrode measured Eh closely resembles groundwater Eh as reflected by the Fe and Mn equilibria, and that redox conditions inferred on the basis of calcite Fe and Mn contents should be compatible with measured Eh values for modern  $CO_2$ -charged fluids. A crucial component of this model is the identification of the correct redox coupled Mn- and Fe-oxyhydroxide phases whose solubilities govern the fluid Mn and Fe content. For the Navajo and Entrada Sandstones the potential Feoxyhydroxide phases include hematite, goethite, magnetite and amorphous ferric hydroxide; potential Mn-oxyhydroxides include pyrolusite, manganite, amorphous MnO<sub>2</sub> and 'complex' MnO<sub>2</sub> (Chan, 2000).

Identification of the oxyhydroxide phases controlling groundwater Fe<sup>2+</sup> and Mn<sup>2+</sup> content can be made based on the assumption that Mn and Fe contents are controlled by equilibrium with an appropriate oxyhydroxide and that measured spring Eh and pH values adequately reflect subsurface Eh/pH conditions. Superposition of measured Eh-pH values for CO<sub>2</sub>-chraged fluids, with the stability boundary of hematite, and its ubiquitous presence in these sediments suggest this phase largely controls fluid Fe (Chapter 2, section 2.4.7). Manganese chemistry in natural systems is complex and not well understood (e.g. Barnaby and Rimstidt, 1989; Bricker, 1965; Potter and Rossman 1979). Mn exists in several possible oxidation states and commonly forms complex nonstoichiometric oxyhydroxides, with highly variable crystallinity (Ponnamperuma *et al.*, 1969). Detailed studies of Mn-oxide mineralogy from various sedimentary environments indicate that insoluble Mn oxides other than pyrolusite (MnO<sub>2</sub>) are the dominant controls on dissolved Mn (see Taylor *et al.*, 1964). Consequently it is assumed that Mn<sup>2+</sup> concentrations are controlled by equilibrium with a relatively insoluble 'complex' MnO<sub>2</sub> phase. Details of the calculation of the solubility of this phase are presented in Appendix C.

Relating values for measured Eh in CO<sub>2</sub>-charged waters to activities of redox elements in solution may be problematic given that internal disequilibrium for any given redox couple is common (Lindberg and Runnells, 1984); however given the time scale of groundwater residence (>10<sup>3</sup> yrs), redox reactions between cations in solution are comparatively instantaneous (e.g. Basolo and Pearson, 1967); furthermore, the dissolution and precipitation rates of Fe- and Mn-oxyhydroxides are also fast (e.g. Cornell and Giovanoli, 1993; Melbourne *et al.*, 1991; Surana and Warren, 1969; Schwertmann, 1991). Thus it is reasonable to assume redox equilibria between groundwaters and oxyhydroxide phases and that Fe and Mn contents of authigenic calcite will reflect this fact.

### 4.3.8. Analytical Methods

Representative thin sections of altered and unaltered Entrada sandstone and veins were qualitatively investigated petrographically using transmitted light microscopy. Percent mineralogy and porosity were estimated by point counting (200 points) at a spacing of 0.1 mm, on representative samples. Polished thin sections were examined with cathodoluminescence using a cold cathode machine and a mono-CL attached to a Jeol JSM 6100 SEM. SEM imaging and SEM-EDS analyses were undertaken on flat, well-polished specimens following Reed, (2005). Samples were analysed using a Jeol JSM 6100 scanning microscope, combined with an Oxford Instruments INCA EDS suite. The accelerating voltage for X-ray intensity measurement and for SEM image capture was 15 kV, using a probe current of 0.3 nA and a mean dead time of 20%. Xray diffraction analysis was conducted on a Bruker AXS D8 diffractometer at the University of Cambridge. Diffraction patters were recorded by step scanning from 2-80°20, with a step size of 0.013605° and counting for 0.7s per step. The Eva 9.0 software by SOCABIM (2003) was used to identify the mineral phases. The major and minor element chemistry of carbonate cements and veins were analysed using a Cameca SX-100 electron microprobe. The operation conditions were a filament voltage of 15 kV and a current of 10 nA with a beam diameter of 5.5 µm for the carbonates. Whole rock major element concentrations were determined by X-ray fluorescence (XRF) spectrometry at the Open University. Analyses were performed on fused discs following Potts et al., (1984). Modal mineralogy was calculated from least squares mixing of mineral proportions to match whole rock compositions using the method of Hermann & Berry, (2002).

Carbon and oxygen isotopes, <sup>18</sup>O/<sup>16</sup>O and <sup>13</sup>C/<sup>12</sup>C, were measured in carbonates from cements and veins. Powdered carbonate micro-samples (~0.5g) taken from homogenized bulk samples (15g) were reacted at 90°C in pure orthophosphoric acid. The resultant CO<sub>2</sub> gas was purified cryogenically and analyzed for <sup>18</sup>O/<sup>16</sup>O and <sup>13</sup>C/<sup>12</sup>C using a Thermo Finnigan MAT253 Gas Bench II stable isotope mass spectrometer.  $\delta^{13}$ C and  $\delta^{18}$ O are expressed in  $\delta\%_0$  deviation relative to Peedee Belemnite (PDB) and VSMOW standards with analytical precisions, based on the repeat analysis of in house standards, estimated at ±0.06 and ±0.08 %<sub>0</sub> respectively (1 $\sigma$ ).

Samples of U-series dated aragonite veins provided by Neil Burnside, University of Glasgow, were analyzed for <sup>87</sup>Sr/<sup>86</sup>Sr,  $\delta^{18}$ O and  $\delta^{13}$ C. Chips taken from dated samples were ground to a powder and duplicated 0.3 to 0.5 mg samples were taken for analysis. The samples were analyzed using a Thermo Gas Bench attached to a Thermo MAT 253 mass spectrometer in continuous flow mode. Results are quoted to the international standard VPDB and the precision is better than ±0.10 %<sub>0</sub> for  $\delta^{18}$ O and better than ±0.06 %<sub>0</sub> for  $\delta^{13}$ C (1 $\sigma$ ). Results are reported as averages of the two analyses. Approximately 0.3 g of each sample was dissolved in 6 M HCl in Teflon beakers for the analysis of <sup>87</sup>Sr/<sup>86</sup>Sr. The solutions were evaporated to dryness on a hot plate at approximately 70°C. Each residue was dissolved in 1 M HCl and 0.4 ml was loaded on a

cation-exchange resin column to separate Sr from Ca and Rb. Eluant was 3 M HCl. The strontium-containing volume of eluant was then evaporated to dryness. After final evaporation to dryness the sample was dissolved in 1 M HNO<sub>3</sub> and approximately 0.5  $\mu$ g of strontium were loaded on a single tungsten filament. Isotopic analyses were performed on the T40 Sector 54 VG mass spectrometer at Cambridge following Bickle *et al.*, (2003). Analyses of NBS987 gave 0.710258 ± 0.000008 (1 $\sigma$ , *n* =20) over the period in which the samples were analysed.

# 4.4. Results and Discussion

### 4.4.1. Field Observations

Exposed along Little Grand Fault and the northern fault of Salt Wash Graben are a series of partial to complete remnants of ancient travertine deposits that parallel the fault trace (Fig. 4.4-1). The ancient travertine deposits form resistant caps to sandstone buttes and are topographically higher than modern, actively-forming travertines. All deposits originate in the footwall proximal to areas where the fold axis of the Green River anticline is cut by normal faults. However, there are variations in the distribution and development of the ancient deposits between the two faults. The Little Grand Fault contains a series of discrete, well-developed, thick (1 to 10 m) deposits that are located in various footwall lithologies from the variably sand-rich Curtis Formation to clay-rich sections of the Morrison Formation (Fig. 4.4-2). The deposits form in the immediate footwall but generally drape over the fault into the hanging wall (Fig. 4.4-3). Additionally, the deposits are confined to sections where the two main fault strands are close together and/or there are pronounced structural complexities such as fault bends and relay ramps (Dockrill, 2005). The northern fault of the Salt Wash Graben contains mainly thinner (0.5 to 4 m) deposits compared to the Little Grand Fault (Fig. 4.4-4). They are located in the sand-rich Entrada Sandstone. The deposits are predominantly confined to the immediate footwall, occasionally draping into the adjacent graben. However, around the Green River fold axis deposits increase in number and form further into the footwall. The easternmost travertine deposits are associated with a breached relay ramp (Dockrill, 2005) (Fig. 4.4-1). In both fault systems the fault gouge is locally well exposed and consists of a zone up to 5m thick of slices of host lithologies separated by clay rich foliated gouge. Where the footwall Upper Jurassic units are juxtaposed against shales in the hanging-wall, the fault core is dominated by low-permeability clay-rich gouge (Dockrill, 2005). Conversely, the surrounding damage zone is dominated by fractures both in the high permeability reservoir units and in the low-permeability seal units (Dockrill and Shipton, 2010). Fracture orientation range and frequency are enhanced in zones of structural complexity improving fracture connectivity and providing pathways for fluids to migrate vertically, parallel to the fault (Dockrill and Shipton, 2010).



**Figure 4.4-1** Distribution of surface travertines along (a) Little Grand Wash Fault and (b) the northern fault of Salt Wash Graben. Also shown is the distribution of iron oxide dissolution and bleaching in the Entrada Sandstone. Insets show the location of each map relative to the Green River, the axis of the Green River Anticline and the two fault systems. Modified after Dockrill (2005).



**Figure 4.4-2** (a-f) Field photographs of ancient travertine mounds from the Little Grand Fault showing distribution of: (a) A layered travertine mound emplaced on partially bleached Mancos Shale. In muddominated lithologies, networks of thin boxwork veins (5 to 10 mm thick) are more common than the thicker white-banded veins, locally destroy the host rock fabrics, and have thin reduction haloes (1 to 5 mm). (b) The faulted and fractured feeder zone to a travertine mound with associated reduction halo in the partially sandy Curtis Formation. (c-f) Horizontal and vertical aragonite veins with diffuse bleaching paralleling the vein trace and following fine fractures radiating from the veins.



**Figure 4.4-3** Field photographs of ancient travertine mounds from the Little Grand Fault showing distribution of (a) A thick mound draping across the fault, dominated by a thick aragonite vein that down turns to the left hand side of the photo, into the fault zone. (b) Large vertical aragonite vein with open cavity feeding travertine (a). (c) Feeder fault cross cutting the Curtis formation (left hand side of (a)) with partial bleaching and extensive bedding parallel calcite cementation, aragonite veining and bleaching (d-e). (f) Close up of the fault zone in (c).



**Figure 4.4-4** Field photographs of a) a travertine mound (Tenmile Butte) collapsing to the south, from the footwall of the northern fault of Salt Wash Graben into the graben itself. (b) Close up of righthand side of photo (a) showing extensive horizontal aragonite veining ~15 m beneath the top of Tenmile Butte which is capped with travertine deposits. (c-e) increasingly close up images of (b) showing aragonite veining and cavity formation within the partially bleached and heavily cemented Entrada Sandstone. Iron is dissolved and locally precipitated on the mm-cm scale as coarse dark Fe-oxides (e). (f) Bedding parallel bleaching and cementation halos in sandy layers surrounding thin bedding parallel aragonite veins, accumulating beneath and between impermeable silty horizons.



4.4.1.1. Ancient Travertine Deposits

**Figure 4.4-5** Figure (from Dockrill, 2005) showing the different stages involved in the formation of a fault related travertine deposit. (a)  $CO_2$ -charged waters migrate up the fault damage zone (DZ) through preexisting fractures. Discharged waters percolate through the surrounding colluvium and flow across the land surface, degassing  $CO_2$  and cementing conglomerate (CG). (b) Sealing of the colluvium initiates layered carbonate (LM) deposits at the surface. Aragonite veins (WBV or BBV) begin to form in the colluvium and host rock beneath the layered deposit. (c-d) Travertine builds up laterally and vertically. Eventually the springs become inactive and the travertine begins to erode.

The morphology and formation of travertine mounds is discussed thoroughly by Dockrill (2005): a brief over view is given here. Travertine mounds essentially comprise (Fig. 4.4-5): a) Calcitecemented colluvium conglomerate which forms the base of the mound. b) A subhorizontal, layered carbonate deposit with moderate to high visible porosity, situated above the conglomerate. The morphology of the layered carbonate varies considerably in texture and packing, but is generally composed of layered, subhorizontal alternating porous and dense horizons. Each layer contains subvertical, dendritic precipitates that branch out from a thin, laminated substrate. The substrate commonly has an irregular, sinuous shape similar to the pooland-rim geometries of microterraces on the present-day travertines. c) Horizontally and vertically orientated banded aragonite veins cross cut the travertine mounds and extend to depth beneath individual deposits.

## 4.4.2. Petrology, Cathodoluminescence, SEM and XRD

### 4.4.2.1. Entrada Sandstone

The aeolian sandstones of the Slick Rock and Earthy members of the Entrada are fine- to medium-grained quartz arenites to subarkose sandstones (Trimble, 1978). These sandstone units alternate with siltstone and silty sandstone of the Dewey Bridge Member at the base of the Entrada Sandstone. The sandstones are red in colour due to the presence of hematite and goethite grain coatings (Beitler *et al.*, 2005, Bowen *et al.*, 2007, Chan *et al.*, 2000, Parry *et al.*, 2004). Regionally, the detrital mineralogy of dune facies sandstones comprises subangular to rounded grains of 76-89 wt% quartz, 8.5-16.5 wt% K-feldspar, 2.2-6.5 wt% plagioclase and trace muscovite (<0.4 wt%), tourmaline, apatite and zircon (<0.5 wt%) (Cullers, 1995; Mirsky and Treves, 1962). All samples vary somewhat in grain size (0.12-0.56 mm), sorting and packing. Type and amount of cement varies considerably and includes quartz, dolomite, calcite, illite, smectite, kaolinite, hematite and goethite.

Point counted samples from SWG average 72.2 vol% quartz grains and 9.8 vol% feldspar grains (both K-feldspar and plagioclase). Quartz grains show occasional quartz overgrowths (0.1 vol%) that exhibit a euhedral outline and occasionally preserve illite and haematitic grain coatings on the original grain rim. Samples average 3.3 vol% illite and 0.2 vol% kaolinite. Two illite textures are present: illite coatings on quartz and K-feldspar grains and pore filling illite, which may replace K-feldspar. Samples average 1.8 vol% illite coating and 1.5 vol% pore filling illite. Samples average 7.6 vol% rhombohedral dolomite and trace (detrital?) calcite (0.1 vol%). Cryptocrystalline hematite averages 1.2 vol% in red dune facies samples and they contain trace detrital oxides (0.1 vol%)



**Figure 4.4-6** Typical crossed polarized light photomicrographs of micro-wafers from thick aragonite veins illustrating the typical pattern of grain morphology and size through an individual growth set. Also prominent in the images are the Fe and Mn rich layers that occur on inception of a new growth surface

## 4.4.2.2. Aragonite Veins

Aragonite and calcite veins parallel bedding or infill open joints and are observed at depths up to  $\sim$ 30m below ancient travertine mounds. Thick aragonite veins are composed of multiple sets of growth surfaces, generally 5 to 30 mm thick, defined by radial and ray crystals elongate perpendicular to the plane of the veins (Fig. 4.4-6). Thin veins are composed of equant and euhedral, occasionally twinned, pseudohexagonal aragonite crystals which grow in open fractures and within the porosity (Fig. 4.4-8). Individual veins grew primarily from the fracture walls inwards (Figs. 4.4-2 to 4.4-4). The carbonate lining the fracture walls are usually equidimensional and occasionally separated by a central cavity. At the inception of a new growth surface aragonite crystals are equant and pigmented containing micro-inclusions of Fe- and Mn-oxides and crystallize with cryptocrystalline hematite and goethite (Fig 4.4-6 & 4.4-7). With distance from the growth surface towards the vein centre crystals increase in size and become elongate, acicular and prismatic. Thick veins thin laterally and terminate in networks of thin veins, occluding lenses of the local host rock, which becomes heavily altered. Fe-oxyhydroxides precipitate on the inner surface of the vein occluding sections of the host rock. Feldspar grains included in these vein segments exhibit evidence of extensive dissolution and reprecipitation of silica, kaolinite and smectite within the pore volume formed by the occluding vein (Figs. 4.4-10 to 4.4.12).



**Figure 4.4-7** XRD patterns from a) coarsely crystalline transparent aragonite and b) from one of the pigmented growth surfaces in Fig. 4.4-6 illustrating the presence of hematite and goethite.



**Figure 4.4-8** Typical plane and crossed polarized light photomicrographs from aragonite micro-veins growing either a) at  $\sim 30$  m below the paleo-land surface or b-e) at the lateral termination of a shallow thick aragonite vein. a) Illustrates the variety of twinned and pseudohexagonal habits of the aragonite crystals which grow in thin micro-veinlets within fractures or the porosity of the local host rock. b-e) Illustrates inclusion of host rock, Fe-mobilization and reprecipitation on the inner surface of the occluding veinlet.



**Figure 4.4-9** Cold cathodoluminescence photomicrographs of thick aragonite veins exhibiting a-c) Inclusion of fragments of host rock grains, at the inception of a new grow surface, around which new crystals or rosettes of crystals nucleate. d) CL image from the coarse portion of a vein showing the generally homogeneous nature of the CL pattern.

Cathodoluminescence patterns for aragonite veins are homogeneous reflecting relatively uniform fluid compositions throughout the precipitation of a single vein (Fig. 4.4-9). Some difference in CL brightness is observed on individual crystal facets reflecting the preferential attachment of ions to surfaces which grow at different rates. Bright yellow-orange (calcite) and blue (K-feldspar) CL patterns observed at the inception of a new growth surface represent grains from the host rock lithology entrained into the vein cavity. These sites comprise amalgams of many small crystals reflecting rapid crystal nucleation due to the density of nucleation sites on the surface of the entrained grains.

Back-scatter electron (BSE) and mono-CL images of micro-aragonite veins (Figs. 4.4-10 to 4.4-11) from the lateral tip of a thick horizontal vein reveals that individual micro-veins are composed of a single, or up to three, growth events and that early growth stages are broken apart and then occluded by later growth stages. Electron intensity increases with proximity to an included portion of host rock reflect dissolution of silicate grains in the matrix and increased incorporation of foreign ions into the aragonite. Increased electron intensity, where no concurrent change in CL intensity is observed reflects an increase in  $Sr^{2+}$ , Na<sup>+</sup> and K<sup>+</sup> content. Later stages of vein growth have higher CL intensities but lower electron intensities reflecting a decreased Fe<sup>2+</sup>,

 $Sr^{2+}$ ,  $Na^+$  and  $K^+$  content. This general pattern reflects a decrease in wall rock interaction in these fine veins as fluid becomes isolated from the host rock by precipitation of aragonite on the fracture surface. EDS patterns and SEM imaging reveal extensive kaolinite veining in these micro-veins where they interact with the host rock, deriving SiO<sub>2</sub> and Al<sup>3+</sup> locally, from the dissolution of silicate minerals.



**Figure 4.4-10** a) BSE and b) Mono-CL photomicrographs of an aragonite micro-veinlet and alteration of occluded portions of the local host rock. EDS spectral for various secondary products including a) smectite surrounding a dissolving K-feldspar grain, b) kaolinite precipitating as fine micro-veins surrounding sand grains and intergrowing with  $CaCO_3$  and c) the aragonite vein.







**Figure 4.4-12** SEM photomicrographs at various scales of a single feldspar grain occluded by an aragonite micro-vein. a) The grain is heavily corroded and is preferentially dissolved along cleavage planes. b-f) The feldspar surface is largely free of secondary mineral coatings. Dissolved components are reprecipitated within the porosity volume created by the dissolved grains as flakes of silica, smectite and micro-platelets of kaolinite on portions of the grain surface and the cavity wall. Clay gains adhering to the aragonite crystal surface inhibit carbonate nucleation, creating pockets of clay occluded in the growing vein.

## 4.4.2.3. Altered Entrada Sandstone

The host rock below individual ancient travertine mounds are generally altered along fractures and bedding planes (Fig. 4.4-4 & 4.4-13). Alteration includes; pervasive calcite, aragonite and

silica cementation, and calcite and aragonite veining. Poikilitic aragonite crystals occur in zones away from fracture conduits. Point counted bleached yellow-orange dune facies samples average 6.5 vol. % feldspar (both K-feldspar and plagioclase), much of which is heavily corroded (Fig. 4.4-12 & 4.4-14), and 65.5 vol. % detrital quartz grains, which are commonly overgrown by euhedral and irregular quartz overgrowths (2.4 vol. %). Overgrowths surround both hematite and illite grain coatings, grains from which the haematitic coatings have been dissolved and commonly include calcite. Grain rimming illite/smectite (1.8 vol. %) and kaolinite (0.5 vol. %) are common and many feldspar grains have 2-10µm coatings of clay intergrowths (Fig. 4.4-14). Samples contain trace, heavily corroded fragments of dolomite (0.2 vol. %) and abundant pore filling calcite (13.7 vol. %) (Fig. 4.4-15 to 4.4-17). Grain rimming, cryptocrystalline hematite and coarse crystalline oxides average 0.4 % and 2.6 %, respectively.



**Figure 4.4-13** Photomicrographs of representative samples of Entrada Sandstone showing a) Unaltered diagenetically red dune facies sandstone from SWG. Dark pigmented layers are zones with thicker (4-6 $\mu$ m) hematitic grain coatings. b) Altered sandstone from a travertine feeder zone at SWG. Cryptocrystalline haematitic grain coatings have been dissolved and the Fe locally reprecipitated as coarse hematite and goethite grains. The pore space is completely occluded by calcite cement. c) Altered Entrada Sandstone from SWG adjacent to an aragonite filled fracture (left hand side of image). Grain coatings have been removed and some Fe has been locally reprecipitated and some mobilized to the fluid. The fracture is in filled with aragonite, kaolinite and smectite. Some fine fracturing in the host rock adjacent to the fracture is observable in the sample due to alteration of the adjacent host rock and the growth of the fracture fill.

Dissolved hematite grain coatings are locally reprecipitated, at the mm-cm scale, as goethite, and occasionally as coarse hematite grains (Fig. 4.4-13). Calcite occurs as granular to blocky, equant to poorly prismatic poor rimming and filling cements. Individual calcite crystals typically contain a pigmented core reflecting a high Fe and Mn content in the crystal and the inclusion of micro-crystalline inclusions of Fe-oxyhydroxides (Fig. 4.4-15). CL patterns for samples close to fracture conduits exhibit a dominant single stage of calcite growth, with no pronounced concretionary zoning and gradational changes in Fe and Mn content from calcite core to rim (Fig. 4.4-16).



**Figure 4.4-14** SEM photomicrographs at various scales of a sand grains in the altered portions of the host rock surrounding an aragonite vein. a) heavily corroded feldspar grains and local reprecipitation of kaolinite and smectite. b) pore-filling kaolinite. c) Dissolving feldspar grain which continues to dissolve even though it is surrounded by a 5 to 10  $\mu$ m thick layer of reprecipitated silica and clay. d-f) close up of secondary products surrounding c).



**Figure 4.4-15** Cold CL photomicrographs of pore occluding calcite (a-f) cement close to a fracture conduit. The calcite fills pore space and is gradationally zoned suggesting continuous precipitation from a fluid of relatively homogenous composition. The cores of most grains are pigmented contain high concentrations of Fe and Mn and micro inclusions of oxyhydroxides, whilst the rims are transparent. Large-scale image of the same sample showing the homogenous nature of the calcite.



**Figure 4.4-16** Typical plane and crossed polarized light photomicrographs from a-d) pore occluding calcite cement close to a fracture conduit in Fig. 4.4-14; e-f) poikilitic aragonite in calcite cemented host rock  $\sim$  3m from the fracture conduit.

Where calcite cementation is associated with joints or open fractures a systematic increase in cement volume is observed with proximity to the conduit. Typically the calcite cementation occludes the majority of the porosity in individual samples.



**Figure 4.4-17** Cold CL photomicrographs of pore filling calcite and poikilitic aragonite in cemented host rock ~3 m from a facture conduit.

Other samples (Fig. 4.4-17), typically forming some distance from fracture conduits or at the edges of calcite cemented halos, around veins, exhibit more complex CL patterns, concretionary and concentric zoning and abundant pokiolitic aragonite cements

## 4.4.3. Carbonate Trace Element Compositions and Paleo-Fluid Chemistry

A single representative sample from each of the two distinct cementation zones; zones containing only calcite cements and zones containing calcite and aragonite cements, were analyzed for major and minor element chemistry (Figs 4.4-18 to 4.4-22).



Figure 4.4-18 Cumulative frequency plot of  $Sr^{2+}$  concentrations in a) calcite only and b) calcite and aragonite cemented host rock.



 $Mg^{2^+}$  Concentration (ppm) Figure 4.4-19 Cumulative frequency plot of  $Mg^{2^+}$  concentrations in a) calcite only and b) calcite and aragonite cemented host rock.



Figure 4.4-20 Cumulative frequency plot of  $Fe^{2+}$  concentrations in a) calcite only and b) calcite and aragonite cemented host rock.



Figure 4.4-21 Cumulative frequency plot of  $Mn^{2+}$  concentrations in a) calcite only and b) calcite and aragonite cemented host rock.



**Figure 4.4-22** Cumulative frequency plot of  $Na^+$  concentrations in a) calcite only and b) calcite and aragonite cemented host rock.

### 4.4.3.1. Calcite Cements

Calcite cements, in samples containing only calcite, contain a gradational zonation in Fe and Mn from core to rim (Figs. 4.4-15, 4.4-16 & 4.4-23). Mg<sup>2+</sup>, Sr<sup>2+</sup>, Na<sup>+</sup> and K<sup>+</sup> concentrations are essentially homogenous (Figs. 4.4-23). Mg contents reflect crystallization at low temperatures: crystallization temperatures calculated from the temperature dependent  $D_{Mg}$  (Oomori *et al.*, 1987) have a mean (~15 °C) close to the average emanation temperature of CO<sub>2</sub>-charged springs in SWG (Fig. 4.4-24). Parent fluid Sr<sup>2+</sup>, Na<sup>+</sup> and K<sup>+</sup> concentrations calculated from the distribution coefficients of Mucci and Morse (1982) and Ishkawa and Ichikumi, (1984) overlap with the Sr<sup>2+</sup>, N<sup>+</sup> and K<sup>+</sup> contents of the modern CO<sub>2</sub> charged fluids at SWG and exhibits similar co-variation of these solutes (Figs. 4.4-25 to 4.4-27). N<sup>+</sup> and K<sup>+</sup> range to higher values in part due to the effects of ion incorporation into intestinal sites (Busenberg and Plummer, 1984). Superposition of calculated parent fluid chemistry and crystallization temperature suggest deposition from a fluid of comparable composition to that of the modern CO<sub>2</sub>-charged fluids at SWG.



**Figure 4.4-23** Tr/Ca of calcites in samples containing only calcite cements showing the variation in cement composition between crystal cores and rims.



**Figure 4.4-24** Cumulative frequency plot of crystallization temperature calculated from the temperature dependent  $D_{Mg}$  expression of Oomori *et al.*, (1987) and using the average Mg/Ca of the modern CO<sub>2</sub>-charged fluids (0.51) at SWG.



Figure 4.4-25 Parent fluid  $Fe^{2+}$  and  $Mn^{2+}$  concentrations calculated using the distribution coefficients of Lorens (1981).


**Figure 4.4-26** Parent fluid Na<sup>+</sup> and K<sup>+</sup> concentrations calculated using the distribution coefficients of Ishkawa and Ichikumi, (1984). The range of Na/Ca and K/Ca observed in calcite cements suggests Na<sup>+</sup> and K<sup>+</sup> concentrations in the paleo-CO<sub>2</sub>-charge fluids that overlap with those of the modern fluid but ranged to higher concentrations. However, both Na and K probably occupy interstitial positions in the calcite structure and their incorporation is thus partly dependent on the number of surface defect sites (see Busenberg and Plummer, 1984) which probably explains the high concentrations observed in some cements.



**Figure 4.4-27** Parent fluid  $Mg^{2+}$  and  $Sr^{2+}$  concentrations calculated using the distribution coefficients of Mucci and Morse (1982).  $Sr^{2+}$  concentrations in the paleo-fluids largely overlap those of the modern fluids.  $Mg^{2+}$  concentrations range to higher values suggesting  $Mg^{2+}$  concentrations in the paleo- $CO_2$ -charged fluids where probably higher, but not significantly so, than those observed in the modern fluids.

#### 4.4.3.2. Calcite Precipitation Rates

Given the similarity in composition of the parent fluid and the modern CO<sub>2</sub>-charged fluids, in-situ distribution coefficients can be derived from measured calcite compositions and the Tr/Ca and activity coefficients of the modern fluid. Using the rate dependent expression for  $D_{Sr}$  (Equation (4.29) derived from experimental studies (section (4.3.5)) the rate of calcite precipitation can then be calculated from the Sr/Ca<sup>cc</sup>. Average calcite precipitation rates calculated for calcite core compositions are 2.1x10<sup>-6</sup> mol/m<sup>2</sup>/s and from rim compositions are 1.3x10<sup>-6</sup> mol/m<sup>2</sup>/s (Fig. 4.4-28). The values approximate a Gaussian distribution and fall within the range of experimentally observed calcite precipitation rates (e.g. Morse, 1987; Mucci and Morse, 1984; Lee and Morse, 1999; Nancollas and Reddy, 1971) (Fig. 4.4-29). Implicit in this model is that fluid Sr/Ca is invariant throughout the precipitation of calcite; this is likely to be a significant simplification. However, uncorrelated Sr and Mg, and the range of values observed, suggest that fluid Mg/Ca and Sr/Ca are not significantly fractionated by calcite precipitation. Varying the calculation through the full range of Sr/Ca<sup>fluid</sup> observed at SWG (0.006 to 0.009, average = 0.007, n = 6) changes the mean rate by only +11 to -17 %. The mean values of Sr/Ca<sup>cc</sup> are probably derived from fluids with Sr/Ca values close to that observed in the modern fluid and mean calculated precipitation rates will reflect this fact. Modern fluid Mn/Ca and Fe/Ca ratios are ~0.001 and  $\sim 0.005$  respectively, values sufficient to suppress calcite precipitation but only by a small degree (e.g. Dromgoole and Walter, 1990b). Paleo-CO<sub>2</sub> charge fluids had up to an order of magnitude higher Fe/Ca ratios (although similar Mn/Ca ratios) than modern CO<sub>2</sub> charged fluids (Fig. 4.4-25) & assuming  $[Ca^{2+}]$  was of the same order of magnitude as the modern fluid). The dependence of precipitation rate on Fe/Ca has not been quantified but if it exhibits a similar magnitudinal relationship as Mn (Dromgoole and Walter, 1990b) this would imply an order of magnitude inhibition of rate. The variation in calculated rate probably reflects a variety of factors including changes in the solution saturation state,  $pCO_2$ , small variations in the Tr/Ca of inhibiting trace ions (mainly Mn and Fe) and nucleation site density and the variation of all these parameters in pores of different sizes and degrees of connectivity.



**Figure 4.4-28** Calcite precipitation rate calculated from  $Sr/Ca^{CC}$  and  $Sr/Ca^{fluid}$  and the  $D_{Sr}$  rate dependence derived from a least square fit to the data of Mucci and Morse (1983) and Mucci (1986). Displayed are the rates for all a) calcite compositions and b) the rates for core and rim compositions. Curves are best fit Gaussian distributions.



**Figure 4.4-29** Laboratory derived calcite precipitation rates as a function of solution saturation state for fluids of various compositions. Data for the variation in rate with:  $pCO_2$  are from Zuddas and Mucci 1993 (25°C, pH 8, [Mg/Ca] = ~5, 1.2 M NaCl); for [Mn/Ca] from Dromgoole and Walter, 1990b (25°C, pH 8, [Mg/Ca] unknown, 0.1 M NaCl,  $pCO_2$  = 100 Pa; and for [Mg/Ca] from House *et al.*, 1988 (25°C, pH 8, 1.0 M NaCl,  $pCO_2$  = ~100 to 1000 Pa).

#### 4.4.3.3. Paleo-fluid Eh-pH

Constrains on paleo-fluid Eh-pH conditions, base on calcite Fe and Mn contents, the distribution coefficients of Lorens (1981) and simultaneous Fe<sub>2</sub>O<sub>3</sub>-MnO<sub>2</sub> equilibria (section 4.3.7) imply Eh-pH conditions comparable to that of the modern CO<sub>2</sub>-charged fluids (Figs. 2.4-25 & 4.4-30) but which range to lower pH. Actual variations in calcite Mn and Fe reflect variation in the Eh-pH conditions of the fluid and variations in precipitation rate (Fig. 4.4-30 & 4.4-31); although the effects of variation in  $D_{Fe}$  and  $D_{Mn}$  due to variations in precipitation rate are relatively small compared to the magnitude of the partitioning (see section 4.3.7). Differences in the Fe and Mn content between cores and rims reflect a progressive increase in pH through the course of precipitation. Any major variation in pH in these fluids is most likely a result of differing degrees of CO<sub>2</sub> saturation modified either by degassing during ascent of the fluids to the surface or as the initial CO<sub>2</sub>-charge in the aquifer dissipates.

Modelling the solubility of hematite as a function of  $pCO_2$ , at different fixed Eh conditions (Fig. 4.4-32), highlights the high solubility of hematite in fluids with high  $pCO_2$  even at relatively oxidizing conditions.



**Figure 4.4-30** Eh-pH diagrams for the system FeSCOH and MnSCOH, calculated using CHNOSZ (Dick, 2008) at 15°C;  $\log(aCO_2) = -1.4$ ,  $\log(aS_{TOT}) = -2.4$ . Black bands are the projected Eh-pH range of parent fluids calculated for calcite core and rim Fe and Mn contents showing upper and lower Eh-pH limits for maximum and minimum Fe and Mn contents observed in each zone.  $D_{Mn} = 7$  and  $D_{Fe} = 3$  were used based on the rate dependent expressions of Dromgoole and Walter (1990a), calculated for the rates derived in section 4.4.3.1. The calculated trajectory for Eh-pH evolution between cores and rims suggests mainly a transition towards higher pH rather than a change in Eh.



**Figure 4.4-31** Measured calcite Fe and Mn contents (grey squares) versus calcite Fe and Mn contents modelled for the modern CO<sub>2</sub> charged fluids at varying precipitation rates using expressions from Dromgoole and Walter (1990a);  $\log(aFe^{2^+}) = -4.5$  and  $\log(aCa^{2^+}) = -2.3$ . Differences in the dependence of  $D_{Mn}$  and  $D_{Fe}$  on precipitation rate produce non-linear correlations in calcite Mn-Fe and most likely explains some of the variation in measured concentrations. The bimodal distribution of Mn concretions may be explained by precipitation from two generations of fluid with varying  $aMn^{2^+}$  but similar  $aFe^{2^+}$  and  $aCa^{2^+}$ .



**Figure 4.4-32** Fluid Fe<sup>2+</sup> concentration in equilibrium with hematite as a function of  $pCO_2$ , up to 100 bar and for different fixed values of Eh, from -120mV to +300mV. A wide range in Fe<sup>2+</sup> concentrations is observed over the full range of  $pCO_2$ , and hematite is relatively soluble at high  $pCO_2$  even at relatively oxidizing conditions. Calculations performed in PHREEQC; 0.1M NaCl solution, hematite equilibrium, fixed Eh using O<sub>2</sub> fugacity, progressive titration of CO<sub>2</sub>

#### 4.4.3.4. Calcite and Aragonite Cements

Fe, Mn, Na, K contents of these calcites (Fig. 4.4-33) are similar to the concentrations in samples containing only calcite but Sr and Mg concentrations range to higher values and exhibit a strong positive correlation. Positively correlated Mg/Ca and Sr/Ca suggest calcite precipitation from a closed fluid reservoir. Thus cation concentrations cannot be accurately used to estimate temperature or precipitation rate due to the highly variable nature of the parent fluid composition. Given the rate independence of Mg-incorporation into calcite, and an insignificant variation in  $D_{Sr}$  with temperature, only variation in the composition of the parent solution can explain correlated Mg/Ca and Sr/Ca. Positively correlated variation in Tr/Ca for multiple cations in calcite (e.g., Mg/Ca, Sr/Ca, Na/Ca), where both  $D_{Tr}$  are either <1, =1 or >1 is indicative of a Rayleigh fractionation process occurring during precipitation. Precipitation from a closed system results in modification of the fluid Tr/Ca due to the non-uniform incorporation of Tr into calcite relative to Ca<sup>2+</sup>.

Rayleigh fractionation as applied to individual trace element behaviour has been discussed thoroughly elsewhere (e.g. Mcintire, 1963). When examining multiple Tr/Ca<sup>2+</sup> systems where the incorporation of one trace component (e.g. Mg<sup>2+</sup>) modifies the degree or rate of incorporation of a second trace component (e.g. Sr<sup>2+</sup>) one must consider a modified form of the Rayleigh relationship where by  $D_{\rm Sr}^{\rm cc}$  varies as a function of Mg/Ca.

The Sr/Ca of calcite  $[(Sr/Ca)^{cc}]$  precipitated at any point during a Rayleigh process from a closed solution of initial Sr/Ca can be calculated from the initial solution composition  $[(Sr/Ca)_o^{fluid}]$  assuming a constant effective partition coefficient  $(D_{Sr}^{cc})$ :

$$\left(\frac{Sr}{Ca}\right)^{cc} = D_{Sr}^{cc} \cdot \left(\frac{Sr}{Ca}\right)_{o}^{fluid} \cdot F^{D_{Sr}^{cc}-1}$$
(4.30)

where the extent of precipitation is defined as:

$$F = \left(\frac{Ca}{Ca_o}\right)_{fluid}$$
(4.31)

Mg/Ca can be described similarly to Eq. (4.30), where Sr/Ca is replaced by Mg/Ca and  $D_{Sr}^{cc}$  by  $D_{Mg}^{cc}$ . Since Mg/Ca and Sr/Ca are linked by the extent of precipitation, *F*, the expressions can be combined, eliminating *F*, yielding a linear log–log relationship:



Figure 4.4-33 Tr/Ca of calcites in samples containing both calcite and aragonite cements.

$$\ln\left[\frac{\left(Sr/Ca\right)^{cc}}{D_{Sr}^{cc} \cdot \left(Sr/Ca\right)_{o}^{fluid}}\right] \left/ D_{Sr}^{cc} - 1 = \ln\left[\frac{\left(Mg/Ca\right)^{cc}}{D_{Mg}^{cc} \cdot \left(Mg/Ca\right)_{o}^{fluid}}\right] \right/ D_{Mg}^{cc} - 1$$
(4.32)

For the incorporation of  $Sr^{2+}$  and  $Mg^{2+}$  into calcite where the  $(Mg/Ca)^{fluid}$  modifies the  $D_{Mg}^{cc}$  and  $D_{Sr}^{cc}$  and the functional relationship (Fig. 4.4-34) can be derived from a least means squared fit to the experimental data of Mucci and Morse (1983) giving:

$$D_{Mg}^{cc} = 0.0275 \cdot \left( Mg / Ca \right)_{fluid}^{-0.3197}$$
(4.33)

and

$$D_{Sr}^{cc} = 0.146 + 1.833 \cdot \chi_{Mg}^{cc} \tag{4.34}$$

where  $\chi_{Mg}^{cc}$  is the mole fraction of Mg in calcite at a given  $(Mg/Ca)_{cc}$ . Combining Eq. (4.32) to (4.34) yields

$$\left(Sr / Ca\right)^{cc} = \exp\left\{ \left[ \ln\left[ \frac{(Mg/Ca)^{cc}}{0.0275 \cdot (Mg/Ca)^{-0.3197}_{fluid}} \cdot (Mg/Ca)^{fluid}_{o} \right] / \left[ \left( 0.0275 \cdot (Mg/Ca)^{-0.3197}_{fluid} \right) - 1 \right] \right] \right\}$$
  
$$\cdot \left[ \left[ \left( 0.146 + 1.833 \cdot \chi^{cc}_{Mg} \right) - 1 \right] \right]$$
  
$$\cdot \left\{ \left[ \left( 0.146 + 1.833 \cdot \chi^{cc}_{Mg} \right) - 1 \right] \right\}$$
  
$$\cdot \left\{ Sr / Ca \right]^{fluid}_{o} \right\}$$
(4.35)

Under the conditions of closed system precipitation with constant partition coefficients and any initial fluid composition, trace–trace behaviour is predicted to follow Eq. (4.32) In Eq. (4.32) the slope of the log–log relationship is determined by the partition coefficients of each Tr and the intercept is influenced by both the initial solution composition and the partition coefficients. The slope in Eq. (4.32) is relatively less sensitive to variations in  $D_{Mg}^{cc}$  than  $D_{Sr}^{cc}$ , since  $D_{Mg}^{cc}$  is <<  $D_{Sr}^{cc}$ .

First we can consider the simple model of constant  $D_{Mg}^{cc}$  and  $D_{Sr}^{cc}$ . We can calculate a value for  $D_{Mg}^{cc}$  and  $D_{Sr}^{cc}$  from the composition of the calcites precipitated from the unfractionated reservoir, and the modern fluid ( $D_{Mg}^{cc} = 0.0131$  close to the value of 0.0154 predicted from the temperature dependence of Mg incorporation into calcite (Oomori *et al.*, 1987) and  $D_{Sr}^{cc} = 0.23$ ).



**Figure 4.4-34 a)** Variation in  $D_{Mg}^{cc}$  as a function of  $(Mg/Ca)^{fluid}$  (Mucci and Morse, 1983). **b**) Mg/Ca and Sr/Ca covariation in samples containing calcite and aragonite cements. Curves are the Rayleigh fractionation models previously described. Model 1) Constant  $D_{Mg}^{cc}$  and  $D_{Sr}^{cc}$ . Model 2) Variation in the fluid Mg/Ca as a result of fraction of the fluid composition due to calcite precipitation modifies  $D_{Mg}^{cc}$  and  $D_{Sr}^{cc}$  resulting in a non-linear relationship which best describes the measured data. Error bars are  $2\sigma$  uncertainties in the deviation of repeat analysis of points.

We can also consider a second model describing the Sr/Ca of calcite precipitating from a closed system where the fluid composition is undergoing a Rayleigh type fractionation and the resulting modification of  $(Mg/Ca)_{fluid}$  results in a progressive modification of  $D_{Mg}^{cc}$  and  $D_{Sr}^{cc}$ . Fitting these two models to the measured data (Fig. 4.4-34) suggests the functional form of the variation in Mg/Ca and Sr/Ca is best described by the second model, consistent with the experimental prediction that the incorporation of Mg<sup>2+</sup> into the calcite lattice is dependent on the Mg/Ca of the parent solution and that the  $X_{Mg}$  in calcite exerts a control on the incorporation of Sr<sup>2+</sup> as discussed. Further this suggest that closed system fraction of the solution composition results in elevated  $(Mg/Ca)_{fluid}$  and Mg<sup>2+</sup>.

It has been well established that the presence of dissolved Mg<sup>2+</sup> favours the precipitation of  $CaCO_3$  as aragonite, rather than the more stable calcite, from magnesium-rich aqueous solutions (Lippmann, 1973). Also, other studies (e.g. Taft, 1967; Bischoff and Fyfe, 1968) indicate that Mg<sup>2+</sup> inhibits the low temperature transformation, via dissolution-reprecipitation, of aragonite to calcite. A commonly accepted explanation of these observations is that Mg<sup>2+</sup> inhibits calcite nucleation and/or crystal growth, and, as a result aragonite, which precipitates more rapidly, is kinetically 'stabilized' (Bischoff, 1968). Dissolved Mg is not readily absorbed on to the surface of aragonite, nor is Mg<sup>2+</sup> taken up to any extent into the aragonite crystal lattice. As a result aragonite crystal growth is relatively unaffected by the presence of dissolved Mg<sup>2+</sup>. By contrast Mg<sup>2+</sup> is readily absorbed on to the surface of calcite and incorporated into its crystal structure. Most of the Mg inhibition is believed to be due to the non-equilibrium incorporation of Mg into growing calcite crystals, which causes them to be considerably more soluble than pure calcite (e.g. Mcintire, 1963). Also, the presence of Mg<sup>2+</sup> ions in solution inhibits nucleation kinetics of calcite as hydrated magnesium is adsorbed onto the surfaces of the pre-critical nuclei of the calcite (i.e., crystallites that are too small to be stable in solution and quickly dissolve) and poisons the active growth sites (Fernández-Díaz et al., 1996).

The findings of Fernández-Díaz *et al.*, (1996) and Given and Wilkinson (1985) suggest that carbonate mineralogy and morphology are not controlled by a single parameter but by interplay between super-saturation and solution Mg/Ca ratios. These findings are further supported by the fact that aragonite can be precipitated from low-Mg<sup>2+</sup> solutions at very high super-saturations (González and Lohmann 1988), indicating that  $CO_3^{2-}$ -controlled kinetics also play a major role in aragonite precipitation in fluids with low Mg/Ca, such as dilute surface and ground waters.

Thus the presence of pokiolitic aragonite cements growing with calcite can be attributed to the modification of  $(Mg/Ca)^{fluid}$  through closed system fractionation of the parent fluid resulting in elevated Mg/Ca ratios suitable for the inhibition of calcite precipitation and the kinetic stabilization of aragonite. The additional role of  $CO_3^{2-}$  and thus  $\Omega_{cc}$  is difficult to asses in

this situation. Significant modification of the  $\Omega$  of carbonate minerals in this setting is probably best achieved by H+ consumption by CO<sub>2</sub> degassing following the conversion of CO<sub>2</sub> (aq)  $\rightarrow$  CO<sub>2</sub> (g).

#### 4.4.4. Stable Isotope Geochemistry

Twenty samples of bleached and altered Entrada Sandstone and twenty samples of aragonite veins, from travertine feeder systems, where collected from Salt Wash Graben. Table B-VI and B-VII (Appendix B) displays the  $\delta^{13}$ C and  $\delta^{18}$ O of samples of carbonate cemented Entrada Sandstone associated with travertine mounds, aragonite veins and modern travertine samples obtained in this study. These samples were supplemented with 16 chips of U-Th dated aragonite veins from travertine feeder systems (Burnside, 2009) from both LGF and SWG (Table B-IX, Appendix B). U-Th dated samples where obtained from the thickest portions of homogeneous veins in order to limit the effects of wall rock interaction. This data is presented in figure (4.4-35) together with data from Dockrill (2005) for aragonite veins, ancient travertine deposits and travertine samples from the actively forming mound at Crystal Geyser.



Figure 4.4-35 Stable Isotope analyses for carbonate deposits associated with the modern  $CO_2$  systems from this study and from Dockrill (2005).

#### 4.4.5. Modern Travertine Deposits

Modern travertine deposits exhibit extreme enrichment in <sup>13</sup>C with values of  $\delta^{13}C_{CaCO3}$  ranging from 5.2 to 11.3 % V-PDB (Fig. 4.4-36). This ~6 % variation is attributed to CO<sub>2</sub> degassing and carbonate precipitation driven <sup>13</sup>C enrichment in the out-gassing fluid. Positively correlated  $\delta^{13}C$ and  $\delta^{18}O$  is attributed to kinetic isotope effects during the degassing processes (see section 4.4.6). The range in  $\delta^{18}O_{CaCO3}$  of these modern deposits is largely attributed to kinetic degassing effects (but see section 4.4.7). The least fractionated values of  $\delta^{18}O_{CaCO3}$  are consistent with the  $\delta^{18}O_{HCO3}$ . beginning controlled by equilibration with  $\delta^{18}O_{H2O}$  of modern CO<sub>2</sub>-charged waters. The fraction models suggest that the modern fluid undergoes ~20% degassing before the initiation of calcite precipitation (Figs. 4.4-36 & 4.4-40).



**Figure 4.4-36** The  $\delta^{18}$ O (PVB) and  $\delta^{13}$ C (PVB) of HCO<sub>3</sub><sup>-</sup> calculated from the isotopic composition of modern travertine samples from springs in Salt Wash Graben and from samples of travertine from Crystal Geyser (Dockrill, 2005) using appropriate equilibrium fractionation factors calculated for the emanation temperature of each spring. Also plotted is the  $\delta^{18}$ O and  $\delta^{13}$ C of HCO<sub>3</sub><sup>-</sup> in modern CO<sub>2</sub>-charged fluids calculated from the measured  $\delta^{18}O_{H2O}$  and  $\delta^{13}C_{CO2(g)}$ . Lines are Rayleigh distillation models of kinetic fraction of the average HCO<sub>3</sub><sup>-</sup> of modern fluid resulting from for CO<sub>2</sub> degassing only, and coupled CO<sub>2</sub> degassing and calcite precipitation (see section 4.5.2 for a complete discussion). Error bars are the  $2\sigma$  of analytical uncertainty.

#### 4.4.6. CO<sub>2</sub> Degassing, Carbonate Precipitation and Kinetic Isotope Fractionation

Carbonate precipitation in shallow subsurface and surface systems will be driven by changes in  $pCO_2$  resulting from changes in ambient pressure. As CO<sub>2</sub>-charged fluids ascend through the shallow subsurface the water will move toward chemical equilibrium with its new environment by degassing CO<sub>2</sub>, dissolved as CO<sub>2</sub>(aq). During this first stage of out gassing of CO<sub>2</sub>(aq) from the solution the concentrations of Ca<sup>2+</sup> and HCO<sub>3</sub><sup>-</sup> will stay constant (Dulinski and Rozanski, 1990). The equilibrium concentrations of HCO<sub>3</sub><sup>-</sup> and Ca<sup>2+</sup> with respect to CaCO<sub>3</sub> are determined by the initial  $pCO_2$  at depth and consequently the fluid becomes quickly supersaturated with respect to CaCO<sub>3</sub> as  $pCO_2$  decreases. After the first stage of out gassing of CO<sub>2</sub>, carbonate precipitation starts, the stoichiometry of the overall reaction;

$$2HCO_3^- + Ca^{2+} \leftrightarrow CaCO_3 + CO_2 + H_2O \tag{4.36}$$

requires that for each CaCO<sub>3</sub> molecule deposited one CO<sub>2</sub> molecule is created. In fluids with high DIC the rate of CaCO<sub>3</sub> precipitation will ultimately be governed by the state of CaCO<sub>3</sub> saturation which will be a direct function of the amount of degassing experience by the fluid. The rate of CaCO<sub>3</sub> precipitation is therefore dependent on the CO<sub>2</sub> degassing rate of the solution.



**Figure 4.4-37** Evolution of the isotopic composition of the reactant DIC pool during the kinetic fractionation of  $\delta^{18}$ O and  $\delta^{13}$ C (from an initial  $\delta^{18}$ O and  $\delta^{13}$ C of both 0%) during different mechanism of DIC loss from an open and closed fluid reservoir. Only CO<sub>2</sub> degassing from an HCO<sub>3</sub><sup>-</sup> reservoir and coupled CO<sub>2</sub> degassing and CaCO<sub>3</sub> precipitation can lead to positively correlated  $\delta^{18}$ O and  $\delta^{13}$ C. Open system behaviour leads to large fractionations in the reacting DIC pool.



**Figure 4.4-38** Evolution of the  $\delta^{13}$ C of the reactant DIC pool as a function of various degrees of C loss during the kinetic fractionation of  $\delta^{13}$ C (from an initial  $\delta^{13}$ C of 0 %) under different mechanism of DIC loss from an open (exponential functions) and closed (linear functions) fluid reservoir.

As calcium carbonate precipitation and  $CO_2$  degassing, progresses, the  $HCO_3^-$  reservoir in the fluid will undergo <sup>13</sup>C enrichment (Fig. 4.4-37 & Fig. 4.4-38) if C isotope exchange reactions between DIC and CO<sub>2</sub>(g) are sufficiently slow and/or fluid/gas velocities is small. This <sup>13</sup>C enrichment results from the relatively low  $\delta^{13}$ C value of the CO<sub>2</sub> that is lost from the fluid by degassing. The extent of <sup>13</sup>C enrichment is a function of the fractionation factors between the C species and the fraction of total DIC lost to CO<sub>2</sub> degassing and CaCO<sub>3</sub> precipitation. Only relatively slow hydration-dehydration reactions permit oxygen isotope exchange between  $CO_2(aq)$  and  $H_2O_2$ , so if the precipitation of calcium carbonate proceeds rapidly, there may be progressive <sup>18</sup>O enrichment in the HCO<sub>3</sub><sup>-</sup> and in the  $CO_3^{2-}$  that is ultimately incorporated into the calcium carbonate. Both batch (closed) and Rayleigh distillation (open) models can be used to describe the covariation in  $\delta^{13}$ C and  $\delta^{18}$ O of the precipitated CaCO<sub>3</sub> during CO<sub>2</sub> degassing and CaCO<sub>3</sub> precipitation from a fluid. Batch and Rayleigh distillation can be used to model the C and O isotope evolution of precipitating calcium carbonate because if C and O isotopes are fractionated during calcium carbonate precipitation, there must be an effect on the isotope composition of the remaining reactant. It is assumed that an instantaneous isotopic equilibrium fraction occurred among the degassed  $CO_2$ , remaining  $HCO_3^-$  and precipitated CaCO<sub>3</sub>. During rapid mineral precipitation it is not uncommon for isotopic disequilibrium to occur (e.g. Fantidis and Ehhalt, 1970; Hendy, 1971). However, equilibrium fractionation factors are used as a best first approximation because they are known, whereas any deviation from isotopic equilibrium is unknown.

An estimation of the maximum <sup>13</sup>C enrichment in the HCO<sub>3</sub><sup>-</sup> reservoir owing to CO<sub>2</sub> degassing and CaCO<sub>3</sub> precipitation was made, using an open system Rayleigh distillation model, and published isotope fractionation factors. The effects of Rayleigh distillation on the  $\delta^{13}$ C value of the DIC reservoir can be modelled by:

$$(\delta + 1000) / (\delta_o + 1000) = f^{(\alpha_{p-r} - 1)}$$
(4.37)

where  $\delta$  is the C isotope composition of HCO<sub>3</sub><sup>-</sup>,  $\delta_0$  is the initial C isotope composition of HCO<sub>3</sub><sup>-</sup>, *f* is the fraction of HCO<sub>3</sub><sup>-</sup> remaining at a given point in the fluids evolution, and  $\alpha_{p-r}$  is the equilibrium carbon isotope fractionation factor between a bulk product and the HCO<sub>3</sub><sup>-</sup> reactant. Because the C in HCO<sub>3</sub><sup>-</sup> is evenly partitioned between CaCO<sub>3</sub> and CO<sub>2</sub> (g) during CaCO<sub>3</sub> precipitation, a fractionation factor between a bulk product and HCO<sub>3</sub><sup>-</sup> can be defined such that

$$\alpha_{(bulk\_product-HCO_3^-)} = \frac{1}{2} \left( \alpha_{CO_2 - HCO_3^-} \right) + \frac{1}{2} \left( \alpha_{calcite-HCO_3^-} \right)$$
(4.38)

Using fractionation factors for  $\alpha_{CO2-HCO3}$  and  $\alpha_{calcite-HCO3}$  of 0.9922 and 1.0010, respectively (Romanek *et al.*, 1992; Zhang *et al.*, 1995), the  $\alpha_{(bulk product-HCO3)}$  is 0.9966 at 15 °C. The oxygen isotope effects of CO<sub>2</sub> degassing, CaCO<sub>3</sub> precipitation, and H<sub>2</sub>O formation, can be modelled using an analogous Rayleigh distillation approach with the following assumptions: There is no oxygen isotope exchange between DIC and water, and the fractionation factor between the bulk product and HCO<sub>3</sub><sup>-</sup> is

$$\alpha_{(bulk\_product-HCO_3^-)} = 2/6 \left( \alpha_{CO_2 - HCO_3^-} \right) + 3/6 \left( \alpha_{calcite-HCO_3^-} \right) + 1/6 \left( \alpha_{H_2O - HCO_3^-} \right)$$
(4.39)

or in proportion to the oxygen in each of the three products. Using fractionation factors for  $\alpha_{CO2-HCO3}$ ,  $\alpha_{calcite-HCO3}$  and  $\alpha_{H2O-HCO3}$  of 1.0062, 0.9939, and 0.9667, respectively,  $\alpha_{(bulk product-HCO3)}$  is 0.9935 at 15 °C (Brenninkmeijer *et al.*, 1983; Kim and O'Neil, 1997; Usdowski and Hoefs, 1993).



**Figure 4.4-39** Changes in the  $\delta^{18}$ O and  $\delta^{13}$ C of HCO<sub>3</sub><sup>-</sup> as a result of progressive loss of HCO<sub>3</sub><sup>-</sup> during CO<sub>2</sub> degassing and CaCO<sub>3</sub> precipitation with different isotope effects. The  $\delta^{18}$ O of HCO<sub>3</sub><sup>-</sup> can either be maintained at a constant value by equilibration between DIC and H<sub>2</sub>O through equations (4.41) and (4.42). In the absence of any oxygen exchange  $\delta^{18}O_{HCO3}$  will evolve, as HCO<sub>3</sub><sup>-</sup> is removed from solution, according to the equilibrium fractionation between dissolved species, out gassing CO<sub>2</sub> and precipitating CaCO<sub>3</sub>. An intermediate situation is also possible. (Redrawn after Mickler *et al.*, 2006).

Similarly, the effects of batch degassing on the isotopic composition of the fluid can be expressed as (after Valley, 1986):

$$\delta = \delta_o - (1 - f) \cdot 1000 \cdot \ln \alpha_{p-r} \tag{4.40}$$

where the notations are as previously described. If crystallization of CaCO<sub>3</sub> is sufficiently rapid,  $HCO_3^-$  enriched in <sup>18</sup>O will be incorporated into CaCO<sub>3</sub> before <sup>18</sup>O re-equilibration occurs between  $HCO_3^-$  and the bulk water. This approach is an end-member calculation because it neglects CO<sub>2</sub> hydration and hydroxylation reactions (equations 4.41 and 4.42), which will buffer the oxygen isotopic composition of the  $HCO_3^-$  reservoir and reduce the magnitude of the oxygen isotope effects of CO<sub>2</sub> degassing. The relatively slow forward and backward reactions outlined in equations (4.41) and (4.42) will result in the  $HCO_3^-$  acquiring a  $\delta^{18}$ O value closer to equilibrium with the large reservoir of oxygen in H<sub>2</sub>O (Hendy, 1971). Note that in the pH range of interest, reaction (4.41) is dominant.

CO<sub>2</sub> hydration-dehydration

$$CO_2 + H_2O \leftrightarrow H_2CO_3 \leftrightarrow HCO_3^-(aq) + H^+$$

$$(4.41)$$

and

CO<sub>2</sub> hydroxylation

$$CO_2 + OH^- \leftrightarrow HCO_3^-(aq)$$
 (4.42)

This model of progressive loss of  $HCO_3^-$  during calcium carbonate precipitation, while excluding oxygen isotope exchange between DIC and H<sub>2</sub>O, will cause progressive <sup>18</sup>O and <sup>13</sup>C enrichment in the  $HCO_3^-$  reservoir, as shown in figures (4.4-37) to (4.4-39). Kinetic fractionation of  $HCO_3^-$  (aq) implies rapid rates of  $CO_2$  degassing and carbonate precipitation, faster than the  $HCO_3^-H_2O$  equilibration reaction which operates on the 1000's to 10000's sec time-scale (Hendy, 1971).

#### 4.4.7. Ancient Travertine Deposits

 $δ^{13}C_{CaCO3}$  of ancient travertine deposits (Dockrill, 2005) range from 2.5 to 6.5 %*c*, the variation being attributed to fractionation during CO<sub>2</sub> degassing. Minimum  $δ^{13}C_{CaCO3}$  values 1%*c* lower than modern travertine deposits suggest deposition from an isotopically lighter, less degassed reservoir of carbon. This suggests the  $δ^{13}C$  of the DIC reservoir has evolved through time and was lighter during earlier periods of CO<sub>2</sub> leakage Ancient travertines from Little Grand Fault (Dockrill, 2005) exhibit trends consistent with kinetic fractionation of the HCO<sub>3</sub><sup>-</sup> reservoir. The lack of a positive correlation in  $δ^{13}C$  and  $δ^{18}O$  in Salt Wash Graben samples (Dockrill, 2005) may reflect under representation of the sample population or that these fluids were sufficiently degassed at the time of travertine deposition to suppress kinetic effects. The wide variation in  $δ^{18}O_{CaCO3}$  (Fig. 4.4-40) ( $δ^{18}O$  SWG: 18.6 to 25.1 %*c*;  $δ^{18}O$  LGWF: 17.3 to 21.7 %*c*) and values that range to compositions significantly heavier than the modern travertine deposits is attributed to larger concentrations of Paradox Formation brine in the groundwaters during past periods of leakage. Differences in the range of  $δ^{18}O$  observed between each fault system reflect differences in the maximum flux of brine in each fault system.



**Figure 4.4-40** The  $\delta^{18}$ O and  $\delta^{13}$ C of HCO<sub>3</sub><sup>-</sup> calculated from the isotopic composition of modern travertine samples and from ancient travertine samples from Little Grand Fault (a) and Salt Wash Graben (b). The composition of Crystal Geyser fluid and springs from SWG are shown. Lines are Rayleigh distillation models as in Fig. 4.4-36. The fraction models suggest that the modern fluid undergoes ~20% degassing before the initiation of calcite precipitation. Only the ancient travertines from LGF exhibit a correlation consistent with kinetic fractionation of the HCO<sub>3</sub><sup>-</sup> reservoir. The wide range in  $\delta^{18}$ O of the SWG samples is interpreted to reflect a wide variation in the range of brine fractions in the source fluid. In both instances the lowest  $\delta^{13}$ C of HCO<sub>3</sub><sup>-</sup> in the ancient travertine samples is between 1 to 1.5 % lower than the modern samples which is interpreted to reflect progressive fraction of the initial  $\delta^{13}$ C of the subsurface CO<sub>2</sub> reservoir through the life of the leaking site. This is most likely due to fraction of the  $\delta^{13}C_{CO2}$  due to in-situ degassing.

#### 4.4.8. Aragonite Veins

The wide range of  $\delta^{18}$ O observed in aragonite veins and modern travertine samples is indicative of variation in the  $\delta^{18}$ O composition of the parent fluid as a result of both mixing of meteoric and brine fluid sources and modification by kinetic fraction of the solution HCO<sub>3</sub><sup>-</sup> pool during CO<sub>2</sub> degassing and CaCO<sub>3</sub> deposition. Positive correlated  $\delta^{18}O_{CaCO3}$  and  $\delta^{13}C_{CaCO3}$  is a general indication that kinetic affects may be influencing isotopic fractionation during the precipitation of calcium carbonate, although other physical variables may also result in this correlation (e.g. fluid temperature, surface evaporation-condensation processes or progressive dissolution of a precursor carbonate phase and subsequent enrichment in <sup>13</sup>C and <sup>18</sup>O).

The range of  $\delta^{18}$ O observed in aragonite and modern travertine samples exceeds that expected for likely temperature variations in shallow subsurface and surface environments. The 4 to 5 % variation in  $\delta^{18}$ O observed in aragonite veins would be equivalent to an ~20 to 25 °C variation in precipitation temperature. The slope of the trend in  $\delta^{18}$ O versus  $\delta^{13}$ C resulting from variation in precipitation temperature is significantly lower than the observed correlations. Aragonite deposition occurs at shallow subsurface to near surface depths and so evaporationcondensation processes are unlikely. Given that the stabilization of aragonite at low temperatures requires high  $[CO_3^{2-}]$  and high levels of supersaturation, non-equilibrium fractionation is to be expected during its deposition.



**Figure 4.4-41** The  $\delta^{18}$ O and  $\delta^{13}$ C of HCO<sub>3</sub><sup>-</sup> calculated from the isotopic composition of aragonite veins and ancient travertines from (a) LGF and (b) SWG (Dockrill, 2005). Dated aragonite samples (this study) are also shown and encompass the general trend of all samples in both fault systems. Both data sets do not fit a kinetic degassing model from an initial fluid of the same composition as the modern CO<sub>2</sub>-charged waters (compare to Fig 4.4-40) suggesting derivation from a fluid with lower initial  $\delta^{13}C_{HCO3}$ . and heavier  $\delta^{18}O_{H2O}$ . Both fault systems exhibit variation in  $\delta^{18}O$  attributed to variation in the brine additions. This is especially noticeable in SWG where clusters of compositions reflect distinct leakage events with progressively younger events having lighter  $\delta^{18}O$  as the brine additions decline (see section 4.5-7). A corresponding decline in the average  $\delta^{13}C$  of each cluster is attributed to the  $\delta^{13}C_{CO2(g)}$  becoming increasingly heavy due to fractionation of the in-situ composition by exsolution of CO<sub>2</sub> in the subsurface. Within individual populations linear correlations in  $\delta^{18}O$  and  $\delta^{13}C$  are attributed to kinetic fraction of the HCO<sub>3</sub><sup>-</sup> pool. Travertines from LGF have compositions close to or lighter than their corresponding aragonite veins which is attributed to rapid ascent of the fluid with limited CO<sub>2</sub> degassing in the subsurface. Travertines from SWG are always lighter than their corresponding aragonite veins, attributed to extensive CO<sub>2</sub> degassing in the subsurface prior to effusion of fluid at the surface.

#### 4.4.9. Altered Host Rock

Variation in the  $\delta^{13}$ C of altered and calcite cemented Entrada Sandstone samples in travertine feeder systems is interpreted as reflecting degassing driven <sup>12</sup>C depletion from an initial HCO<sub>3</sub><sup>-</sup> reservoir of ~ -0.7 %<sub>o</sub>. The variation in  $\delta^{18}$ O of all samples is attributed to both differences in the proportions of fluid end-members and kinetic fractionation. The trends suggest that the initial  $\delta^{13}C_{HCO3-}$  of the CO<sub>2</sub>-charged fluids may have been ~2 %<sub>o</sub> lower than that observed in the modern system.



**Figure 4.4-42** The  $\delta^{18}$ O and  $\delta^{13}$ C of HCO<sub>3</sub><sup>-</sup> as above but including the values for altered Entrada Sandstone from SWG.

#### 4.4.10. Implications for modern and ancient travertine formation

The presence of large kinetic isotope effects during precipitation of aragonite veins in travertine feeder systems suggests substantial CO<sub>2</sub> degassing from the ascending fluid, in the shallow subsurface, increasing  $\Omega_{cc}$ , enforcing very rapid rates of CaCO<sub>3</sub> precipitation, sufficient to suppress equilibration of HCO<sub>3</sub><sup>-</sup> and H<sub>2</sub>O in solution.

The absence of a positive correlation in <sup>18</sup>O versus <sup>13</sup>C in ancient travertine samples from Salt Wash Graben is interpreted to reflect the slow equilibrium degassing of CO<sub>2</sub>-charged fluids as they escape from the fault zone, having undergone extensive  $CO_2$  degassing in the shallow subsurface.



**Figure 4.4-43** (a-d): Deformation and alteration beneath travertine mounds from Salt Wash Graben. The degassing of  $CO_2$  in the shallow subsurface results in free gas accumulation and cavity formation inducing buoyant uplift of the surrounding rock volume and associated deformation. Cavity formation induces folding of the Entrada Sandstone which is in part accommodated by the formation of conjugate reverse fault sets. This active deformation will be important for the formation and maintenance of leakage pathways at shallow depth.

Conversely, positively correlated  $\delta^{13}$ C and  $\delta^{18}$ O of modern travertines, and ancient travertines from Little Grand Fault, are interpreted to reflect rapid CO<sub>2</sub> degassing and calcite precipitation as the effused fluid flows over the land surface. It is inferred that some largely undegassed fluid was able to escape to the surface at LGF imply rapid fluid velocities and leakage rates.

This is consistent with the observed morphologies of travertine deposits in each fault setting: individual travertines of LGF are up to 10 m thick, drape over fault scarps and local topographic features and are of relatively narrow lateral extent having degassed rapidly at the surface, depositing carbonate rapidly; travertines from SWG are much thinner (up to 4m), but of larger lateral extent having degassed slowly at the surface. Additionally, altered Entrada Sandstone beneath travertine mounds in SWG shows extensive deformation, faulting and folding attributed to accumulation of pockets of  $CO_2(g)$  in the subsurface and buoyant uplift of the surrounding rock volume (Fig. 4.4-43), a feature largely absent in LGF. Differences in the styles of leakage are interpreted to be a result of a) differences in the fault architecture; b) differences in the depth of the leaking reservoir; c) differences in the local hydrology d) differences in the hydraulic conductivities of the shallow lithologies. This is discussed further in section 4.5.8.

#### 4.4.11. Reconstructing the CO<sub>2</sub> Leakage History

Variation in the  $\delta^{18}$ O,  $\delta^{13}$ C and  ${}^{87}$ Sr/ ${}^{86}$ Sr of U-series dated aragonite veins (Burnside, 2009) from Salt Wash Graben and Little Grand Fault record a history of CO<sub>2</sub> injection, migration, degassing and CO<sub>2</sub> promoted fluid-mineral reactions within the Navajo Aquifer. Both fault systems exhibit the same style of covariance in isotopic systems, although the timing and magnitude of events differ between the two.

#### 4.4.11.1. Salt Wash Graben

The Navajo Aquifer was charged with  $CO_2$  at some point prior to 413 ka and was later recharged with a second major pulse of  $CO_2$  at ca. 135 ka. Enrichment in the  $\delta^{13}C$  of aragonite of 1.13 % between 413 ka and 219 ka, and 1.23 % between 135 ka and 60 ka is interpreted to reflect  $CO_2$  leakage and kinetic fraction of the fluid  $HCO_3^-$  reservoir via coupled CaCO<sub>3</sub> precipitation-CO<sub>2</sub> degassing.



Spring); and LGF) The lowest measured values of  ${}^{13}$ C and  $\delta^{18}$ O travertine samples from Crystal Geyser of Dockrill (2005) and for: SWG) for the lowest measured  $\delta^{13}$ C and  $\delta^{18}$ O travertine from SWG and its equivalent spring  ${}^{87}$ Sr/ ${}^{86}$ Sr (Big Bubbling uncertainties. Uncertainties for <sup>87</sup>Sr/<sup>86</sup>Sr and most ages are smaller than the symbols used. Green symbols are the modern values lies 3.4 km further along the fault trace, in the direction of groundwater flow. Uncertainties are the  $2\sigma$  of analytical to the intersection of the apex of the Green River and the northern fault of SWG, with the exception of the star symbol which Th ages (Burnside, 2009). Travertine volumes are calculated from the maps of Dockrill, (2005). For SWG all samples are close the Crystal Geyser fluid <sup>87</sup>Sr/<sup>86</sup>Sr. Travertine volumes are estimated from the maps of Burnside, (2007).



**Figure 4.4-45** The change in  $\delta^{13}$ C and  $\delta^{18}$ O of aragonite with time, during periods of kinetic fractionation, for both LGF and SWG. The near identical slopes of  $d\delta^{13}$ C/dt and  $d\delta^{18}$ O/dt highlights that the same mechanism is modifying both isotopic systems.

Suppression of the  $\delta^{13}$ C and  $\delta^{18}$ O of aragonite between these two periods of degassing reflects introduction of a fresh unfractionated CO<sub>2</sub> charge at ca. 135ka, sufficient to suppress the  $\delta^{18}$ O composition of the HCO<sub>3</sub><sup>-</sup>. The enrichment in both  $\delta^{13}$ C and  $\delta^{18}$ O from 135 ka to 60 ka reflects rapid leakage and kinetic fractionation of  $HCO_3^{-1}(aq)$ , which implies rapid rates of  $CO_2$  degassing and carbonate precipitation, faster than the  $HCO_3$ -H<sub>2</sub>O equilibration reaction which operates on the 1000's to 10000's sec time-scale (Hendy, 1971). Travertine mounds show a maximum volume at 135ka and the volume of travertine mounds decreases exponentially from 135ka to 60ka. The covariation of travertine volume and linearly increasing  $\delta^{13}$ C and  $\delta^{18}$ O, and the initiation of an increase in <sup>87</sup>Sr/<sup>86</sup>Sr are interpreted to reflect introduction of a new CO<sub>2</sub> charge at 135ka which saturated the reservoir fluid and produced a free gas phase. This CO<sub>2</sub>-charge then degassed rapidly from 135ka to a state of under-saturation at 65ka. The linear covariation in  $\delta^{13}$ C and  $\delta^{18}$ O over these periods, and the similarity of  $d\delta^{13}$ C/dt and  $d\delta^{18}$ O/dt in each fault system reflects kinetic fraction of the HCO<sub>3</sub><sup>-</sup> reservoir due to rapid rates of CaCO<sub>3</sub> precipitation as a result of a large degree of CaCO<sub>3</sub> oversaturation in the fluid caused by rapid rates of CO<sub>2</sub>degassing. This state of oversaturation is due to: a) rapid  $CO_2$  degassing in the subsurface and; b) higher concentrations of  $Ca^{2+}$  and  $HCO_3^{-}$  in the ascending fluid following a CO<sub>2</sub>-charge as the fluid moves towards equilibrium with respect to carbonate by dissolving dolomite in the reservoir under conditions of elevated  $pCO_2$ . High  $pCO_2$ , and consequently elevated Ca<sup>2+</sup> and HCO<sub>2</sub>, will lower the depth at which over-saturation with respect to CaCO<sub>3</sub> is reached in the ascending fluid, promoting rapid rates of  $CaCO_3$  deposition. As  $pCO_2$  in the reservoir falls the point at which CaCO<sub>3</sub> super-saturation in the ascending fluid is reached will move closer to the surface and subsurface CaCO<sub>3</sub> deposition rates will decline, inhibiting kinetic fractionation of the HCO<sub>3</sub><sup>-</sup> pool. A cessation in covarying  $d\delta^{13}$ C/dt and  $d\delta^{18}$ O/dt following these periods reflects a decline in the rate of CaCO<sub>3</sub> deposition due to a reduction in the CO<sub>2</sub> degassing rate and in-situ pCO<sub>2</sub>, and consequently a lowering of fluid Ca<sup>2+</sup> and HCO<sub>3</sub><sup>-</sup> and  $\Omega_{cc}$  at shallow depths. This reflects the depletion of the free gas phase and a return to CO<sub>2</sub> under saturated conditions.

 $\delta^{18}$ O of aragonite progressively decreases from ca. 413 ka to ca. 135ka by 3.25 ‰ (Fig. 4.4-41 & 4.4-45). Initially high  $\delta^{18}$ O of aragonite is interpreted to reflect heavy  $\delta^{18}O_{H2O}$  resulting from an increased proportion of Paradox formation brine in the early fluids, with progressively decreasing contributions to ca. 135ka, and constant contributions there after. Following the CO<sub>2</sub> charge at ca. 135ka  $\delta^{18}$ O of aragonite progressively increases at the same rate as  $\delta^{13}$ C. Differences in the range of  $\delta^{18}$ O between LGF and SWG reflect consistent differences in the volume of brine influx between each fault system, in both modern and ancient settings. This probably reflects intrinsic differences in the fault architecture and hydrological systems between each fault. The northern fault of Salt Wash Graben penetrates to greater depth than Little Grand Wash Fault (Dockrill, 2005). And as such the fault may also act as a more significant conduit to upward fluid movement.

#### 4.4.11.2. <sup>87</sup>Sr/<sup>86</sup>Sr

Depression of the fluid  $\delta^{13}$ C is accompanied by the initiation of exponentially increasing  ${}^{87}$ Sr/ ${}^{86}$ Sr. Increase in the <sup>87</sup>Sr/<sup>86</sup>Sr of aragonite reflects an increased contribution of <sup>87</sup>Sr from silicate mineral dissolution following injection of  $CO_2$  into the reservoir. Covariation of  $\delta^{13}C$  and <sup>87</sup>Sr/<sup>86</sup>Sr reflects a coupling between the CO<sub>2</sub>-charge and mineral dissolution. Influxing CO<sub>2</sub> will suppress fluid pH and mineral saturation, elevate  $[H^+]$  and enhance mineral dissolution rates. Sr incorporated into aragonite will de derived from three primary sources: 1) dissolved Sr carried in groundwater advected into the fault system; 2) high <sup>87</sup>Sr/<sup>86</sup>Sr derived from silicate mineral hydrolysis and; 3) low <sup>87</sup>Sr/<sup>86</sup>Sr derived from dolomite dissolution, within the zone of high CO<sub>2</sub>charge. Additionally, low <sup>87</sup>Sr/<sup>86</sup>Sr may be added at the site of CO<sub>2</sub> injection derived from brine entrained in the CO<sub>2</sub> stream. The rate of change d<sup>87</sup>Sr/<sup>86</sup>Sr/dt of aragonite will largely reflect the ratio of the rate of Sr liberation from silicate and dolomite dissolution assuming 1) the initial dissolved Sr flux and <sup>87</sup>Sr/<sup>86</sup>Sr is constant; 2) the flux of Sr in groundwater is exceeded by the flux in Sr derived from mineral dissolution. The exponential increase in <sup>87</sup>Sr/<sup>86</sup>Sr following introduction of the 135 ka  $CO_2$  charge can reflect either; 1) initial dissolution of both silicate and dolomite, but at different rates, or; 2) that the rate of silicate mineral dissolution increased with time. The former explanation is the most likely and the form of d<sup>87</sup>Sr/<sup>86</sup>Sr/dt suggests a decline in the rate of dolomite dissolution to ca 95ka. Inversion of the exponentially increasing trend in <sup>87</sup>Sr/<sup>86</sup>Sr to an exponentially decreasing trend at ca 93 ka reflects groundwater Sr flux exceeding Sr-flux from mineral dissolution. This reflects slowing of the dissolution rate of silicate minerals over ca. 42 ka as the fluid losses CO<sub>2</sub> through degassing, pH is neutralized by reaction and porefluid chemistry moves towards equilibrium with the silicate mineral surface.

#### 4.4.11.3. Little Grand Wash Fault

<sup>87</sup>Sr/<sup>86</sup>Sr declines exponentially from 114 ka to 106 ka and  $\delta^{13}$ C and  $\delta^{18}$ O increase (Fig. 4.4-45) concomitantly due to rapid CO<sub>2</sub>-leakage and degassing. <sup>87</sup>Sr/<sup>86</sup>Sr decline from an initially high value suggests injection of CO<sub>2</sub> prior to 114ka and that silicate dissolution rates declined as CO<sub>2</sub> saturation decreased. Between ca. 59ka and 5ka a gradual decline in  $\delta^{13}$ C coupled with increasing <sup>87</sup>Sr/<sup>86</sup>Sr and  $\delta^{18}$ O is interpreted to reflect slow bleeding of a CO<sub>2</sub>-brine mixture into the reservoir (Figs. 4.4-45 & 4.4-46).



**Figure 4.4-46** The  $\delta^{13}$ C and  $\delta^{18}$ O of HCO<sub>3</sub><sup>-</sup> in equilibrium with aragonite veins from LGF. Fitting of kinetic fraction models implies degassing from a fluid reservoir with initial  $\delta^{13}C_{HCO3}$  lower than that observed in modern fluids. Dated veins constrain the trajectory of the evolution in isotopic composition of HCO<sub>3</sub><sup>-</sup> through time.

#### 4.4.12. Controls on Leakage

Differences between the slope of  $d\delta^{13}$ C/dt and  $d\delta^{18}$ O/dt, the time taken for the  $\delta^{13}$ C/ $\delta^{18}$ O trend to plateau, and the rate of travertine deposition (Fig. 4.4-45) reflect intrinsic differences in the CO<sub>2</sub>-leakage rate of each fault. The trends record far more rapid CO<sub>2</sub> loss from Little Grand Fault. The volume of dated travertine records the mass of CO<sub>2</sub> leaked from each fault and the variation in the CO<sub>2</sub> leakage rate through time (Fig. 4.4-47). The mass of leaked CO<sub>2</sub> can be estimated by assuming that every litre of effused fluid deposited ~10 mmoles of CaCO<sub>3</sub> (Ca<sup>2+</sup> loss is estimated from differences in Ca<sup>2+</sup> concentration in spring waters and Ca<sup>2+</sup> concentration after prolonged runoff) and that each litre of fluid was initially saturated with CO<sub>2</sub> at reservoir conditions. This calculation implies a similar cumulative loss of CO<sub>2</sub> from each fault: LGF; 1.2x10<sup>7</sup> tonnes (CO<sub>2</sub>) and SWG; 1.3x10<sup>7</sup> tonnes (CO<sub>2</sub>). Initial leakage rates are up to ~633 t/a and ~927 t/a for SWG

and LGF, respectively. However, average leakage rates of 50-100 t/a are more common. These leakage rates during periods of quiescence are comparable to modern CO<sub>2</sub> effusion rates of ~55 t/a measured at SWG by Allis *et al.*, (2005). Variation in the leakage rate is presented in figure (4.4-47). The 'average' large (600 Mw) coal burning power station in the USA produces  $4-5x10^6$ t/a (CO<sub>2</sub>) (IPCC, 2007). Many of these have been in existence since the 1950's, giving a cumulative CO<sub>2</sub> production of ~2.3x10<sup>8</sup> tonnes (CO<sub>2</sub>). Whilst the magnitude of leaked CO<sub>2</sub> obviously depends on the volume of the initial CO<sub>2</sub>-charge a fault leaking CO<sub>2</sub>-saturated reservoir will therefore still leak at rates significantly lower than 'leaking' power stations.

The spatial-temporal pattern of travertine formation (Fig. 4.4-48), for both LGF and SWG, suggests that: a) a new CO<sub>2</sub>-charge always initial exploits leakage pathways at the crest of the anticline (or zones of high structural complexity such as the easterly breached relay ramp); b) for SWG this central leakage site moves by small distances (10's to 100's meters) eastward with younger charges, in the direction of groundwater flow, suggesting the continued formation of new leakage pathways rather than the re-exploitation of older leakage pathways, at the anticline crest; c) with time from the initial introduction of a new CO<sub>2</sub>-charge, leakage pathways spread from the anticline crest laterally along the fault trace. This spatial-temporal relationship is interpreted as reflecting: a) the establishment of new leakage pathways with the introduction of a new CO<sub>2</sub>-charge due to mineral-fluid reactions at the cap-rock reservoir interface, and within fracture zones and the fault damage zone. These pathways are localized at the apex of the anticline initially, due to the buoyant accumulation of free-phase CO<sub>2</sub>; b) these initial leakage pathways then become blocked by the deposition of carbonate within fractures; c) the lateral migration of leakage points as initial pathways become blocked and CO<sub>2</sub>-charged fluids exploit, and initiate, more complex and ss hydraulically conductive leakage pathways along the length of the fault trace.



**Figure 4.4-47** Variation in the cumulative travertine volume with time for LGF and SWG. Estimated leakage rates (tonnes  $(CO_2)$ /year) during periods of rapid  $CO_2$  loss and quiescence are detailed at the top of each figure. Temporal data and surface travertine volumes are estimated from the maps of Burnside, (2007).

The spatial-temporal trend of travertine deposition (Fig. 4.4-48) implies an increase in the blocking rate of leakage pathways with time. This is interpreted to reflect progressive CO<sub>2</sub> loss from the reservoir and a decrease in in-situ  $pCO_2$ , which elevates  $\Omega_{cc}$  in the upwelling fluid increasing the rate of carbonate deposition. Differences between the slope of this trend in each fault system record more rapid blocking rates in SWG than in LGF. This may be due to differences in reservoir depth (the Navajo Aquifer is located at ~500m depth at LGF and at ~250m depth at SWG) and thus differences in the in-situ  $pCO_2$  at each fault, which imposes differences in the  $\Omega_{cc}$  of the upwelling fluid.

Differences in the rate of CO<sub>2</sub>-leakge at each fault may reflect differences in the volume of the initial CO<sub>2</sub>-charge, depth to the host reservoir, the fracture blocking rate, local hydraulic head, pore over-pressure and intrinsic differences in the permeability structure of the fault damage zone, the stratigraphic architecture and reservoir-seal juxtaposition between each fault. Slow leakage rates at SWG, as compared to LGF, are largely due to the high throw, lower degree of reservoir-reservoir juxtaposition and higher shale gouge ratio (Dockrill, 2005) of this fault system. However, the hydraulic properties of the near surface lithologies may also impact on the leakage rate. Shallow lithologies at LGF comprise low permeability formations of the Curtis Formation and Mancos Shale, and at SWG the more permeable Entrada Sandstone. The observation of aragonite veining extending laterally some distance from individual travertine mounds and the extensive deformation associated with free gas accumulation in the subsurface, together with isotopic evidence discussed, suggests substantial degassing of  $CO_2$  in the shallow subsurface at SWG. These features are largely absent from LGF suggesting fluids rapidly ascended leakage pathways without significant interaction with shallow formations. It is inferred that surface leakage at LGF has historically taken the form of active cold water geysering, which has actively stimulated leakage and has had a significant impact on the time taken for an individual  $CO_2$  charge to dissipate. Additionally, higher levels of local hydraulic head at LGW will have helped sustain high rates of fluid discharge.



**Figure 4.4-48** The spatial distribution of individual travertine mounds versus their age for LGF, SWG and for travertines associated with the 135ka leakage event at SWG. Spatial and temporal data from Burnside, (2007).

## 4.5. Conclusions

Extensive alteration and cementation in the Entrada Sandstone beneath surface travertine deposits preserves the geochemical and mineralogical impacts of interaction with  $CO_2$ -charged fluids. Feldspar grains show evidence of extensive corrosion and reprecipitation of silica, smectite and kaolinite on grain surfaces and within the local pore volume. Feldspar grains continue to dissolve even when coated with up to 10µm surface coatings of inter-grown clay minerals, suggesting the maintenance of porosity within the surface coating. This adds to the evidence that the presence of such a coating does not inhibit dissolution at the mineral surface.

High Mn and Fe concentrations in fracture and host rock calcite cements record elevated  $Mn^{2+}$  and Fe<sup>2+</sup> concentrations in the parent fluid. Fe and Mn concentrations imply reducing Eh conditions (30 to -50 mV) in the parent fluid and a pH in the range 5.5 to 6.5, comparable to the Eh-pH conditions of the modern CO<sub>2</sub>-charged groundwaters. This finding, together with hematite solubility modelling and field and petrographic observations of extensive dissolution of hematite grain coatings and Fe-oxide reprecipitation, suggests that CO<sub>2</sub>-charged fluids alone are capable of dissolving and mobilizing Fe in these sediments. However, the precise control on Eh is uncertain. Equilibrium redox potentials for the SO<sub>4</sub><sup>2-</sup>-H<sub>2</sub>S and CO<sub>2</sub>-CH<sub>4</sub> redox couples are in the region of 0 to -200 mV and -200 to -500mV, respectively (Drever, 1997). The calculated Eh values are generally higher those expected for redox potentials controlled by either SO<sub>4</sub><sup>2-</sup>-H<sub>2</sub>S or CO<sub>2</sub>-CH<sub>4</sub> equilibrium. The range of values obtained is more comparable to redox potentials observed in groundwaters with low O-fugacity (e.g. White *et al.*, 1990).

Sr concentrations in these cements record mean calcite precipitation rates of  $1.3 \times 10^{-6}$  to  $2.1 \times 10^{-6}$  mol/m<sup>2</sup>/s, comparable to laboratory derived calcite precipitation rates, in fluids with moderate Mn/Ca and Fe/Ca, at  $\Omega_{cc}$  of ~1 to 3. The overall variation in rate is large, from ~1x10<sup>-9</sup> to ~1x10<sup>-5</sup> mol/m<sup>2</sup>/s, probably reflecting both variation in the intrinsic rate and variation in the Sr/Ca of the parent fluid.

Mg and Sr concentrations in calcite cements away from fracture conduits record closed system fractionation of the fluid Sr/Ca and Mg/Ca by calcite precipitation, which elevated the Mg/Ca ratio sufficiently to allow kinetic stabilization of aragonite and the precipitation of poikilitic aragonite cements. However, other kinetic factors such as the  $\Omega_{cc}$  of the fluid and  $[CO_3^{2-}]$  most likely also contributed to this stabilization.

Ancient travertine deposits and aragonite veining record leakage of CO<sub>2</sub> from the Navajo Aquifer that initiated at ca 413 ka at Salt Wash Graben and at ca 114 ka at Little Grand Fault. At Salt Wash Graben a second injection of CO<sub>2</sub> at ca 135 ka initiated simultaneous variation in  $\delta^{18}O_{CaCO3}$  and  $\delta^{13}C_{CaCO3}$ , and a spike in <sup>87</sup>Sr/<sup>86</sup>Sr which is interpreted to reflect near coeval injection of CO<sub>2</sub> into the aquifer and the initiation of surface leakage as a result of this injection. Temporal trends in <sup>87</sup>Sr/<sup>86</sup>Sr record enhanced silicate mineral dissolution rates following injection of this CO<sub>2</sub> charge, but dissolution rates decreased as CO<sub>2</sub> was lost from the reservoir, pH increased and saturation with respect to the dissolving mineral was approached (Chapter 3). Correlations in  $\delta^{18}O_{CaCO3}$  and  $\delta^{13}C_{CaCO3}$ , kinetic fractionation of the HCO<sub>3</sub> (aq) reservoir, the volume and rate of surface travertine formation and its spatial and temporal distribution suggest that initially leakage: a) occurred rapidly and at a constant rate, b) was localised at the anticline crest and c) occurred from a reservoir fluid saturated in  $CO_2$ , coexisting with a free-gas phase. Additionally, kinetic fractionation of  $HCO_3$  (aq) during these periods implies rapid rates of  $CO_2$ degassing and carbonate precipitation, faster than the  $HCO_3$ -H<sub>2</sub>O equilibration reaction which operates on the 1000's to 10000's sec time-scale (Hendy, 1971). A sharp inflection in leakage rate and an approximately concurrent cessation in kinetic fraction of the HCO<sub>3</sub> (aq) reservoir are interpreted to reflect depletion of the saturated CO<sub>2</sub> and a return to undersaturated conditions, after ~75ka of leakage. During this time leakage sites propagated laterally along the length of the fault trace as fracture conduits were blocked by carbonate deposition and new leakage pathways were exploited and opened by mineral-fluid reactions. Fracture blocking rates increased as the  $CO_2$  charge dissipated,  $pCO_2$  in the aquifer fell and the fluids became increasingly oversaturated in carbonate.

Whilst the cumulative CO<sub>2</sub> loss from both Little Grand Fault and Salt Wash Graben are of the same order of magnitude ( $\sim 1 \times 10^7$  tonnes CO<sub>2</sub>), the time required to deplete the initial CO<sub>2</sub>charge to a state of  $CO_2$ -undersaturation (~8 ka versus ~75 ka), and leakage rates during this period (~927 t/a versus ~164 t/a), vary by an order of magnitude between the two fault systems. This is attributed primarily to intrinsic difference in the fault architecture and properties of the fault damage zone, including the shale gouge ratio and degree of reservoir-reservoir juxtaposition. However, the depth of the host reservoir, and thus maximum in-situ  $pCO_2$ , imposes difference in the fracture blocking rate in each fault which may impact the overall leakage rates. In addition the hydraulic properties of shallow lithologies appear to be important in controlling leakage rates where permeable formations allow migration of  $CO_2$ -charged fluids away from the fault damage zone, prolonging the fluid ascent time, enhancing  $CO_2$  degassing in the shallow subsurface and promoting carbonate deposition and fracture blocking. This highlights the importance of accurately modelling the fault surface, damaged zone, shallow lithological properties and regional hydraulic gradients when modelling leakage from  $CO_2$  storage sites. The findings suggest that in geological storage sites fault controlled CO<sub>2</sub> leakage rates from shallow CO<sub>2</sub> saturated fluids will be slow (relative to  $CO_2$  emission rates from anthropogenic sources) and fracture conduits will seal through carbonate precipitation impeding leakage, but that this process is likely to take place on 100's to 1000's year time-scales.

## **Chapter 5**

# Fluid Inclusion Petrography of Diagenetic Bleaching in the Entrada Sandstone, Green River, Utah

## 5.1. Introduction

Across the Paradox Basin, adjacent to faults and preferentially in coarser grained sandstone units, originally red Jurassic sandstones are frequently bleached pale-yellow or white were hematite grain coatings have been dissolved by the passage of diagenetic fluids (Foxford *et al.*, 1996; Garden *et al.*, 2001). This bleaching has been attributed by various authors to a variety of different extra-formational fluids including hydrocarbon liquids, organic acids and methane (Beitler *et al.*, 2005; Bowen, 2005; Chan *et al.*, 2000, 2001; Eichhubl *et al.*, 2009; Garden *et al.*, 2001; Parry *et al.*, 2004), and carbon dioxide and hydrogen sulphide (Haszeldine *et al.*, 2005).

Regionally bleached sandstones record the passage of migrating diagenetic fluids over a variety of physical and temporal scales (e.g. Bowen *et al.*, 2007). Understanding their geochemical origin facilitates their use as a reservoir analogue, from which the petrophysical and geochemical controls on fluid flow can be made by direct observation. Additionally, exhumed reservoirs such as these provide the opportunity to examine the coupling of fluid transport and mineral-fluid interactions, directly (e.g. Bickle, 1992). Constraining the large-scale migration of fluids in the subsurface has traditionally only been possible via numerical simulation or by direct geochemical observations in well studied groundwater systems (e.g. O'Nions et al., 1993) or hydrocarbon fields (e.g. Bradley et al., 1986).

In this chapter the petrology and isotope geochemistry of large-scale diagenetic bleaching of the Entrada Sandstone at Salt Wash Graben is discussed. Fluid inclusions trapped in secondary minerals associated with this bleaching, and with bleaching in travertine feeder zones (discussed in Chapter 4) were examined using laser Raman microspectroscopic and microthermometric techniques, and the results are presented and discussed. Mineral hosted fluid inclusions may preserve fluid and vapour compositions at the time of trapping yielding information on the thermal, pressure and chemical regimes under which that mineral developed. The objectives of this chapter are to a) establish the composition of the volatile phase(s) (i.e. CH<sub>4</sub>, CO<sub>2</sub>, N<sub>2</sub>, O<sub>2</sub>, H<sub>2</sub>,  $H_2S$ ,  $SO_2$ ) associated with large-scale diagenetic bleaching of the Entrada Sandstone at Salt Wash Graben. b) To assess whether volatile phase(s) in addition to  $CO_2$ , were present in the ancient  $CO_2$ -system c) to derive thermal and pressure data which will inform on the relative timing of the large-scale diagenetic bleaching.

## 5.2. Methodology

#### 5.1.1. Fluid Inclusions

When crystals grow or recrystallize in a fluid medium, growth irregularities result in the trapping of small portions of the fluid in the solid crystal, yielding primary fluid inclusions. Healing of fractures developed in existing crystal can also lead to the entrapment of secondary fluid inclusions.

#### 5.1.1.1. Microthermometry

Microthermometry techniques provide information on the melting point of included aqueous fluids and the homogenisation temperature of two phase vapour-liquid mixtures. Measurement of the homogenization temperature ( $T_h$ ) and temperature of last ice melting ( $T_m$ ) in fluid inclusions provides information on the minimum temperature of the fluid inclusions formation and the salinity of fluids from which the cement(s) precipitated (Roedder, 1984).

#### 5.1.1.2. T<sub>m</sub>

Aqueous fluids in geological environments typically contain varying amounts of salt, dominantly NaCl, KCl or CaCl<sub>2</sub> (Bodnar, 2003). Salts and other solutes depress the melting point of ice, thus the temperature at which the last remaining ice in an inclusion melts will reflect the salinity of the fluid. The relationship between freezing point depression and salinity varies only slightly for the various species dominant in the fluid (Bodnar, 2003). Most researchers report their interpretations of freezing point depression in weight % NaCl equivalent, simply stating the salinity of fluid inclusions assuming all dissolved species to be NaCl. This yields a salinity that is fairly close to reality for many diagenetic systems (Roedder, 1984).



**Figure 5.2-1** NaCl-H<sub>2</sub>O phase diagram, after Bodnar, (2003). I = ice; L = liquid; HH = hydrohalite; H = halite; P = peritectic (0.1°C, 26.3 wt% NaCl); E = eutectic (-21.2°C, 23.2 wt% NaCl).

Figure (5.2.1) shows the H<sub>2</sub>O-NaCl phase relations in the low temperature region, including the relationship between salinity and the ice melting temperature. Hall *et al.*, (1988) determined the freezing-point depression of H<sub>2</sub>O-NaCl solutions ranging from pure water to the eutectic composition (23.2 wt% NaCl), and Bodnar (1993) presented a simple equation according to:

$$Salinity(wt\%) = 1.78\alpha - 0.0442\alpha^2 + 0.000557\alpha^3$$
(5.1)

where  $\alpha$  is the freezing point depression (FPD) in degrees Celsius (FPD is simply the negative of the freezing temperature). Equation (5.1) reproduces the original experimental data of Hall *et al.*, (1988) to better than ±0.05 wt% NaCl at all temperatures from 0.0°C to -21.2°C, the eutectic temperature for H<sub>2</sub>O-NaCl.

The presence of  $CO_2$  in a fluid inclusion may affect the melting temperature obtained from phase relations determined in  $CO_2$ -free systems. However, in fluid inclusions which have both liquid and vapour phases, most  $CO_2$  is contained in the vapour phase at the temperature of final ice melting (Roedder, 1984). Therefore, only very small  $CO_2$  concentrations exist in the liquid phase, and thus the affect of  $CO_2$  on the temperature of ice melting is considered insignificant (Frantz *et al.*, 1992). Frantz *et al.*, (1992) observed that the presence of up to 43.2 mol%  $CO_2$  in individual inclusions had a negligible effect on final ice melting temperature.

#### $5.1.1.3. T_h$

A conspicuous feature of many aqueous fluid inclusions is a vapour or gas bubble. Phase separation (liquid and vapour) is a result of differential shrinkage of the host mineral and the inclusion fluid on cooling from the temperature of trapping to that of observation. Upon cooling
to room temperature, the fluid shrinks far more than the host, thus, the pressure in the inclusions drops below the saturation vapour pressure of the contained fluid and the fluid splits into two phases: liquid and vapour. Artificially heating a two-phase inclusion observed at ambient temperatures and observing the point of homogenisation provides information on the temperature of entrapment.

If a fluid inclusion is trapped from a homogeneous fluid below or on a boiling curve (i.e. under P-T conditions such that it was in equilibrium with either a vapour or gas phase) the temperature of homogenisation represents the actual trapping temperature of the inclusion. However, some inclusions have trapped fluids at a P-T combination above the liquid/vapour curve. In these, a bubble disappears on heating up from room temperature when the pressure and temperature have increased to the liquid/vapour curve, below the actual temperature at which the fluid was included. There can be a large difference between the measured  $T_h$  and the true trapping temperature ( $T_t$ ). In order to obtain the true trapping temperatures of an inclusion trapped at high P-T conditions, a pressure correlation needs to be applied. However given that fluids within the studied system were included at temperatures significantly below the boiling curve for H<sub>2</sub>O-NaCl-CO<sub>2</sub> systems this consideration is unnecessary.

#### 5.1.2. Raman Microspectroscopy

The laser Raman microprobe (LRM) permits the spectroscopic analysis of solid, liquid and gas phases as small as a few micrometers. In this technique of molecular spectroscopy the sample is imaged through the high power objective of an optical microscope. The Raman effect is the shift in frequency that monochromatic light (e.g., laser light) undergoes during inelastic scattering (Burke, 2001). Only the spectral distribution of the inelastically scattered light emitted by the sample (Raman scattering) is of analytical interest, since it is caused by component-specific molecular vibrational and rotational phenomena in the sample. The scattered light is transmitted through the microscope into a double monochromator, step scanned, and detected with a monochannel photon-counting system (Seitz *et al.*, 1987). The spectra are recorded in terms of the amount of displacement from the frequency of the exciting (laser) radiation.

The accompanying spectra are plots of total counts vs. wave numbers (cm<sup>-1</sup>). The photon count rate of the inelastically scattered radiation is a function of both the sample and the instrumental conditions (Burke, 2001). In regard to the former the Raman band intensities are largely proportional to the number of molecules in the scattering volume or the density (Long, 1977). Among the latter are the exciting laser power, the alignment of the laser in the optical system, the optical properties of the objectives, the chosen slit width, and the electronic parameters of the detection system (Burke, 2001). The total number of recorded counts depends upon the count rate, the counting time (signal integration time per step of the monochromator

during a scan), and the spacing of the steps (number of wave numbers between each step) (Seitz *et al.*, 1987). Analysing the spectra collected enables identification of the species that are contained within a fluid inclusion by identifying the unique band assemblage of individual species.

Multiple species in both the vapour and liquid phase of a fluid inclusion can be identified by laser Raman microprobe spectroscopy (Wopenka and Pasteris, 1987). Raman quantitative analysis based on Placzek's polarizability theory (Placzek, 1934) can be applied to derive a compositional analysis for Raman active species (e.g. H<sub>2</sub>O, CO<sub>2</sub>, CO, N<sub>2</sub>, H<sub>2</sub>S, SO<sub>2</sub>, CH<sub>2</sub>, O<sub>2</sub>, H<sub>2</sub>) in a fluid inclusions liquid and vapour phases. This allows estimates of the relative gas composition and the contribution of CO<sub>2</sub> in individual inclusions and distinct diagenetic events.

Theoretical estimates of the detection limits of Raman microprobes in general are in the pictogram  $(10^{-12} \text{ g})$  range (Etz, 1979). As pointed out by Rosasco *et al.*, (1979), the detection limit for a species in a fluid inclusion depends upon the scattering efficiency of the species itself, the counting time and stepping interval, the Raman and optical properties of the host, the geometry of the inclusion, spectral interference (e.g., overlapping Raman peaks, fluorescence) from other components, and the stability of the species under the impinging laser beam. Using Raman spectroscopy, CO<sub>2</sub> can be detected to about 1 bar at ambient temperature (Rosso and Bodnar, 1995). A lack of appropriate standards prevents the quantification of instrumental detection limits in this study.

In this study Raman spectroscopy was used to identify  $CO_2$  and other volatile bearing inclusions in distinct diagenetic assemblages and to provide a quantitative estimation of the gas composition of vapour bearing fluid inclusions. The pressure dependent bond configurations of some Raman active species (e.g.  $CO_2$ ,  $CH_4$  and  $N_2$ ) allows features of the Raman spectra to be used to calculate vapour phase gas densities, dissolved gas concentrations in the liquid phase, entrapment pressures and thus entrapment depths.

## 5.1.2.1. The Spectrum of $CO_2$

The CO<sub>2</sub> molecule is linear and thus has four modes of vibration (Fig. 5.2-2); a symmetric stretching mode (v1), an antisymmetric stretching mode (v<sub>3</sub>), and two bending modes (v<sub>2</sub>a and v<sub>2</sub>b)



Figure 5.2-2 Schematic representation of the three fundamental vibrations of  $CO_2$  (after Rosso and Bodnar, 1995)



**Figure 5.2-3** Typical Raman spectrum of  $CO_2$  with background subtracted. Peaks marked ( $v_1$ -2 $v_2$ ) comprise the  $v_1$ -2 $v_2$  Fermi diad. The hot bands are also coupled through Fermi resonance (modified after Rosso and Bodnar, 1995).

which have the same frequency of vibration and form a degenerate pair (Gordon and McCubbin, 1966) (Fig. 5.2-3). The symmetric stretching mode is the only predicted Raman-active vibration because the derivative of the change in total molecular polarizability during this motion is nonzero (Rosso and Bodnar, 1995).

Due to Fermi resonance, the admixed excited  $v_1$  and  $2v_2$  states are split apart and two strong CO<sub>2</sub> bands are present in the Raman spectrum. These two bands are referred to as the  $v_1$ - $2v_2$  Fermi diad and have the approximate frequencies 1388 cm<sup>-1</sup> (upper band) and 1285 cm<sup>-1</sup> (lower band) (Gordon and McCubbin, 1966; Rosso and Bodnar, 1995) (Fig. 5.2-3). Another band type is represented by low intensity peaks flanking the Fermi diad, which are referred to as hot bands. Their resultant frequencies are approximately 1264 cm<sup>-1</sup> and 1409 cm<sup>-1</sup> (Fig. 5.2-3). They arise from transitions that originate in excited vibrational states higher in energy than the ground vibrational state due to the thermal energy of the molecules (Rosso and Bodnar, 1995). The hot bands are also perturbed by Fermi resonance (Rosso and Bodnar, 1995). The intensity of the hot bands of the Raman spectra of  $CO_2$  increases concomitantly with increased temperature of  $CO_2$ ; at ambient temperatures they are typically not observable (Brown and Steeper, 1991).

#### 5.1.2.2. Relative Gas Compositions

According to Placzek's (1934) polarizability theory, the area of a Raman peak (over a finite range of wave numbers) is a function of (1) the number of molecules of a certain species in the scattering volume (absolute concentration of the species), (2) the Raman scattering cross section of the species, (3) the irradiance of the specimen, and (4) the solid angle of light collection. If two or more Raman-active species in the same phase of a fluid inclusion are analyzed either at the same time or one immediately after the other, the irradiance, the scattering volume, and the angle of collection of light are assumed to be the same for all the species. Thus instrumental effects on peak height and area are negated and the ratio of two or more species can be estimated. In practice, for a two-component system, the experimental result in units of mole percentages ( $C_a$ ,  $C_b$ ) is the function of three ratios: one for the determined Raman peak area ( $A_a$ ,  $A_b$ ), one for the relative scattering cross sections ( $\sigma_a$ ,  $\sigma_b$ ) of the two species, and one for the instrumental efficiencies ( $\eta_a$ ,  $\eta_b$ ) for Raman scattered light at specific wavelengths and polarization orientation. The  $\sigma$ 's and  $\eta$ 's can be combined into "Raman quantification factors" ( $F_a$ ,  $F_b$ ) (Wopenka and Pasteris, 1987). The quantitative relationship between the relative concentration of two components, *a* and *b*, and their Raman peak areas reduce to a simple formula:

$$A_a/A_b = (C_a/C_b) \cdot (\sigma_a/\sigma_b) \cdot (\eta_a/\eta_b) = (C_a/C_b) \cdot (F_a/F_b)$$
(5.2)

This equation requires knowledge of the Raman scattering efficiencies ( $\sigma$ 's) for the different components and the instrumental efficiencies ( $\eta$ 's) for Raman scattering radiation arising from those components.

In calculating the mol% of  $CO_2$  and  $CH_4$  in gas mixtures the 1388 cm<sup>-1</sup> and 2917 cm<sup>-1</sup> peak are used as comparative bands. It has long been realized that the cross-section of a volatile changes with the total pressure in a given fluid inclusion (Rosso and Bodnar, 1995). For  $CH_4$  and  $CO_2$  in calibration gas mixtures up to 15 bars total pressure, Wopenka and Pasteris (1987) determined F-factors (relative to N<sub>2</sub>) of 6.7 and 1.5, respectively, for their laser Raman microprobe. The ratio of these F-factors is 4.4. Such ratios for low density gas mixtures are the ones most appropriate for the species in gas bubbles in this study and are therefore adopted to quantify the contents of the vapour phase. For a  $CH_4$ - $CO_2$  supercritical fluid with a density of about 80 cm<sup>3</sup>/mole (about 80 bars at room temperature), the empirically determined F-factor ratio

is 2.9, a relative decrease of about 34% compared to the ratio obtained at low pressure (Seitz *et al.*, 1987).

However, the fact that there are several instrument-specific parameters makes it problematic to apply the above empirical F-factors to different instruments. Among the most important instrumental factors are the different sensitivities of the gratings and the detector system for Raman scattered light of different polarization orientations and/or wavelengths. The use of the microscope of a laser Raman spectrometer will cause additional optical effects due to different components (e.g., objective, beam splitter, lenses) (Wopenka and Pasteris, 1987). Since each optical component has its own spectral characteristics that are a function of both wavelength and polarization orientation of the interacting light, the published F-factors are only approximate solutions for the Raman instruments used in this study.

In fluid inclusions from high temperature geological systems, ductile strain (e.g. Hollister, 1989) or diffusion along dislocation edges (e.g. Cordier et al., 1994) can lead to because enrichment of components such as  $CO_2$  and NaCl as  $H_2O$  is soluble and can diffuse through the silicate lattice. In such a low temperature system as that examined these processes are not thought to significantly contribute to alteration of the fluid composition.

#### 5.1.2.3. Gas Density

The sensitivity of bond configuration to the pressure on or density of a phase has been documented in the Raman spectra of gaseous  $CO_2$  (Bertran, 1983),  $CH_4$  (May *et al.*, 1959), and N<sub>2</sub>. This effect has been previously noted in the spectra of natural fluid inclusions (e.g. Burke, 2001; Rosasco *et al.*, 1975; Dubessy *et al.*, 2001).

Many previous studies have documented the density-dependent band shift in Raman peaks of pure CO<sub>2</sub> (e.g., Wang & Wright, 1973; Bertrán, 1983; Garrabos *et al.*, 1989a,b; Rosso & Bodnar, 1995; Yamamoto & Kagi, 2006). In the spectrum of CO<sub>2</sub>, the bands of the Fermi diad shift to lower wave numbers with increasing density. The frequency shift of the lower band has a higher density dependence than does the upper band. At the same time, the intensity ratio of the upper band to the lower band increases with increasing density (Garrabos *et al.*, 1980) The split ( $\Delta$ ) between the Fermi diad peaks increases with increasing density of CO<sub>2</sub> (e.g., Bertrán, 1983; Kawakami *et al.*, 2003). Rosso and Bodnar (1995) have calibrated the dependence of the Fermi diad separation on CO<sub>2</sub> density from a compilation of experimental results ranging from analyses of low density gaseous CO<sub>2</sub> to liquid CO<sub>2</sub> in the density range of 0.01– 1.20 g/cm<sup>3</sup>. Within this density range the relationship between  $\Delta$  and density is assumed to be linear (Hacura *et al.*, 1997). This resulted in the following empirical fit suitable for estimating CO<sub>2</sub> densities (g/cm<sup>3</sup>):

$$\rho_{co_2} = \frac{\left(\Delta - 102.68\right)}{2.49} \tag{5.3}$$

The overall precision of the determination of  $\Delta$  is approximately 0.05 cm<sup>-1</sup> which equates to  $\pm 0.02$  g/cm<sup>3</sup>.

The total pressure  $(P_T)$  of a mixture of ideal gases is equal to the sum of the partial pressures of the individual gases in the mixture as stated by Dalton's law. For the vapour phase of a fluid inclusion containing CO<sub>2</sub>, CH<sub>4</sub> and H<sub>2</sub>O vapour, P<sub>T</sub> is defined as

$$P_T = P_{CH_4} + P_{CO_2} + P_{H_2O}$$
(5.4)

where  $P_{CH4}$ ,  $P_{CO2}$  and  $P_{H2O}$  are the gas partial pressures of CH<sub>4</sub>, CO<sub>2</sub> and H<sub>2</sub>O in the vapour phase. For fluid inclusions at room temperature the total pressure is essentially  $P_{CO2}+P_{CH4}$  since the vapour pressure of water at ambient temperatures is negligible (Hedenquist and Henley, 1985).

The mole fraction of a gas component in a gas mixture is equal to the volumetric fraction of that component in a gas mixture. The mole fraction  $(x_i)$  of an individual gas component (i) in an ideal gas mixture can be expressed in terms of the component's partial pressure  $(P_i)$  or the moles of the component  $(n_i)$  as

$$x_i = \frac{P_i}{P_T} = \frac{n_i}{n} \tag{5.5}$$

and the partial pressure of an individual gas component in an ideal gas can be obtained using this expression:

$$P_i = x_i \cdot P_T \tag{5.6}$$

From the calculated  $CO_2$  gas density the inclusion  $CO_2$  partial pressure can be estimated from the combined ideal gas law expressed as a function of density and temperature as

$$P_{CO_2} = \rho_{CO_2} \cdot (R \cdot T) \tag{5.7}$$

where  $\rho_{CO2}$  is the CO<sub>2</sub> gas density,  $P_{CO2}$  is CO<sub>2</sub> partial pressure, R is the specific gas constant for CO<sub>2</sub> (188.9 J/kg·K) and T is absolute temperature at the time of the spectra acquisition. In inclusions containing only CO<sub>2</sub> in the vapour phase  $P_{CO2}=P_T$ . The uncertainty associated with measurement of  $\rho_{CO2}$  results in an uncertainty in  $P_{CO2}$  of ±1.03 MPa.

From the total inclusion pressure  $(P_T)$  the depth (m) of inclusion formation can be estimated, assuming a hydrostatic pressure gradient, according to

$$Depth = \left(P_T - P_{atm}\right) / \left(\rho_{fluid} \cdot g\right)$$
(5.8)

Where  $P_T$  is the inclusion pressure,  $P_{atm}$  is atmospheric pressure,  $\rho_{fluid}$  is the average density of the pore fluid (1.01 g/cm<sup>3</sup>) and g is the acceleration due to gravity. Propagating the uncertainty in  $\rho_{CO2}$  results in an uncertainty in the depth estimate of ±96 m.

As shown by May *et al.*, (1959), the Raman spectrum of CH<sub>4</sub> in the fluid state depends on pressure. The wave number of the Raman peak for the symmetric C-H stretching mode ( $v_1$ ) decreases as pressure increases. Lu *et al.*, (2007) have quantified the dependency of the measured Raman shifts of C–H symmetric stretching band ( $v_1$ ) in the vapour phase with methane vapour pressures in inclusions from a compilation of experimental and natural fluid datasets. They derive a unified equation for the relationship between pressure and Raman peak position at isothermal conditions by using all available data, such that it can be applied reliably in any laboratory. The shift, D (in cm<sup>-1</sup>) of  $v_1$  from  $v_0$  (2917.30 cm<sup>-1</sup>), the CH<sub>4</sub>  $v_1$  peak position at near zero pressure (or density), with total inclusion pressure, P<sub>T</sub> (in MPa) can be represented by

$$P_T = -0.0148 \cdot D^5 - 0.1791 \cdot D^4 - 0.8479 \cdot D^3 - 1.765 \cdot D^2 - 5.876 \cdot D$$
(5.9)

where 
$$D = v_{sample} - v_0$$
 (5.10)

Methane density,  $\rho_{CH4}$  (g/cm<sup>3</sup>), can be represented as a function of D as follows:

$$\rho_{CH_4} = -5.17331 \times 10^{-5} \cdot D^3 + 5.53081 \times 10^{-4} \cdot D^2 - 3.51387 \times 10^{-2} \cdot D$$
(5.11)

The uncertainty of *D* is estimated to be about  $0.3 \text{ cm}^{-1}$ , and therefore, the uncertainty of the calculated density of methane in vapour is about  $0.012 \text{ g/cm}^3$  and the uncertainty of the calculated inclusion pressure is  $\pm 1.34$  MPa.

From an estimate of vapour phase gas partial pressure the concentration of a dissolved gas in equilibrium with the inclusion fluid can be calculated. For a dilute solution in equilibrium with  $CO_2(g)$  the ideal gas vapour pressure of  $CO_2$  is proportional to its mole fraction in the solution The calculations utilise Henry's Law constant  $K_H$ , which relates the partial pressure of a gas  $P_i$  to its mole fraction in aqueous solution  $X_i$  according to:

$$P_i \alpha = K_H X_i \tag{5.12}$$

where  $\alpha$  is the fugacity coefficient. For any non-electrolyte solution, the fugacity of the dissolved component, *i*, becomes closer to being directly proportional to the mole fraction  $x_i$  as  $x_i$  approaches zero. Such that in solutions with low gas concentrations, the fugacity coefficient will be close to unity so that it can safely be ignored. This study uses the expression for K<sub>H</sub> (CO<sub>2</sub>) generated by Wilkinson (2001) over the temperature range 0-350°C and the salinity range 0.0-2.0 M NaCl by regression of data from the studies of Ellis and Golding (1963) and references therein.

### 5.1.3. Sample Material

65µm thick doubly polished wafers for fluid inclusion analyses were made from ten samples of Entrada Sandstone host rock and vein material collected from exposures at Tenmile Butte, outcropping in the footwall of the northern fault of Salt Wash Graben. Sections were prepared from: i) two samples of gypsum veins petrograpically associated with large-scale diagenetic bleaching of the Entrada Sandstone; ii) two samples of bleached sandstone; iii) one sample of unbleached sandstone, and; iv) five samples of aragonite veins, including samples of thick veins (>40cm thickness) and thin veins (<3mm) in bleached and unbleached host rock. Individual wafers were broken into fragments in order to enable multiple microthermometry runs from each sample.

#### 5.1.4. Analytical Methods

Six representative samples were investigated using Raman microspectroscopy. Dispersive laser-Raman spectra were obtained at the University of Cambridge by means of a LabRam 300 spectrometer equipped with a 632.81 nm diode laser, a 1200 lines/mm diffraction grating and a CCD detector. The spectrometer is attached to an Olympus microscope, with 5×, 20×, 50× and 100× objective lenses, giving a lateral resolution down to ~1  $\mu$ m.

Raman spectra were collected at room temperature in the spectral window of 100-4000 cm<sup>-1</sup> which covers the  $v_1$ -2 $v_2$  bands of CO<sub>2</sub> at 1285 cm<sup>-1</sup> and 1388 cm<sup>-1</sup> and its two hot bands at 1264 cm<sup>-1</sup> and 1409 cm<sup>-1</sup>; the N<sub>2</sub> band at 2328 cm<sup>-1</sup>; the SO<sub>2</sub> band at 1151 cm<sup>-1</sup>; the large stretching band of H<sub>2</sub>O (2900 – 3700 cm<sup>-1</sup>) and the  $v_1$  band of CH<sub>4</sub> at 2917 cm<sup>-1</sup> (Pasteris *et al.*, 1988). Overlap of Raman bands from volatiles in inclusions with bands from the mineral hosts (typically 400 – 1000 cm<sup>-1</sup>) does not usually occur.

Microthermometric measurements on fluid inclusions from two representative vein samples (one aragonite, one gypsum) were conducted at the University of Leeds using a Linkam heating-freezing stage. It was calibrated using the temperature of the CO<sub>2</sub> triple point (56.6 °C) and H<sub>2</sub>O triple point (0 °C) and the critical homogenization of an H<sub>2</sub>O fluid inclusion (374.1 °C). The accuracy of measurement is  $\pm 0.1$  °C in the range of -100 °C to +25°C,  $\pm 0.5$  °C between 25 °C and 250 °C and increases linearly to  $\pm 1$  °C at 374.1 °C. During heating, the temperature was increased at a rate of 1 to 2°C/min to minimize thermal-gradient effects. Homogenization temperatures were not corrected for pressure.

## 5.3. Results

### 5.1.5. Field Observations

At Green River bleaching of aeolian Lower to Middle Jurassic sandstones occurs to varying degrees in the footwalls of both Little Grand Fault and Salt Wash Graben (see Chapter 4, Fig. 4.4-1 for maps detailing the distribution of bleaching and sample localities). The distribution of bleaching in the footwalls of both faults is focused in the faulted fold axis of the Green River anticline (Fig. 5.3-1), though its spatial extent varies depending on the footwall lithologies. Along the more shale-rich Little Grand Wash fault footwall, bleaching is mainly confined to the lower, sand-rich sections of the Curtis Formation, with the bottom 2 m of the outcropping sandstone partially to completely bleached, while the next 4m contains sporadic, thin bleached horizons (1 to 10 cm thick) subparallel to bedding and thin bleached haloes (1 to 5cm thick) surrounding steeply-dipping fractures that are sporadically infilled with calcite or rare gypsum veins.

Along the more sand-rich rocks exposed in the footwall of the northern fault of Salt Wash Graben, the red Entrada Sandstone is extensively bleached to pale yellow-white and is especially well exposed at Tenmile Butte. The zone of bleaching, up to 8m thick, is localized to the stratigraphic base of the formation and extends up to 300m into the footwall. Above this contact, bleaching is mainly located around clusters of steeply-dipping fractures with bleached haloes up to 5 m wide, which are sporadically infilled with calcite or gypsum veins. The bleached zone is domal in structure and is coincident with the structural high formed by the anitclinal crest. The zone thins both down-dip, away from the fault trace and laterally E-W along the fault outcrop, eventually forming elongate stringers. The basal contact of the bleached zone with underlying unbleached rock is not exposed. The upper contact of the bleached zone with overlying unbleached rock is sharp, dips at a low angle over its length and terminates in bulbous fronts towards the north, east and west. It cross cuts stratigraphic boundaries and its macroscopic form is more influenced by the distance from faults and fracture conduits, than by permeability heterogeneity. Small-scale permeability heterogeneity, such as the presence of granulation seems or facies heterogeneity exerts controls on the geometry of the bleached front at the outcrop scale (Fig. 5.3-2).



Figure 5.3-1 Tenmile Butte, intersection of the apex of the Green River anticline and the northern fault of Salt Wash Graben. Field photographs showing the spectacular bleaching of the Entrada Sandstone (a-e). Bleaching is localised to a horizontally continuous 4-8m thick layer at the base of the Entrada introduced into the Entrada Sandstone, from deeper formations. Sandstone. d) The chimney structure, formed as an array of closely spaced subvertical fractures, through which the extra-formational bleaching fluid was



**Figure 5.3-2** Field photographs showing granulation seems both enhancing (a) and impeding (b) propagation of the bleaching front. Steeply dipping fractures (c-d) extend from the larger bleached zone and commonly have bleached halos that thin and terminate m's to 10m's along the fracture length. Fracture cores occasionally contain reprecipitated Fe-oxides, indicating transport of Fe in solution and multiple generations of fluid flow. Scales: Hammer: 35cm, Coin: 2.5 cm.

#### 5.1.6. Petrology and Cathodoluminescence

Bleached Entrada Sandstone samples average 6.2 vol.% feldspars and 70.8 vol.% detrital quartz grains, which are occasionally overgrown by euhedral and irregular quartz overgrowths (2.0 vol.%). Overgrowths surround both hematite and illite grain coatings and grains from which the haematitic coatings have been dissolved. Bleached sandstones samples average 2.9 vol.% illite and 1.1 vol.% kaolinite. Bleached samples average 3.3 vol.% corroded dolomite and abundant pore filling calcite (8.2 vol.%). Cryptocrystalline hematite and coarse crystalline Fe-oxides average 0.2 vol.% and 1.2 vol.% respectively. Scatter plots (Fig. 5.3-3) indicate potential paragenetic relationships between phases.



**Figure 5.3-3** Scatter plots of the point counted mineralogies for samples of bleached and unbleached Entrada Sandstone. Negatively correlated volumes of quartz overgrowths and feldspar suggests derivation of silica from the dissolution of feldspar. Negative correlated volumes of dolomite+feldspar versus calcite suggest, at least in part, derivation of some  $Ca^{2+}$  for calcite precipitation from the dissolution of these phases. Negative correlated cryptocrystalline hematite and coarse Fe-oxide volumes suggest a non-detrital origin for coarse oxides and their formation from the dissolution and reprecipitation of cryptocrystalline hematite to coarse crystalline hematite. Porosity is occluded by calcite and clay precipitation.

Dolomite is present as an early cement and is often corroded and shows evidence of patchy recrystallization. Calcite rims sand grains and overgrows dolomite cement partially filling and completely occluding pore space. Calcite has a tabular, blocky habit and individual grains range in size from (5-45µm). Two distinct calcite phases can be identified based on cathodoluminescence properties (Fig. 5.3-4): 1) an early, pigmented, bright yellow-orange luminescent calcite that rims grains and overgrows dolomite and 2) a second later calcite phase that infills remaining pore space, overgrows earlier calcite cement, and is weakly orange-red or nonluminescent. The luminosity in calcite is relatively homogeneous with no evidence or zonation. The blocky texture of the calcite and homogenous CL pattern suggests partial recrystallization.

Minor amounts of pore-filling poikilotopic barite and sylvite were observed in samples from the base of the bleached zone. Intergrowths of calcite and sylvite towards the edges of these poikiloblasts suggest contemporaneous precipitation. Extensive occurrence of barite was described by Morrison and Parry (1986) and Breit *et al.*, (1990) from areas associated with collapsed salt cored anticlines to the south east of Green River, in the vicinity of the Moab fault. Based on the sulfur isotopic composition of barite found in the Upper Jurassic Morrison Formation, Breit *et al.*, (1990) attributed barite formation to fluids originating in the underlying Pennsylvanian evaporites.

Proximal to faults, and within fractures, gypsum veins (Fig. 5.3-5) (0.5-2mm thick) grew contemporaneously with calcite. Individual gypsum veins contain inclusions of pyrite and are paralleled by occasional hematite and magnetite liesegang bands (Fig. 5.3-6). Occasional calcite veins (0.25-1mm) cross cut and are cut by gypsum veins and contain inclusions of Fe-oxides.



**Figure 5.3-4** Typical cold CL and plane polarized light photomicrographs from bleached Entrada Sandstone from the fracture conduit (Fig. 5.3-1D) feeding the bleached zone. Ubiquitous calcite cements (yellow-orange CL) are pigmented and overgrow corroded dolomite rhombs (red CL).



**Figure 5.3-5** Typical plane and crossed polarized light photomicrographs from bleached Entrada Sandstone, in Fig. 5.3-4, adjacent to a fracture filling gypsum vein. Gypsum contains inclusions of calcite and pyrite. Secondary crystalline Fe-oxides (a-b) parallel the veinlet.



**Figure 5.3-6** Typical plane and crossed polarized light photomicrographs from bleached Entrada Sandstone adjacent to a fracture filling gypsum vein showing: a) coarse hematite liesegang bands; c-e) coarse secondary hematite.



**Figure 5.3-7** SEM images from bleached Entrada Sandstone showing: a-c) corroded feldspar grains and pore filling and grain rimming illite/smectite and kaolinite; d) amalgams of kaolinite and calcite; e) extensively corroded feldspar rimmed by calcite and kaolinite and; f) coarse amalgams of kaolinite and calcite.

## 5.1.7. Scanning Electron Microscopy

Samples contain corroded K-feldspar and plagioclase overgrown by patchy coatings of illite, illite-smectite and kaolinite (Fig. 5.3-7). Corroded feldspars contain abundant clay precipitates in adjoining pore space. Occasional remnant feldspar grains have been completely replaced by

coarse pore filling illite/smectite or kaolinite. Equant and irregular quartz overgrowths are visible occasionally. Pore filling kaolinite often inter-grows with small <0.5µm euhedral calcite.

#### 5.1.8. XRD and XRF

X-ray diffraction patterns (Fig. 5.3-8) from bleached Entrada Sandstone include typical detrital minerals; quartz and K-feldspar and secondary minerals calcite, dolomite, kaolinite and mixed layer illite-smectite. Modal mineralogy (Table 5.3-1) was calculated from least squares mixing of mineral proportions to match whole rock compositions using the program MINSQ (Hermann & Berry, 2002). Recalculated modal mineral proportions are similar to those determined from point counting and exhibit similar patterns in the genetic relationships of detrital and secondary minerals. Whilst bleached sandstone is depleted in Fe ~25% of the initial Fe content remains.



Figure 5.3-8 XRD pattern from bleached Entrada Sandstone.

Sample	Туре	Qtz	Kspar	Plag	Dol	Kao	Hem	Cc	MnOx	Apt	Il	тот	SSQ
RS060	В	65.4	10.7	5.7	6.4	0.3	0.4	3.5	0.00	0.0	7.5	100.0	0.8
RS029	R	64.4	13.2	5.9	10.3	0.0	2.0	0.0	0.04	0.1	3.9	100.0	1.5

**Table 5.3-1** Modal Mineralogy of bleached (RS060) and unbleached (RS029) Entrada Sandstone recalculated from XRF analyses. Abbreviations: Qtz = Quartz, Kspar = K-feldspar, plag = plagioclase, Dol = dolomite, Cc = calcite, Kao = kaolinite, Hem = Fe<sub>2</sub>O<sub>3</sub>, MnOx = Mn-oxide, Apt = apatite, II = illite/smecite

## 5.1.9. Discussion: Petrology of Diagenetic Bleaching in the Entrada Sandstone

Hematite grain coatings are the earliest determinable diagenetic event and reddening is considered to have occurred during earliest burial. (Walker *et al.*, 1979). Petrographic

observations and XRF analyses suggest that during bleaching cryptocrystalline hematite was dissolved and reprecipitated locally as coarse hematite grains and some Fe was transported, in solution. The red colour of the Entrada Sandstone is caused by the reflectance in the red part of the visible spectrum by cryptocrystalline hematite. However, reflectance in the red part of the spectrum decreases as hematite particle size increases. With increasing size from 0.1 to 0.8  $\mu$ m, the colour progressively changes from orange to red to purple (Kerker *et al.*, 1979; Morris *et al.*, 1996). The colour of hematite changes to gray in the 5-10  $\mu$ m-size range (Lane *et al.*, 1999) so that coarse-grained hematite is black or steel gray. The colour change in bleached sandstone is a result of changes in the grain size of hematite in addition to removal of Fe from the sandstone. Cryptocrystalline hematite grain coatings are largely absent in thin sections of bleached sandstones and modal (Fig. 5.3-3) and compositional measurements (Table 5.3-1) confirm the removal of hematite and Fe in bleached samples.

In unbleached Entrada Sandstone (Chapter 4, section 4.4.2.1) illite/smectite occurs as 1-5  $\mu$ m thick pore-lining cements which generally dust entire detrital grains. Illite-smectite coating is absent or very thin at grain contacts. No detrital clay is observed in the Entrada Sandstone. Kaolinite occurs as authigenic pore filling cement which post dates dolomite cementation and is intimately associated with feldspar grains. Both these clay products are thought to represent alteration of silicate grains during burial. Volumetrically minor quartz overgrowths (<1%) were also precipitated during this episode. In bleached Entrada Sandstone reaction between volatile components in the extra-formational fluid and the host formation resulted in moderate dissolution of detrital feldspar grains and precipitation of additional grain rimming and pore-filling kaolinite and illite/smectite. This implies elevated [H<sup>+</sup>] in the bleaching fluid. Feldspar dissolution was accompanied by reprecipitation of silica as euhedral and irregular quartz overgrowths which crystallize on grains from which the hematite grain coatings have been removed. Feldspar and hematite dissolution was accompanied by calcite veining and cements which follow regional bleaching.

Calcite cement contents decreasing from ~17 vol. % close to the main feeder conduit (Fig.5.3-1D) to ~6 vol. % towards the northerly and easterly extremes of the bleached zone. Regionally the Entrada Sandstone is loosely cemented relative to the sandstones which are stratigraphyically below and above it (Ohran, 1992). Dolomite occurs as pore filling rhombs in unbleached interdunal and dune facies sandstone. Regionally, dolomite was precipitated from an isotopically heavy fluid which may have originated as evaporated playa water on the Entrada dune field (Desborough and Poole, 1992). Regionally, calcite occurs mostly as a poikilotopic cement, well developed in the extreme upper and lower parts (30-50cm) of the Entrada Sandstone but is absent elsewhere (Ohran, 1992). This calcite cement is thought to be sourced from infiltration of CaCO<sub>3</sub> bearing solutions from formations above and bellow the Entrada during

early compaction (Ohran, 1992). Extensive calcite cementation in bleached sandstones is directly related to the bleaching event, which implies that the bleaching fluid was enriched in C and had elevated [HCO<sub>3</sub><sup>-</sup>].

Localization of bleaching to the base of the formation suggests derivation from a fluid denser than the original pore fluid. The presence of gypsum veining and pore-filling poikilotopic barite and sylvite cements suggest the involvement of a saline fluid enriched in  $SO_4^{2-}$ , Cl<sup>-</sup>, Ba<sup>2+</sup> and K<sup>+</sup>.

#### 5.1.10. Isotope Geochemistry

#### 5.1.10.1. Carbon and Oxygen Stable Isotopes

Tables B-VI and B-VII (Appendix B) displays the  $\delta^{13}$ C and  $\delta^{18}$ O of samples of the bulk Entrada Sandstone (both bleached and unbleached) and calcite veins associated with bleaching. Twenty three of the samples were collected from Tenmile Butte, Salt Wash Graben, from calcite veins, bleached and unbleached Entrada Sandstone. In addition twenty samples of the Navajo Sandstone were collected from core chips from petroleum exploration wells Salt Valley 22-34 and Salt Wash #1 (well details can be found in Appendix B, Table VII) which penetrate the Navajo Sandstone on the eastern limb of the Green River anticline. In both the sampled wells the Navajo Sandstone shows a progressive colour change from very pale-white to pale yellow over the entirety of the sampled interval and only the upper 5 to 10m were unbleached and retained the original red colouration. This data is projected in Figure 5.3-9, together with published data sets from carbonate cements, veins and concretions from bleached Jurassic Sandstones in the Moab and Courthouse syncline regions of the northern Paradox Basin (Beitler *et al.*, 2005, Chan *et al.*, 2000, Eichhubl *et al.*, 2009, Garden *et al.*, 2001).

## 5.1.10.2. <sup>87</sup>Sr/<sup>86</sup>Sr

 $^{87}$ Sr/ $^{86}$ Sr of calcite veins in bleached Entrada Sandstone range from 0.712115 to 0.712645, n=2, and gypsum veins in bleached Entrada Sandstone range from 0.711837 to 0.711919, n=3. Analyses are presented in figure 5.3-10 against values for aragonite veins from the Green River anticline, the silicate fraction of the Entrada and Navajo Sandstone (Truini and Longsworth, 2003), early diagenetic cements in these formations elsewhere in the Northern Paradox Basin (Goldstein *et al.*, 2008), secondary hematite concretions associated with bleaching of the Entrada Sandstone along the Moab Fault (Chan *et al.*, 2000), analyses of barite cements in the Morrison Formation from the Slickrock Mining District (Breit *et al.*, 1990) part of a large salt collapse structure and zone of upward brine movement from the Paradox formation, and values for the Paradox formation brine from the Greater Aneth Oil Field (Spangler *et al.*, 1996).



**Figure 5.3-9** Stable isotope analyses for calcite cements and veins associated with bleached portions of the Entrada and Navajo Sandstones from this study. Included are a compilation of stable isotope analyses of calcite cements and veins associated with bleached Jurassic sandstones from the northern Paradox Basin (see text for references) and the isotopic composition of aragonite veins and modern and ancient travertine deposits associated with the leaking  $CO_2$  system.



**Figure 5.3-10** <sup>87</sup>Sr/<sup>86</sup>Sr of aragonite, calcite and gypsum veins, modern travertine and modern CO<sub>2</sub>-charged waters. Additionally the <sup>87</sup>Sr/<sup>86</sup>Sr of diagenetic carbonate cements and the silicate fraction in the Navajo and Entrada Sandstones, Paradox Formation Brine, hematite concretions from bleached Jurassic Sandstones near Moab fault and salt collapse related barite cements are shown for reference. See text for references.

## 5.1.10.3. Discussion: Isotope Geochemistry

 $\delta^{18}O_{CaCO3}$  of bleached Entrada Sandstone samples range from 19.9 to 23.6 % (V-SMOW) and  $\delta^{13}C_{CaCO3}$  values range from -1.5 to -3.9 % (V-PDB) (Fig. 5.3-9).  $\delta^{18}O_{CaCO3}$  of bleached Navajo Sandstone range from 19.2 to 22.7 % (V-SMOW) and  $\delta^{13}C_{CaCO3}$  values range from -2.2 to -3.7 % (V-PDB) (Fig. 5.3-9). Calcite cements from both bleached Entrada and Navajo Sandstones exhibit a similar range and trends in  $\delta^{13}C_{CaCO3}$  and  $\delta^{18}O_{CaCO3}$  (Fig. 5.3-11). This suggests formation of calcite from a fluid of comparable isotopic composition at similar temperatures and implies that carbonate deposition occurred from a fluid migrating vertically through the stratigraphy.

 $\delta^{18}O_{H2O}$  calculated from  $\delta^{18}O_{CaCO3}$  (Fig. 5.3-11) (using the crystallization temperatures determined in section 5.1.13) of bleaching related cements in both Entrada and Navajo Sandstone is isotopically similar to that of carbonate associated with the modern CO<sub>2</sub>-system, but is heavier than calcite cements associated with bleaching in the wider Paradox Basin area (determined from various crystallizations temperatures reported in Beitler et al., (2005), Chan et al., (2000) and Garden et al., (2001), ranging from ~30-80°C) (Fig. 5.3-11). Bleaching related waters elsewhere in the Paradox basin have been variably attributed to fluids of a largely meteoric origin (Beitler et al., 2005, Eichhubl et al., 2009, Garden et al., 2001) or to mixtures of meteoric water and saline fluids derived from the Pennsylvanian evaporite formations (Chan et al., 2000). The 3.7 to 3.8 % variation in  $\delta^{18}$ O observed here would imply an ~20°C variation in temperature over the course of precipitation if carbonate formed from an invariant, unfractionated fluid source. This range of temperature during deposition of calcite is unlikely. Additionally, the correlated trends in  $\delta^{13}C$ and  $\delta^{18}$ O does not follow that predicted for isotopic variation due to varying precipitation temperatures. The heavy  $\delta^{18}$ O implies precipitation from a fluid enriched in <sup>18</sup>O. This is interpreted as reflecting precipitation from a fluid composed of a mixture of meteoric water and saline fluid derived from Pennsylvanian evaporite formations, but containing higher contributions of brine than observed elsewhere in the Paradox Basin.

<sup>87</sup>Sr/<sup>86</sup>Sr of calcite and gypsum veins is radiogenic, and significantly more so than bleaching related hematite concretions from the Moab fault region (Chan *et al.*, 2000), Paradox Formation brines (Spangler *et al.*, 1996) or diagenetic cements origination from extremely brine enriched fluids (Breit *et al.*, 1990) (Fig. 5.3-10). <sup>87</sup>Sr/<sup>86</sup>Sr is close to, but marginally less radiogenic than, carbonate cements associated with the ancient CO<sub>2</sub> system but overlaps with the range in <sup>87</sup>Sr/<sup>86</sup>Sr observed in modern CO<sub>2</sub>-charged waters. The radiogenic <sup>87</sup>Sr/<sup>86</sup>Sr suggests significant contributions of <sup>87</sup>Sr suggesting the role of a reactive fluid, enriched in H<sup>+</sup>, capable of dissolving significant quantities of silicate minerals in the host aquifer.

 $\delta^{13}$ C of bulk rock bleached samples is on average ~5% lighter than the average  $\delta^{13}$ C of carbonate cements associated with ancient travertines (Fig. 5.3-9). The analysed  $\delta^{13}$ C and  $\delta^{18}$ O will be a mechanical mixture of all carbonate phases present in the sample during powdering.



**Figure 5.3-11**  $\delta^{18}O_{H2O}$  and  $\delta^{13}C_{HCO3}$  calculated from the isotopic composition of bleached Entrada and Navajo Sandstone samples using crystallization temperatures determined in section 5.1.13, uncorrected for dolomite.

The linear correlation in  $\delta^{13}$ C and  $\delta^{18}$ O passes through the composition of samples that contain only sabkha dolomite cements suggesting that the array in  $\delta^{13}$ C and  $\delta^{18}$ O represents a mixing line between this and an isotopically heavy carbon/oxygen source (Fig. 5.3-9). Dolomite formed at low temperatures (e.g. 25°C) typically should be enriched in <sup>18</sup>O by 5-7‰ compared to coexisting calcite (Clark and Fritz, 1997). Therefore the observed isotopic difference between early dolomite and later bleaching related calcite indicates that they were precipitated from different fluids. Due to the mixing of cements during sample preparation, the actual value of  $\delta^{13}$ C and  $\delta^{18}$ O of the calcite cements will be heavier than the bulk values measured. Recalculation of the precise  $\delta^{13}$ C and  $\delta^{18}$ O of individual samples is difficult without having bulk rock chemical analyses for each sample. However, point counted estimates suggest that between 30 to 70% of the C in individual bleached samples is derived from early dolomite cements. This implies that the average  $\delta^{13}$ C of measured calcite is between -1.7‰ and +1.8‰ as apposed to the average measured bulk rock value of -2.5‰.

Secondary carbonate minerals forming in the presence of a precursor carbonate phase will derive <sup>13</sup>C and <sup>12</sup>C from the partial recrystallization of the precursor and from the addition of C from the pore fluid  $HCO_3^-$  reservoir. Carbonate volumes (up to ~ 20 vol. %) significantly in excess of those observed in samples containing only early diagenetic



**Figure 5.3-12**  $\delta^{13}$ C of CO<sub>2</sub>(g) and fluid from the modern CO<sub>2</sub> charged waters, carbonate cements in largescale bleached zones, ancient and modern travertine and aragonite veins compare to the range of  $\delta^{13}$ C in various geological environments and substances.

cements (up to ~10 vol. %) suggests significant addition of  $HCO_3^-$  from an external C reservoir. These distinct C sources are interpreted as being dolomite cement, observed in unaltered samples of both sandstones, related to early diagenetic sabkha deposits and an isotopically heavy source of C and O related to the bleaching fluid.

In this instance likely extra-formational carbon sources, for carbonate cementation during sediment exhumation, include bicarbonate produced from the transformation of organic matter during hydrocarbon generation (Battani *et al.*, 2000; Butala *et al.*, 2000), or geogenic CO<sub>2</sub> sourced from decarbonation reactions involving clay–carbonate mineral diagenetic reactions in deeper formations (Chapter 2, section 2.4.3). Calcite precipitated from the breakdown of hydrocarbon has  $\delta^{13}C_{CaCO3}$  values as low as -20% (Tucker and Wright, 1996; Wood and Boles, 1991) and are typically in the range -20 to -10%. Diagenetic and metamorphic CO<sub>2</sub> would have about the same  $\delta^{13}C_{CO2(g)}$  as the carbonate mineral source because fractionation is only about ~1% at 150°C (Friedman and O'Neil, 1977). It is therefore unlikely, but not impossible, that this <sup>13</sup>C enriched HCO<sub>3</sub><sup>-</sup> arose from hydrocarbon breakdown. Early  $\delta^{13}C_{HCO3}$  in the ancient CO<sub>2</sub> system

was certainly as light as 1% $_{0}$  (Chapter 4, section 4.4.8), may have had values as low as -0.7 $%_{0}$  (Chapter 4, section 4.4.9) and has certainly evolved from lighter to heavier  $\delta^{13}C_{HCO3}$  through time.  $\delta^{13}C_{HCO3}$  calculated from the  $\delta^{13}C_{CaCO3}$ , corrected for C derived from dolomite, for samples from which point count estimates of dolomite/calcite is available, have values between ~ -3.52 to - 0.56 $%_{0}$ . Which is lighter than the  $\delta^{13}C_{HCO3}$  in modern and ancient CO<sub>2</sub> systems, but not only moderately so. The heavy  $\delta^{13}C$  may therefore have arisen from crustally sourced, unfractionated CO<sub>2</sub> and/or from a mixture of CO<sub>2</sub> and a lighter, hydrocarbon C source, although this cannot be conclusively confirmed from C-isotopes alone.

#### 5.1.11. Fluid Inclusion Petrography

Fluid inclusions examined in this study occur in aragonite, calcite, gypsum, and in quartz overgrowths surrounding detrital quartz grains. Most of the fluid inclusions examined in this study are found in aragonite (Fig. 5.3-13) and gypsum (Fig. 5.3-14) crystals and in healed microfractures within, and quartz overgrowths surrounding, detrital quartz grains (Fig. 5.3-15). Only quartz overgrowths possessing a clear petrographic link to, and contemporaneous timing with, the overall diagenetic assemblage and event of interest were analysed. Petrographic criteria for the acceptance of a genetic link between quartz overgrowth and other diagenetic phases include i) the observation of intergrowths or solid inclusions of the other diagenetic phases of interest within quartz ii) a consistent vapour/liquid ratio between inclusions in overgrowths and other cements. Necking-down or stretching textures were observed and avoided. Primary and secondary inclusions were distinguished by their relationships to crystallographic surfaces and microfractures, respectively.

Primary inclusions within aragonite crystals (Fig. 5.3-13) are typically small (1-5 $\mu$ m), single or two phase (aqueous liquid ± vapour), ovoid and occur in dense clusters along growth and cleavage planes (A1 type) (e.g. Fig. 5.3-13A-F). Larger type A1 inclusions (10-20  $\mu$ m) typically have a subhedral to euhedral negative crystal shape (e.g. Fig. 5.3-13F). Primary fluid inclusions in aragonite also occur at impinging crystal boundaries (type A2), where they typically trap both aqueous and hydrocarbon liquids (e.g Fig. 5.3-13B,E,F) and occur as single (aqueous or hydrocarbon), two (aqueous and/or hydrocarbon and/or vapour) or three phase inclusions (aqueous, liquid hydrocarbon and vapour). Curviplanar arrays of secondary fluid inclusions also occur along healed microfractures (A3 type) (e.g. Fig. 5.3-13B,C).

Gypsum crystals (Fig. 5.3-14) contain a variety of primary inclusion types, ranging from clusters of small equant inclusions (1-5µm) along growth and cleavage planes (type G1), to larger irregular inclusions (8-20µm) along growth planes and between impinging crystal boundaries (type G2).



Figure 5.3-13 Photomicrographs illustrating the various primary and secondary fluid inclusions types observed in aragonite crystals from vein and matrix samples of the Entrada Sandstone, Salt Wash graben, Green River.



**Figure 5.3-14.** Photomicrographs illustrating the various primary and secondary fluid inclusions types observed in gypsum crystals from vein samples of the Entrada Sandstone, Salt Wash graben, Green River.



**Figure 5.3-15.** Photomicrographs illustrating the various primary and secondary fluid inclusions types observed in quartz crystals from vein and matrix samples of the Entrada Sandstone, Salt Wash graben, Green River.

Small (2-8 $\mu$ m), primary fluid inclusions within quartz overgrowths (Fig. 5.3-15) are found on the boundary between detrital grains and overgrowths (type Q1) and, less commonly, within the overgrowths themselves (type Q2). Most primary fluid inclusions show a subhedral to euhedral negative crystal shape. Curviplanar arrays of small (2-6  $\mu$ m), secondary fluid inclusions also occur along healed microfractures (Q3 type).

#### 5.1.12. Raman Spectroscopy

The optical properties of fluid inclusions that are 'ideal' for Raman analysis are the same as those that are desirable for microthermometric analysis, i.e., high optical clarity, sufficient size (> 5  $\mu$ m desirable), and shallow depth below the sample surface. The chosen inclusions are generally between 2 to 15  $\mu$ m in size. They occur in clusters or have an isolated occurrence. All the fluid inclusions which were examined by LRM spectroscopy contain two phases, liquid and vapour at room temperature. The vapour phase volume ranges from ~ 2 to ~ 15 %. Inclusions sufficiently large to allow reliable LRM analysis on their vapour bubbles proved difficult to find. Due to the small size of inclusions in carbonate minerals and the turbidity of the host, targeting these inclusions for LRM is highly problematic. Due to the close proximity to the homogenization temperature, vibration and Brownian motion of vapour bubbles makes them difficult to target with the laser: movement of vapour bubbles would lead to distorted spectra, with enhanced bands of the volatiles when the bubbles are on target and subdued bands when the bubbles moved off the laser beam.

Over 120 fluid inclusions were examined by LRM in this study.  $CO_2$  and  $CH_4$  were detected as volatiles. It was found that the volatile content varies strongly in these inclusions: some show moderate intensities for the H<sub>2</sub>O,  $CO_2$  or  $CH_4$  bands, while others show only weak or no signal. The vast majority of the fluid inclusions analysed contained only H<sub>2</sub>O and no other volatile components were detected. This is either because the vapour bubble was not accurately targeted; the volatile content was below the detection limit of the apparatus or the inclusion was devoid of volatile material.

 $CO_2$  was identified in eight fluid inclusions.  $CO_2$  and  $CH_4$  were found to coexist in three. The compositions of volatile species of these fluid inclusions are displayed in Table 5.2. As Fig. 5.3-16 shows, the  $CO_2$  bands can be easily resolved against the bands of the host mineral. Superposition of the two  $v_1$ - $2v_2$  bands of  $CO_2$  on the broad but low quartz bands can be clearly resolved. No other volatiles were found in this fluid inclusion, indicating that the inclusion primarily contains water vapour and  $CO_2$ .

Three inclusions were found to contain  $CH_4$  as a coexisting species. In the vapour phase spectrum (Fig. 5.3-18), for example, the  $CH_4$  band at 2916.5 cm<sup>-1</sup> is present together with the two  $v_1$ - $2v_2$  bands of CO<sub>2</sub>, highlighting the presence of both CO<sub>2</sub> and  $CH_4$ . The results of the calculations of gas composition, CO<sub>2</sub> and  $CH_4$  gas density, inclusion pressure and formation depth and the dissolved content of CO<sub>2</sub> and  $CH_4$  in the inclusion fluid are presented in Table 5.2. Peak areas used to calculate gas composition where determined from Raman spectra, after baseline correction, using a Gaussian curve fitting algorithm in Origin Pro (version 7.0, OriginLab Corporation, Northampton, MA).



**Figure 5.3-16.** Raman spectra of the host and the vapour phase of a fluid inclusion in a quartz overgrowth associated with an aragonite bearing sample from the feeder zone of an ancient travertine deposit in the Entrada sandstone, Salt Wash Graben, Green River. The main  $v_1$ -2 $v_2$  peak of CO<sub>2</sub> is visible at 1389.40 cm-1. The broad peak 3100-3700 cm<sup>-1</sup> corresponds to a weak  $v_1$  vibration of H<sub>2</sub>O vapour.



**Figure 5.3-17.** Close up of the region 1200-1800 cm<sup>-1</sup> for the Raman spectra of the host and the vapour phase of a fluid inclusion in a quartz overgrowth associated with an aragonite bearing sample from the feeder zone of an ancient travertine deposit, Salt Wash Graben, Green River. The upper and lower  $v_1$ - $2v_2$  peaks of CO<sub>2</sub> are visible at 1389.40 and 1286.60 cm<sup>-1</sup> respectively.



**Figure 5.3-18.** Raman spectra of the host and the vapour phase of a fluid inclusion in a quartz overgrowth associated with gypsum in a sample from a bleached zone in the Entrada Sandstone, Salt Wash Graben, Green River. The main  $v_1$ - $2v_2$  peak of CO<sub>2</sub> is visible at 1388.92 cm<sup>-1</sup>. The  $v_1$  peak of CH<sub>4</sub> is visible at 2916.5 cm<sup>-1</sup>.



**Figure 5.3-19.** Close up of the region 1200-1800 cm<sup>-1</sup> for the Raman spectra of the host and the vapour phase of a fluid inclusion in a quartz overgrowth associated with gypsum in a sample from a bleached zone in the Entrada Sandstone, Salt Wash Graben, Green River. The upper and lower  $v_1$ - $2v_2$  peaks of CO<sub>2</sub> are visible at 1388.92 and 1286.03 cm<sup>-1</sup> respectively.



**Figure 5.3-20.** Close up of the region 2825-3000 cm<sup>-1</sup> for the Raman spectra of the host and the vapour phase of a fluid inclusion in a quartz overgrowth associated with gypsum in a sample from a bleached zone in the Entrada Sandstone, Salt Wash Graben, Green River. The  $v_1$  peak of CH4 is visible at 2916.5 cm<sup>-1</sup>.

#### **5.1.13.** Microthermometry

 $T_m$  and  $T_h$  of analysed fluid inclusions are displayed in Figs. 5.3-21 and 5.3-22. Fig. 5.3-23 shows  $T_h$  and  $T_m$  for those fluid inclusions from which both quantities could be analysed. The salinity (in terms of total weight % Na, K, Ca, Mg, Cl, SO<sub>4</sub> and HCO<sub>3</sub>) and the emanation temperature of modern CO<sub>2</sub>-spring fluids are included in these figures for comparison. Due to the turbidity of both minerals visual determination of melting point temperature was problematic and  $T_m$  could only be determined for ~1/3 of inclusions examined. The majority of inclusions examined possessed or nucleated a gas bubble upon cooling. Homogenization temperatures where measured on inclusions upon heating, following melting point determination.

Homogenization temperatures and salinity estimates for the two specimens examined fall into distinct clusters (Fig. 5.3-23). Fluid salinities (1.31-2.82 wt% salt) and homogenisation temperatures (16.1-17.5 °C) for inclusions in aragonite (n = 12) lie within the range of salinity (0.38-1.90 wt% salt) and temperatures (14.7-27.0 °C) of modern CO<sub>2</sub>-charged fluids at Green River (n = 10). Fluid salinities (2.49-6.95 wt% salt) and homogenisation temperatures (22.1-27.1 °C) for inclusions in gypsum (n = 25) formed from more saline fluid, at moderately higher formation temperatures.



**Figure 5.3-21.** Fluid salinities, estimated from last ice melting temperatures  $(T_m)$ , for primary aqueous inclusions in aragonite and gypsum veins from the Entrada Sandstone, Salt Wash Graben, Green River. The salinities of modern CO2-charged fluids are included for comparison.



**Figure 5.3-22.** Homogenization temperatures  $(T_h)$  of primary aqueous inclusion in aragonite and gypsum veins from the Entrada Sandstone, Salt Wash Graben, Green River. The emanation temperatures of modern CO<sub>2</sub>-charged fluids are included for comparison.



**Figure 5.3-23.** Fluid salinities versus homogenization temperatures of primary aqueous inclusion in aragonite and gypsum veins from the Entrada Sandstone, Salt Wash Graben, Green River.

# 5.4. Discussion: Fluid Inclusion Petrology

Aragonite crystals and associated quartz overgrowths contain: i) primary single phase aqueous inclusion of moderate salinity (1.31-2.82 wt% salt); ii) primary two phase inclusions of saline fluid and both pure CO<sub>2</sub> (100 mol% CO<sub>2</sub>) and a single inclusion with mixed CO<sub>2</sub> and CH<sub>4</sub> vapour (92 mol% CO<sub>2</sub>, 8 mol% CH<sub>4</sub>) and; iii) primary inclusions of liquid hydrocarbon, aqueous fluid and vapour (vapour composition could not be determined with LRM due to the fluorescence of the hydrocarbon phase). Homogenisation temperatures (16.1-17.5 °C) and vapour phase densities (0.01-0.05  $\pm 0.02$  g/cm<sup>3</sup>) attest to inclusion at low pressures (0.41-2.49  $\pm 1.03$  MPa) at shallow burial depths (29-221  $\pm 97$  m) during the most recent periods of basin exhumation. Fluid salinities, entrapment temperatures and dissolved CO<sub>2</sub> concentrations (0.06-0.88  $\pm 0.33$  mol/l) for these fluid inclusions fall with the ranges of those quantities observed in the modern CO<sub>2</sub>-charged fluids at Green River. This suggests that aragonite and its associated alteration textures formed from a fluid of composition similar to that of the modern CO<sub>2</sub>-charged fluids. The brine content of this fluid, based on the measured salinities of the inclusions, would have been within the range of those observed in the modern CO<sub>2</sub>-charged fluids or ~1 wt% more saline.

 $CO_2$  was only observed in the vapour phase of a small number of the actual inclusions examined in aragonite bearing samples (4 out of 52 examined). This is thought to be due to difficulties in accurately targeting the vapour phase, the small size of the vapour bubble (typically <1.5 µm) and the very close proximity of the  $CO_2$  concentrations to the theoretical detection limit of LRM.

Gypsum crystals and associated quartz overgrowths examined in this fluid inclusion study are petrologically associated with large-scale diagenetic bleaching of the Entrada Sandstone at the crest of the Green River anticline. Gypsum crystals and associated quartz overgrowths contain: i) primary single phase aqueous inclusion of high salinity (2.49-6.95 wt% salt); ii) primary two phase inclusions of saline fluid and both pure CO<sub>2</sub> (100 mol% CO<sub>2</sub>) and mixed CO<sub>2</sub> and CH<sub>4</sub> vapour (88-73 mol% CO<sub>2</sub>, 11-27 mol% CH<sub>4</sub>) and; iii) primary inclusions of liquid hydrocarbon, aqueous fluid and vapour (vapour composition could not be determined with LRM due to the fluorescence of the hydrocarbon phase). Homogenisation temperatures (22.1-27.1 °C) and vapour phase densities (0.04-0.09  $\pm 0.02$  g/cm<sup>3</sup>) attest to inclusions formed in aragonite associated samples. Based on burial curves for the Entrada Sandstone in the area surrounding Green River (Nuccio and Condon, 1996), modified for local variations in burial depth due to the structural high formed by the Green River anticline, the interval from which these samples were taken passed through the burial depth range 200-400  $\pm 97$  m between 2.1-5.5  $\pm 1.5$  Ma (Fig 5.4-1).

Fluid salinities, entrapment temperatures and formation pressures suggest that gypsum and the large-scale diagenetic bleaching formed during the latest stages of basin exhumation from a saline fluid enriched in brines derived from the Pennsylvanian evaporite formations. In a plot of homogenization temperature versus fluid salinity (Fig. 5.3-23) values for the two sets of examined fluid inclusions fall along an approximately linear array of increasing fluid salinity with increasing entrapment temperature. Possible explanations for this apparent correlation included i) the transport of 'hot' brine into the Entrada Sandstone ii) a correlation between pore fluid salinity and temperature where increasing temperatures reflect higher burial depths and fluid inclusions of greater age. Given that fluids passively migrating along faults are likely to loose heat through thermal conduction it seems unlikely that basinal brines would carry significant heat into shallower formations. Thus, increasing salinity with increasing entrapment temperature most likely records a decrease in the proportion of Paradox formation brine entering the Entrada sandstone with time.




A number of single, two and three phase hydrocarbon bearing primary fluid inclusions were observed in all the sample types analyzed.  $CH_4$  is present in the vapour phase of three of the primary fluid inclusions; two in gypsum (17-21 mol%  $CH_4$ ), and one in aragonite (8 mol%  $CH_4$ ).  $CH_4$  may have been derived from: i) dissolved or free phase gas migrating with the  $CO_2$ /brine mixture entering the Entrada Sandstone; ii) exsolved from a liquid hydrocarbon phase that entered the Entrada Sandstone during deep burial; iii) exsolved from a liquid hydrocarbon phase that migrated along with the  $CO_2$ /brine mixture; iv) the reduction of  $CO_2$  to form  $CH_4$  via the reaction:

$$CO_2 + 4H_2 = CH_4 + 2H_2O (5.13)$$

However, this reaction requires elevated temperatures and redox conditions improbable in shallow diagenetic systems (Berndt *et al.*, 1996; Horita and Berndt 1999; McCollom and Seewald 2001). Migration of both liquid hydrocarbons and  $CH_4$ , along with a  $CO_2$  bearing free gas phase or  $CO_2$ -saturated brine, would be aided by the high solubility of  $CO_2$  in hydrocarbon liquids (e.g. Dehima *et al.*, 1999) and the resulting reduction in oil viscosity: a process akin to natural enhanced oil recovery. Gypsum bearing samples contain a higher proportion of  $CH_4$  bearing inclusions, and the vapour phase of these inclusions contains a higher proportion of  $CH_4$  relative to  $CO_2$  than does the aragonite bearing samples (only a single  $CH_4$  bearing inclusion was observed in aragonite, with low mol%  $CH_4$  relative to  $CO_2$ ). This general trend of apparently decreasing  $CH_4$  content with time may reflect a flushing of the hydrological system, with hydrocarbon liquids and  $CH_4$  being stripped from the system by  $CO_2$  rich fluids and gases.

CH<sub>4</sub> would be a suitable redox agent for the reduction of Fe<sup>3+</sup> and dissolution of hematite. However, CH<sub>4</sub> was not observed in all the volatile bearing inclusions, the rest contained only CO<sub>2</sub> and CO<sub>2</sub> is the dominant volatile phase in all volatile bearing inclusions. Reductive dissolution of hematite would be enhanced by pH suppression at high pCO<sub>2</sub> and by the overall availability of H<sup>+</sup> (e.g. Cornell and Giovanoli, 1993). Kinetically rapid dissolution of hematite may explain the sharp nature of the contact between bleached and unbleached sandstone (e.g. Fig. 5.3-2). Additionally, isotopically light HCO<sub>3</sub><sup>-</sup> derived from the break down of CH<sub>4</sub>, mixed with isotopically heavy HCO<sub>3</sub><sup>-</sup> derived from crustally sourced CO<sub>2</sub> may explain measured values of  $\delta^{13}C_{CaCO3}$  lighter than those observed in the young leaking CO<sub>2</sub> system (section 5.1.10.3).

The paragenesis of the Entrada Sandstone is presented in figure 5.4-2, which shows the relative timing and duration of diagenisis observed in this study to regional diagenetic episodes and to local and regional geological events. Detrital fragments of locally derived pisolites and travertine have recently been discovered in the fluvial Lower Cretaceous Yellow Cat Member of the Cedar Mountain Formation, at Crystal Geyser Dinosaur Quarry, near Crystal Geyser (Suarez *et al.*, 2007a, 2007b). The similar morphology and mineralogy of these fragments to actively forming travertine at Crystal Geyser led those authors to attributed their formation to CO<sub>2</sub>-

charged springs. Additionally, extensive carbonate, Fe-oxide, and silicate alteration, including chemical bleaching of the sediment, at the Temple Mountain uranium district, on the edge of the San Rafael Swell have been attributed to  $CO_2$ -charged fluids and dated at ~13Ma (Morrison and Parry, 1988). These finding suggests that  $CO_2$ -charged fluids have been leaking from local Green River area for considerably longer periods than is evident from persevered surface travertine deposits and that  $CO_2$ -hosting paleo-reservoirs could be expected in now exhumed sandstone formations.



**Figure 5.4-2** Paragenesis of the Entrada Sandstone in the vicinity of Green River Interpreted paragenetic relationships of diagenetic alteration and associated geological events constructed from age data of Beitler *et al.*, 2005; Condon, 1997; Dockrill, 2005; Doelling *et al.*, 1988; Morrison and Parry, 1988; McKnight, 1940; Nuccio and Condon, 1996; Suarez *et al.*, 2007a.

## 5.5. Conclusions

Mineral assemblages in samples from travertine feeder systems contain low salinity aqueous single and two phase primary fluid inclusions and single, two and three phase hydrocarbon bearing primary fluid inclusions. The aqueous fluid contained in these inclusions was trapped at a comparable temperature to, and is of salinity similar to that of modern  $CO_2$  charged fluids escaping along normal faults of the Salt Wash Graben and Little Grand Fault systems. Vapour densities, inclusions pressures and homogenisation temperatures suggest these inclusions formed within the most recent periods of basin exhumation at very shallow burial depths (<200 m). The  $CO_2$  content of these fluid inclusions is similar to that of the modern fluid but ranges to higher concentrations. This may represent the trapping of less  $CO_2$ -degassed fluid than that which is seem escaping to the surface today. A single inclusion was observed to contain a low concentration of  $CH_4$  suggesting the intermittent presence of  $CH_4$  in the  $CO_2$ -rich gas phase associated with travertine formation.

Mineral assemblages in samples from zones of extensive  $Fe^{3+}$  bleaching in the Entrada Sandstone contain primary fluid inclusions of moderately saline aqueous fluid, CO<sub>2</sub> and CH<sub>4</sub> vapour and occasional liquid hydrocarbon bearing two and three phase primary inclusions. Vapour densities, inclusion pressures and homogenisation temperatures attest to the formation of these inclusions at shallow burial depth, during basin exhumation, in the last 2.1-5.5 ±1.5 Ma. Fluid salinities are higher than those observed in modern fluid at Green River which suggests an increased component of Paradox formation brine in these older entrapped fluids in agreement with petrological observations and isotopic evidence presented in section 5.1.10.3. The presence of a CO<sub>2</sub> rich vapour phase with moderate quantities of CH<sub>4</sub> is attributed to mobilization of hydrocarbons and CH<sub>4</sub> by migrating CO<sub>2</sub> bearing fluids and gases. The CH<sub>4</sub> dissolved in this fluid would be a suitable redox agent for the reduction of Fe<sup>3+</sup> to Fe<sup>2+</sup>, and the high concentrations of CO<sub>2</sub> would significantly enhance the solubility and dissolution rate of hematite by lowering pH and increasing the availability of H<sup>+</sup>.

Sample	Туре	Host Mineral	Gas Composition	$\Delta v_1 - 2v_2$	$\rho_{\rm CO2}$	P <sub>CO2</sub>	Depth	$\nu_1$	Рсн4	P <sub>T</sub>	Depth	Dissolved CO <sub>2</sub>	Dissolved CH <sub>4</sub>
					(g/cm3)	(MPa)	(m)		(g/cm3)	(MPa)	(m)	(mol/l)	(mol/l)
RS073	В	Quartz	CO2 (73%), CH4 (27%)	102.89	0.04	2.28	202	2916.50	0.028	3.94	356	1.05	0.36
RS061	В	Gypsum	CO2 (89%), CH4 (11%)	102.90	0.09	4.56	413	2916.49	0.029	3.98	360	1.30	0.15
RS066	В	Gypsum	CO2 (100%)	102.84	0.06	3.32	298					1.18	
RS061	В	Quartz	CO2 (100%)	102.81	0.05	2.74	244					0.97	
RS069	Y-B	Quartz	CO2 (100%)	102.75	0.03	1.45	125					0.14	
RS069	Y-B	Quartz	CO2 (100%)	102.72	0.02	0.83	67					0.29	
RS069	Y-B	Aragonite	CO2 (100%)	102.80	0.05	2.49	221					0.88	
RS069	Y-B	Quartz	CO2 (92%), CH4 (8%)	102.70	0.01	0.41	29	2917.27	0.001	0.17	7	0.06	0.005

**Table 5.5-1** Details of the gas composition, gas densities, inclusions pressures, formation depths for the vapour phase of primary fluid inclusions in vein and matrix samples associated with large-scale diagenetic bleaching (B) and bleaching in ancient travertine feeder systems (Y-B) in the Entrada Sandstone, Salt Wash Graben, Green River.

# **Chapter 6**

# **Discussion and Conclusions**

Understanding the geochemical behaviour of anthropogenic carbon dioxide stored in geological reservoirs, over a range of time-scales, is crucial for quantifying the risk of leakage and the evolution of the sequestered form of that  $CO_2$  through the life of an individual storage site. Prediction of the long-term fate of this carbon dioxide requires determination of the relevant gasfluid-mineral reactions and their chemical kinetics (e.g. Xu et al., 2004). These gas-fluid-mineral reactions may act either to increase the stability of stored  $CO_2$  by precipitating carbonate minerals or enhance leakage by corroding well cements, existing boreholes, cap rocks and fault seals. Modelling the progress of such reactions is frustrated by uncertainties in the absolute mineral surface reaction rates and the significance of other rate-limiting steps in natural systems (see White and Brantley, 2003 for a complete review). It is well established that silicate dissolution rates in the natural environment are typically 2 to 5 orders of magnitude slower than, far-fromequilibrium, laboratory-derived rates at similar pH and temperature conditions (White and Brantley, 2003), and the laboratory rates are typically the only rates available for simulations (e.g. Knauss et al., 2005; White et al., 2005; Xu et al., 2004). Quantification of the kinetics of fluidmineral reactions in natural systems, rich in  $CO_2$ , is thus required for the accurate prediction of the long-term performance of geological storage sites.

This thesis uses the chemical evolution of groundwater from the Jurassic Navajo Sandstone, part of a leaking natural accumulation of  $CO_2$  at Green River, Utah, in the Colorado Plateau, USA, to place constraints on the rates and potential controlling mechanisms of the mineral-fluid reactions, under elevated  $CO_2$  pressures, in a natural system. Surface carbonate deposits and cementation within the footwall of the local fault systems record multiple injections of  $CO_2$  into the Navajo Aquifer and leakage of  $CO_2$  from the site over ca. 400,000 years. Geochemical and petrological methods are employed to examine the mineralogical consequences of this fluid-mineral interaction. The stable and radiogenic isotopic composition of these deposits are examined and used to interpret the physical and chemical processes controlling the long-term leakage of  $CO_2$  from the underlying Navajo Aquifer. Additionally, large scale zones of mineralization and mineralogical alteration in the overlying Entrada Sandstone are examined; the role of  $CO_2$  and other volatile phases (e.g.  $CH_4$ ,  $H_2S$ , organic acids) in the production of this alteration is investigated using petrographic techniques and the analysis of volatile bearing, mineral hosted fluid inclusions. The key findings of this thesis are summarized below.

## 6.1. Carbon Storage Site Analogue, Green River, Utah

#### 6.1.1. Summary of the CO<sub>2</sub>-charged Groundwater Hydrogeochemistry

Crustally sourced CO<sub>2</sub>, produced from diagenetic reactions in the Leadville Limestone, at depth within the Paradox Basin, migrates vertically through the stratigraphy mixing with and dissolving into basinal brines of the Paradox Formation. These CO<sub>2</sub>-charged brines migrate along the Little Grand and Salt Wash fault systems into the shallow White Rim and Navajo Aquifers where they mix with meteorically derived groundwaters, flowing along hydraulic gradients from zones of recharge in the San Rafael Swell to zones of discharge near the confluence of the Green and Colorado Rivers. This passive migration of CO<sub>2</sub> is analogous to leakage of a deep geological CO<sub>2</sub> reservoir into shallower aquifer systems. CO<sub>2</sub> leaks to the surface through the fault damage zone of the Little Grand and Salt Wash fault systems and through a number of abandoned petroleum exploration wells.

Time-series analysis of the fluid isogeochemistry from the largest of these leakage sites, Crystal Geyser, has provided important insights into the plumbing of fault leakage and the role of CO<sub>2</sub>-driven cold water geysering in stimulating and enhancing CO<sub>2</sub> leakage rates. Cold water geysering of Crystal Geyser, driven by CO<sub>2</sub>-degassing, causes pressure depletion in the Navajo Aquifer. This stimulates influx of CO<sub>2</sub>-charged brines from deeper formations, most likely from the White Rim Sandstone, on the time-scale of the geysering events, which mix with chemically distinct fluids in the host aquifer. The physical process of CO<sub>2</sub> gas-driven geysering is therefore an important mechanism for the stimulation of vertical fluid and gas migration in the subsurface and will be important for prolonging effusion from leaking wells in CO<sub>2</sub> storage sites. Estimates of the average annual CO<sub>2</sub> emissions from Crystal Geyser range from 5694  $\pm$  1708 t/a to 12702  $\pm$ 3810 t/a. Combining these with estimates of the annual fluid flux results in average CO<sub>2</sub> concentrations of ~4 to 10 mol L<sup>-1</sup>, greatly exceeding the maximum solubility of CO<sub>2</sub> in the Navajo Aquifer. This strongly implies that CO<sub>2</sub>, in addition to brine, is imbibed through the Little Grand fault as a consequence of the geysering process and is added to the Navajo Aquifer close to the site of Crystal Geyser.

 $CO_2$  entering the Navajo Sandstone groundwater system dissolves into the formation water, suppressing pH and mineral saturation in the fluid promoting dissolution of silicate and carbonate minerals in the host aquifer. The introduction of this  $CO_2$  increases the fluids capacity to accept dissolved solids by lowering the pH and the saturation state of the groundwater, enhancing mineral dissolution. As a result, the  $CO_2$ -rich groundwaters evolve towards very high solute concentrations after prolonged water-rock interaction. In geological  $CO_2$  storage sites this processes will ultimately enhance the fluids capacity to accept dissolved  $CO_2$ , through ionic complexation, thereby enhancing solubility trapping.

The groundwater chemistry is controlled by a mix of kinetically rapid, equilibrated mineralfluid reactions and disequilibrated reactions where the mineral surface dissolution kinetics are slow or the saturation state of the reacting phase is controlled by an additional rate limiting step. The dominant controlling reactions are the dissolution of plagioclase (An38) and K-feldspar which result in increasing concentrations of Na<sup>+</sup>, K<sup>+</sup> and Al<sup>3+</sup> as the groundwaters evolve. These phases, in addition to quartz, dominate the mineralogy of the Navajo Sandstone. With progressive flow through the aquifer, feldspar hydrolysis reactions consume H<sup>+</sup> and liberate solutes to solution which increase mineral saturation in the fluid. The concentration of dissolved silica, derived from the dissolution of silicate minerals, is controlled by equilibrium with an amorphous silica phase. Kaolinite and smectite are the dominant stable clay minerals and reaction products of feldspar dissolution. Equilibrium with silica maintains most groundwater samples within the kaolinite stability field. Because  $aSiO_2(aq)$  is fixed by the precipitation of an amorphous silica phase, kaolinite will not regulate the dissolved Al<sup>3+</sup> concentration (Deutsch, 1997) and its concentration will be regulated by the dissolution of silicate minerals.

The fault damage zones of the Little Grand fault and Salt Wash Graben are altered and cemented by the passage of  $CO_2$ -charged fluids. Feldspar grains show evidence of extensive corrosion and reprecipitation of silica, smectite and kaolinite on grain surfaces and within the local pore volume. Feldspar grains continue to dissolve even when coated with up to 10µm surface coatings of inter-grown clay minerals, suggesting the maintenance of porosity within the surface coating. This adds to the evidence that the presence of such a coating does not inhibit dissolution at the mineral surface.

#### 6.1.2. Fluid-Mineral Reaction Kinetics

#### **Silicate Mineral Dissolution**

Using the evolution of the CO<sub>2</sub>-charged groundwater chemistry along defined flow paths the kinetics of the dissolution reactions controlling groundwater chemistry was investigated. The progress of individual reactions, inferred from changes in groundwater chemistry was modelled using mass balance techniques. The mineral reactions are close to stoichiometric with plagioclase and K-feldspar dissolution largely balanced by precipitation of clay minerals and carbonate. Mineral modes, in conjunction with published surface area measurements and flow rates estimated from hydraulic head measurements, are then used to quantify the kinetics of feldspar dissolution. The close to equilibrium plagioclase dissolution rates derived from mass balance and hydrological modelling range from  $10^{-13.74 \pm 0.11/0.15} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  to  $10^{-18.63 \pm 0.6/1.5} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$ . K-feldspar dissolution rates range from  $10^{-15.45 \pm 0.08/0.09} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$  to  $10^{-17.42 \cdot 0.27/0.81} \text{ mol}\cdot\text{m}^{-2}\cdot\text{s}^{-1}$ .

rates are 1 to 3 orders of magnitude slower than rates determined by laboratory experiments at similar temperatures and pH, and 1 to 3 orders of magnitude faster than rates determined in the same aquifer under alkaline groundwater conditions. The enhancement of feldspar dissolution rates in this study area, relative to those determined by Zhu (2005) for alkaline groundwater, is attributed to the introduction of  $CO_2$  which depresses silicate mineral saturation in the fluids. The finding that the Green River system is close to thermodynamic saturation adds to the evidence that the 2–5 orders of magnitude discrepancy between laboratory and field rates may, in part, be explained by differences in the thermodynamic state of experimental and natural fluids (c.f. Burch *et al.*, 1993; White and Brantley, 2003).

The range of rates and the rate: $\Delta G_r$  dependence observed at Green River suggest that feldspar dissolution rate laws should include exponentially declining rates close to equilibrium ( $\Delta G_r$  <-10kJ/mol), over a wider range (and slower absolute values) of dissolution rate than previously suggested by experimental studies. These findings suggest that mineral-fluid reactions in CO<sub>2</sub> hosting reservoirs will be promoted by the state of disequilibrium induced by the introduction of CO<sub>2</sub> and highlight the importance of including a rate: $\Delta G_r$  dependence in the geochemical modelling of the long term interactions of CO<sub>2</sub>-fluid-rock in geological storage reservoirs. This suggests that in the earliest stages of CO<sub>2</sub> injection in storage sites systems can be expected to be highly undersaturated with respect to minerals comprising the host reservoir and reaction rates will be fast, occurring at low  $\Delta G_r$ .

#### Carbonate Precipitation Kinetics in CO<sub>2</sub>-leaking Faults

The fault damage zones of Little Grand fault and Salt Wash Graben are heavily veined and cemented with carbonate where CO<sub>2</sub>-charged fluids ascend to the surface, degassing CO<sub>2</sub> which drives carbonate supersaturation in the fluid. The precipitation of carbonate in CO<sub>2</sub> leaking faults has important implications for the long term performance of these leakage conduits as carbonate precipitation may eventual block leakage pathways. The kinetics of calcite precipitation where quantified by measuring the concentrations of trace elements known to exhibit a kinetically dependent liquid-solid partitioning. Sr concentrations in calcite cements within the fault damage zone record mean calcite precipitation rates of  $1.3 \times 10^{-6}$  to  $2.1 \times 10^{-6}$  mol/m<sup>2</sup>/s, comparable to laboratory derived calcite precipitation rates, in fluids with moderate Mn/Ca and Fe/Ca, at  $\Omega_{cc}$  of ~1 to 3. The overall variation in rate is large, from ~1x10<sup>-9</sup> to ~1x10<sup>-5</sup> mol/m<sup>2</sup>/s, probably reflecting both variation in the intrinsic rate and variation in the Sr/Ca of the parent fluid. This suggests that far-from-equilibrium carbonate precipitation, which blocks fracture conduits and causes the leaking system to self-seal, driven by CO<sub>2</sub> degassing in the shallow subsurface, can be accurately modeled with laboratory derived rates.

The continued study of fluid-rock interactions in natural settings may help further elucidate the relationship between rate and  $\Delta G_r$  for a range of mineral phases, in the close-to-equilibrium region which is so difficult to assess experimentally. These results must be tempered with the understanding that large uncertainties exist in the quantification of modelling parameters in natural settings, especially reactive mineral surface area, indirect sampling of reservoir fluids and the hydro-geological setting. The long duration of reaction accessible in natural studies, whilst allowing access to controlling factors of real mineral weathering such as near equilibrium rate dependence, also introduces uncertainty as many model parameters may change through the duration of the 'experiment'. The change in porosity and reacting mineral surface through the duration of the natural experiment cannot easily be factored into the calculation of the controlling rates. Heterogeneity in reservoir hydraulic properties, mineralogy and fluid chemistry also lead to uncertainty in the calculation of rates.

#### Heavy Metal Mobilization in CO<sub>2</sub>-rich Fluids

The modern  $CO_2$ -charged groundwaters contain high quantities of dissolved  $Fe^{2+}$  and  $Mn^{2+}$ . Superposition of Eh, pH and  $aFe^{2+}$  suggests that the redox sate of the fluid is controlled by low oxygen fugacity and fixed by the  $Fe^{3+/}Fe^{2+}$  redox couple through equilibration with hematite. This has important implications for the mobilization and transport of metals in  $CO_2$  storage sites and is analogues to iron mobilization processes recently observed at the Frio test  $CO_2$ -injection site (Hovorka *et al.*, 2006; Karaka *et al.*, 2006; Smyth *et al.*, 2009). This suggests that, even in the absence of an additional reductant, deep  $O_2$ -depleted groundwaters in  $CO_2$  storage sites will derive high metal concentrations from the pH suppression induced by large quantities of dissolved  $CO_2$ .

The fault damage zones of the Little Grand fault and Salt Wash Graben are altered and cemented by the passage of CO<sub>2</sub>-charged fluids. This alteration includes dissolution and remobilization of pre-existing Fe-oxide grain coatings, which bleaches the sediment from a distinctive ochre red to pale yellows and white at scales of mm's to cm's. High Mn and Fe concentrations are observed in fracture and host rock calcite cements within the mineralized portions of the damage zone. These cements record elevated Mn<sup>2+</sup> and Fe<sup>2+</sup> concentrations in the ancient CO<sub>2</sub>-charged groundwaters. The measured Fe and Mn concentrations where combined with equilibrium modelling techniques to derive groundwater Eh (30 to -50 mV) and pH (5.5 to 6.5) conditions. These ancient groundwaters. This finding, together with hematite solubility modelling and field and petrographic observations of extensive dissolution of hematite grain coatings and Fe-oxide reprecipitation, suggests that CO<sub>2</sub>-charged fluids alone are capable of dissolving and mobilizing Fe in these sediments. However, the precise control on Eh is uncertain.

Equilibrium redox potentials for the  $SO_4^{2^2}$ -H<sub>2</sub>S and CO<sub>2</sub>-CH<sub>4</sub> redox couples are in the region of 0 to -200 mV and -200 to -500mV, respectively (Drever, 1997). The calculated Eh values are generally higher than those expected for redox potentials controlled by either  $SO_4^{2^2}$ -H<sub>2</sub>S or CO<sub>2</sub>-CH<sub>4</sub> equilibrium. The range of values obtained is more comparable to redox potentials observed in groundwaters with low O-fugacity (e.g. White *et al.*, 1990).

Analogues km-scale sandstone bleaching of the Entrada Sandstone is observed at the apex of the Green River anticline. Mineral assemblages in samples from zones of extensive Fe<sup>3+</sup> bleaching in the Entrada Sandstone contain primary fluid inclusions of moderately saline aqueous fluid, CO<sub>2</sub> and CH<sub>4</sub> vapour and occasional liquid hydrocarbon bearing two and three phase primary inclusions. Vapour densities, inclusion pressures and homogenisation temperatures attest to the formation of these inclusions at shallow burial depth, during basin exhumation, in the last 2.1-5.5 ±1.5 Ma. The presence of a CO<sub>2</sub>-rich vapour phase with moderate quantities of CH<sub>4</sub> is attributed to mobilization of hydrocarbons and CH<sub>4</sub> by migrating CO<sub>2</sub> bearing fluids and gases. The CH<sub>4</sub> dissolved in this fluid would be a suitable redox agent for the reduction of Fe<sup>3+</sup> to Fe<sup>2+</sup>, and the high concentrations of CO<sub>2</sub> would significantly enhance the solubility and dissolution rate of hematite by lowering pH and increasing the availability of H<sup>+</sup>.

 $CO_2$  has played an important role in the dissolution and mobilization of metal oxides in all of these sandstone aquifer systems. This has important implications for trace and heavy metal mobilization in CO2 storage sites as solubilisation of heavy metal bearing minerals in shallow groundwater systems is of concern for the contamination of potable water sources (e.g. Wang and Jaffe, 2004). Further work on understanding the kinetics of these reactions, and their coupling to advective and diffusive fluid transport process, is of critical importance to the accurate prediction of the performance of  $CO_2$  storage sites.

#### 6.1.3. CO<sub>2</sub> Leakage from Fault Systems

Ancient surface travertine deposits along the trace of the Little Grand fault and Salt Wash Graben and carbonate veining within the fault damage zones record leakage of CO<sub>2</sub> from the Navajo Sandstone over a ca 400,000 year period (Burnside, 2009). CO<sub>2</sub> leakage initiated at ca 413 ka from Salt Wash Graben and at ca 114 ka from Little Grand Fault (Burnside, 2009). Temporal variation in the  $\delta^{18}O_{CaCO3}$  and  $\delta^{13}C_{CaCO3}$  of these deposits reflects multiple injections of CO<sub>2</sub> into the underlying Navajo Sandstone from deeper formations, at 10,000's year intervals. These new pulses of CO<sub>2</sub> are enriched in <sup>12</sup>C and <sup>16</sup>O, dissolving to form HCO<sub>3</sub><sup>-</sup>(aq) with a light stable isotopic composition, which is inherited by the daughter carbonate precipitates. Following the injection of individual CO<sub>2</sub> pulses, leakage and CO<sub>2</sub> degassing drives a progressive Rayleigh distillation of the HCO<sub>3</sub><sup>-</sup>(aq) reservoir and the precipitating carbonate becomes increasingly enriched in <sup>13</sup>C and <sup>18</sup>O as a consequence. Kinetic fractionation of HCO<sub>3</sub><sup>-</sup>(aq) during these periods implies rapid rates of CO<sub>2</sub> degassing and carbonate precipitation, faster than the HCO<sub>3</sub><sup>-</sup>-H<sub>2</sub>O equilibration reaction which operates on the 1000's to 10000's sec time-scale (Hendy, 1971). Periods of progressive isotopic fractionation correlate with periods of rapid surface travertine accumulation. The linear variation in  $\delta^{18}O_{CaCO3}$  and  $\delta^{13}C_{CaCO3}$  with time reflects constant rates of CO<sub>2</sub> degassing over 10's kyrs. Correlations in  $\delta^{18}O_{CaCO3}$  and  $\delta^{13}C_{CaCO3}$ , kinetic fractionation of the HCO<sub>3</sub><sup>-</sup>(aq) reservoir, the volume and rate of surface travertine formation and its spatial and temporal distribution suggest that initially leakage: a) occurred rapidly and at a constant rate, b) was localised at the anticline crest and c) occurred from a reservoir fluid saturated in CO<sub>2</sub>, coexisting with a free-gas phase. A sharp inflection in leakage rate and an approximately concurrent cessation in kinetic fraction of the HCO<sub>3</sub><sup>-</sup>(aq) reservoir are interpreted to reflect depletion of the saturated CO<sub>2</sub> and a return to undersaturated conditions, after ~75ka of leakage. During this time leakage sites propagated laterally along the length of the fault trace as fracture conduits were blocked by carbonate deposition and new leakage pathways were exploited and opened by mineral-fluid reactions. Fracture blocking rates increased as the CO<sub>2</sub> charge dissipated,  $pCO_2$  in the aquifer fell and the fluids became increasingly oversaturated in carbonate.

Whilst the cumulative  $CO_2$  loss from both Little Grand Fault and Salt Wash Graben are of the same order of magnitude ( $\sim 1 \times 10^7$  tonnes CO<sub>2</sub>), the time required to deplete the initial CO<sub>2</sub>charge to a state of  $CO_2$ -undersaturation (~8 ka versus ~75 ka), and leakage rates during this period (~927 t/a versus ~164 t/a), vary by an order of magnitude between the two fault systems. These leakage rates are also an order of magnitude slower than rates calculated for Crystal Geyser which range between 5694  $\pm$  1708 t/a to 12702  $\pm$  3810 t/a, depending upon assumptions about eruption frequency. Differences in leakage rates between the two fault systems is attributed primarily to intrinsic difference in the fault architecture and properties of the fault damage zone, including the shale gouge ratio and degree of reservoir-reservoir juxtaposition. However, the depth of the host reservoir, and thus maximum in-situ  $pCO_2$ , imposes difference in the fracture blocking rate in each fault which may impact the overall leakage rates. In addition the hydraulic properties of shallow lithologies appear to be important in controlling leakage rates where permeable formations allow migration of CO<sub>2</sub>-charged fluids away from the fault damage zone, prolonging the fluid ascent time, enhancing CO<sub>2</sub> degassing in the shallow subsurface and promoting carbonate deposition and fracture blocking. This highlights the importance of accurately modelling the fault surface, damaged zone, shallow lithological properties and regional hydraulic gradients when modelling leakage from  $CO_2$  storage sites. The findings suggest that in geological storage sites fault controlled CO<sub>2</sub> leakage rates from shallow CO<sub>2</sub> saturated fluids will be slow (relative to  $CO_2$  emission rates from anthropogenic sources) and fracture conduits will seal through carbonate precipitation impeding leakage, but that this process is likely to take place on 100's to 1000's year time-scales.

#### 6.1.4. Future Work

The interaction of fluid-mineral systems is of great importance in a range of Earth System processes including surface weathering, continental scale alteration of the crust, the behaviour and evolution of hydrothermal systems and a range of industrial processes including the long-term containment of nuclear waste and the sequestration of CO<sub>2</sub>. Establishing reliable rates for silicate mineral dissolution and its controls also has important implications for many fundamental aspects of the long term relationship between silicate weathering, global climate (Berner and Berner, 1997) and global elemental cycling (Lasaga et al., 1994).

Further work on groundwater systems over a range of pH conditions, bulk rock mineralogies and fluid residence times is crucial for understanding in-situ dissolution kinetics for the wide variety of mineral structures, and over a range of mineral saturations. Further work on the evolution of mineral surface areas over the long durations of surface mineral weather is vitally important to understand the role of the truly reactive mineral surface, as apposed to the bulk mineral surface, and how the evolution of this surface is coupled to properties of the contacting fluid and the duration of reaction. Ultimately it is likely that a range of transport phenomena are important in controlling fluid-mineral interactions at various scales. Further investigation of mineral reaction kinetics in a range of weathering environments under different conditions of water saturation and fluid velocities is crucial to understanding this coupling.

The role of microbial activity in mediating and catalysing a range of in-situ fluid-mineral reactions is beginning to be appreciated (e.g. Edwards et al., 2005, Fein, 2000). Continued work on understanding the ecology of subsurface microbial systems and the role of microbes in modifying the mineral surface, the production of metabolic by-products that enhance mineral solubilities and mediation of groundwater solute chemistry is crucial for the accurate modelling of large-scale mineral weathering in both surface and subsurface systems.

The further understanding of the long-term containment of  $CO_2$  will be greatly aided by continued work on natural analogue sites. Investigation of the geochemical evolution of a range of  $CO_2$ -accumulations, in a variety of host lithologies, is vital to understanding the underlying fluid-mineral interactions, and their coupling to physical processes, that influence the long term mineralization of  $CO_2$ . The study of a number of 'failed' natural  $CO_2$  accumulations, many of which exhibit evidence of leakage in the geological past but which are now secure, well help understand the coupling between geochemical and physical processes, that both enhance leakage and ultimately lead to its containment.

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# Appendix A Spring Geochemistry Data Tables

## A.1. Gas Isotope Geochemistry

<b>Table A.1-I</b> $\delta^{13}$ C of CO <sub>2</sub> (g)	) collected from CO <sub>2</sub> -charged	springs during the 2006 a	and 2007 field seasons.
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2000 Duiu
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Sample	Spring/Geyser	<b>δ</b> <sup>13</sup> C <sub>CO2(g)</sub> (VPDB)	Notes
UT0601	Crystal Geyser	-7.31	
UT0602	Torrey's Spring	-6.79	
UT0603	Tenmile Geyser	-7.55	Slow Freeze
UT0605	Pseudo Tenmile Geyser	-7.28	
UT0605A	Pseudo Tenmile Geyser	-7.32	
UT0606	Chaffin Ranch	-7.25	
UT0608	Airport Well	-6.61	
UT0609	Big Bubbling Spring	-6.97	Excess Water
UT0610	Small Bubbling Spring	-7.02	
UT0611	Seep, Big Bubbling Spring	-7.18	
UT0615	Tumble Weed Geyser	-6.72	
UT0617	Side Seep, Crystal Geyser	-7.30	

#### 2007 Data

Sample	Spring/Geyser	$\delta^{13}C_{CO2(g)}$ (VPDB)	Notes
GR07g001	Pseudo-Tenmile Geyser	-7.54	
GR07g006	Big Bubbling	-7.21	
GR07g003	Torreys Spring	-7.39	
GR07g004	Airport Well	-6.29	Excess Water
GR07g005	Small Bubbling Spring	-6.98	
GR07g002	Tenmile Geyser	-7.34	
GR07g012	Crystal Geyser	-7.33	
GR07g009	Chaffin Ranch	-6.88	Eruption
GR07g008	Chaffin Ranch	-6.20	Pre-eruption

## A.2. CO<sub>2</sub>-spring Fluid Chemistry & Isotope Data

**Table A.2-I** Major and minor element and isotope data from the  $CO_2$ -charged springs, 2006 and 2007 field seasons. Alkalinity [Alk] was titrated in the field. 2007 data includes field determined redox potentials (mV).

2006 Data	Temp	pН	Al <sup>3+</sup>	Ba <sup>2+</sup>	Ca <sup>2+</sup>	Fe	<b>K</b> <sup>+</sup>	Mg <sup>2+</sup>	Mn	$Na^+$	Si	Sr <sup>2+</sup>	Cl.	SO4 <sup>2-</sup>	[Alk]	DIC	<sup>87</sup> Sr/ <sup>86</sup> Sr
Spring/Sample Name	°C		µmol/l	µmol/l	mmol/l	µmol/l	mmol/l	mmol/l	µmol/l	mmol/l	mmol/l	µmol/l	mmol/l	mmol/l	meq/l	mmol/l	
Green River Airport Well	27.0	6.18	3.6	0.14	19.7	4.6	2.15	7.95	22.7	18.11	922.8	112.7	2.59	19.06	37.08	75.59	0.712660
Crystal Geyser	18.0	6.46	4.9	0.10	21.8	44.4	7.98	9.02	25.1	159.02	186.7	142.9	137.94	26.46	68.86	107.37	0.712588
Small Bubbling Spring	17.2	6.17	3.2	0.12	18.2	2.3	7.35	8.88	19.0	160.27	139.7	138.0	128.63	26.65	56.54	118.89	0.711755
Big Bubbling Spring	17.5	6.30	5.1	0.10	21.6	2.7	9.36	8.55	7.2	212.87	135.7	157.4	178.29	32.17	66.04	116.33	0.712798
Side Seep, Big Bubbling	16.5	6.21	5.0	0.11	19.1	4.0	9.23	8.65	7.5	211.26	131.0	131.0	170.47	30.12	59.69	118.75	0.713053
Pseudo-Tenmile Geyser	15.0	6.52	4.3	0.08	19.3	19.2	9.55	8.09	2.2	228.04	136.7	164.2	177.98	31.20	62.06	93.33	0.713327
Torrey's Spring	15.8	6.59	4.8	0.13	23.5	48.0	11.02	7.93	19.1	251.29	152.3	145.0	193.14	30.16	78.72	111.63	0.712720
Tenmile Geyser	15.7	6.58	5.0	0.14	22.2	83.1	6.79	9.44	18.5	219.01	159.5	236.3	165.19	14.30	58.21	83.19	0.712554
Tumble Weed Geyser	15.9	6.46	5.0	0.12	18.8	5.2	8.11	8.90	12.1	189.25	144.3	153.5	132.88	19.74	62.12	97.94	0.712663
Chaffin Ranch Geyser	14.7	6.73	5.0	0.08	26.0	67.6	7.58	9.78	17.4	193.54	134.0	165.5	128.39	14.54	76.12	100.15	0.712581

2007 Data	Eh	Temp	pН	Al <sup>3+</sup>	Ba <sup>2+</sup>	Ca <sup>2+</sup>	Fe	$\mathbf{K}^{+}$	Mg <sup>2+</sup>	Mn	Na <sup>+</sup>	Si	Sr <sup>2+</sup>	Cl.	SO4 <sup>2-</sup>	DIC	<sup>87</sup> Sr/ <sup>86</sup> Sr	$\delta^{13}C_{DIC}$	<b>δ</b> <sup>18</sup> Ο	$^{3}\mathrm{H}$
Spring/Sample Name	mV	°C		µmol/l	µmol/l	mmol/l	µmol/l	mmol/l	mmol/l	µmol/l	mmol/l	µmol/l	µmol/l	mmol/l	mmol/l	mmol/l		(VPDB)	(SMOW)	TU
Green River Airport Well	-42	26.8	6.18	4.6	0.09	22.18	106.0	2.19	8.82	24.0	20.55	993.0	104.2	2.59	20.93	66.73	N/A	-1.83	-14.48	0.50
Crystal Geyser	-5	16.9	6.37	5.8	0.08	26.13	230.6	9.35	9.63	28.4	163.56	199.8	147.1	121.77	25.58	120.96	0.712719	-0.85	-14.52	0.30
Small Bubbling Spring	-7	19.2	6.14	4.3	0.07	19.81	61.1	8.82	9.54	19.2	164.80	143.4	128.5	131.07	25.44	90.83	0.712530	-1.17	-14.25	N/A
Big Bubbling Spring	-32	17.7	6.26	5.0	0.05	23.20	123.3	11.42	9.35	6.8	218.28	138.2	148.6	183.64	30.12	85.79	0.712721	-0.48	-13.88	0.30
Side Seep, Big Bubbling	-32	17.9	6.25	4.3	0.10	20.79	118.0	11.03	9.28	9.7	213.47	148.9	127.5	161.41	30.33	94.80	N/A	-0.39	-13.77	N/A
Pseudo-Tenmile Geyser	6	15.8	6.42	4.7	0.04	20.72	107.9	11.38	8.53	1.9	223.76	126.9	150.7	153.07	31.61	95.81	N/A	-0.59	-13.76	0.70
Torreys Spring	-40	16.4	6.51	5.8	0.04	25.41	144.2	13.40	8.41	19.8	247.39	123.8	132.6	229.42	31.41	118.75	0.712617	0.74	-13.86	0.70
Tenmile Geyser	-23	18.5	6.55	5.0	0.06	24.08	55.9	7.81	10.13	19.0	220.07	131.6	221.3	197.61	19.71	110.01	0.711788	-1.67	-13.21	0.30
Tumble Weed Geyser	-32	17.9	6.42	6.0	0.03	28.26	263.7	8.62	10.34	17.9	192.66	115.7	154.4	179.45	25.91	84.53	0.713056	-0.19	-13.82	0.40
Chaffin Ranch Geyser	-35	16.0	6.75	5.8	0.02	27.58	267.2	8.62	10.33	17.4	194.19	112.4	147.1	145.74	26.22	118.59	N/A	-0.63	-13.76	0.50

## A.3. Crystal Geyser Fluid Chemistry & Isotope Data

Table A.3-I Major and minor element and isotope data from temporal samples through the build up to, and course of, a large-scale eruption of Crystal Geyser.

Sample	Time	pН	Temp	Al <sup>3+</sup>	Ba <sup>2+</sup>	Ca <sup>2+</sup>	Fe	<b>K</b> <sup>+</sup>	Mg <sup>2+</sup>	Mn	Na <sup>+</sup>	Si	Sr <sup>2+</sup>	CI.	SO4 <sup>2-</sup>	DIC	δ <sup>18</sup> Ο	$\delta^{13}C_{DIC}$	<sup>87</sup> Sr/ <sup>86</sup> Sr
			°C	µmol/l	µmol/l	mmol/l	µmol/l	mmol/l	mmol/l	µmol/l	mmol/l	µmol/l	µmol/l	mmol/l	mmol/l	mmol/l	(VSMOW)	(VPDB)	
CG1	12:00:00	6.52	17.0	5.8	0.08	26.1	231	9.3	9.6	28	164	200	147	123	24.7	109	-14.36	-0.69	0.712712
CG2	12:30:00	6.38	18.1	5.4	0.08	26.3	236	9.4	9.6	28	164	203	149	124	24.9	111	-14.32	-0.92	0.712704
CG3	13:00:00	6.48	18.3	5.8	0.07	26.1	246	9.5	9.6	28	166	203	149	126	24.9	101	-14.35	-0.52	0.712707
CG4	13:30:00	6.38	18.1	6.1	0.09	26.3	250	9.6	9.7	28	169	204	149	129	25.0	103	-14.32	-0.61	0.712723
CG5	14:00:00	6.38	18.2	5.4	0.07	25.8	246	9.7	9.7	27	170	205	148	128	25.2	119	-14.51	-0.81	0.712726
CG6	14:30:00	6.47	18.2	6.2	0.07	26.0	239	9.6	9.5	27	168	199	148	122	24.2	93	-14.48	-0.51	0.712723
CG7	15:00:00	6.51	18.8	5.3	0.08	25.9	229	9.5	9.5	27	169	200	148	123	24.2	90	-14.54	-0.63	0.712723
CG8	15:30:00	6.38	18.7	6.0	0.08	25.7	241	9.7	9.6	27	171	204	147	130	25.5	109	-14.44	-0.94	0.712726
CG9	15:47:00	6.57	18.1	6.0	0.07	26.3	251	9.6	9.6	27	171	201	150	129	25.2	95	-14.43	-0.22	0.712729
CG10	15:55:10	6.57	17.7	6.1	0.08	26.5	252	9.4	9.7	30	163	202	148	123	25.0	98	-14.46	-0.73	0.712698
CG11	16:02:00	6.55	17.3	5.7	0.08	26.3	248	9.2	9.6	30	160	199	148	121	24.6	88	-14.49	-0.19	0.712696
CG12	16:06:00	6.57	17.7	5.8	0.08	26.2	257	9.1	9.6	29	158	202	149	122	24.9	96	-14.50	-0.29	0.712685
CG13	16:10:00	6.55	17.8	5.9	0.07	26.5	258	9.1	9.7	30	158	206	150	119	24.1	102	-14.51	-0.47	0.712669
CG14	16:16:30	6.55	17.8	6.0	0.08	26.5	264	9.1	9.8	30	157	207	151	117	24.2	82	-14.52	-0.35	0.712674
CG15	16:33:00	6.55	18.7	5.7	0.08	26.7	280	8.6	10.0	31	149	203	154	112	23.9	93	-14.55	-0.42	0.712613
CG16	17:00:00	6.53	18.2	5.4	0.08	26.8	281	8.1	10.2	32	133	205	158	97	22.4	93	-14.61	-0.23	0.712551
CG17	17:30:00	6.56	16.6	5.5	0.08	26.7	276	7.8	10.2	32	128	202	159	98	22.7	86	-14.64	-0.42	0.712524

## **A.4. Paradox Formation Brine Analyses**

								mm			
Lat	Long	API	Interval	pН	Ca	K	Mg	Na	HCO3	Cl	<b>SO4</b>
37.32	-109.25	4303706099	DESERT CREEK	7.6	113		38	550	3	846	1
38.14	-109.81	4303706346	PARADOX	8.3	52		46	572	0	719	26
37.09	-109.5	4303705082	PARADOX	8	16		66	578	19	623	50
38.15	-109.8	4303706350	PARADOX	8.2	135		47	596	3	931	14
37.08	-109.5		PARADOX	8	32		31	638	16	649	50
37.08	-109.49	4303705074	PARADOX	7.1	51		19	663	19	700	42
38.15	-109.8	4303706350	PARADOX	6.8	187		40	674	3	1100	14
37.05	-109.49	4303705047	PARADOX	7.18	66		62	703	20	869	36
37.07	-109.6	43037005068	PARADOX	8.3	57	12	50	739	15	880	35
37.3	-109.18	4303706002	PARADOX HERMOSA	6.8	177		77	793	2	1298	1
37.07	-109.6	4303705068	PARADOX LOWER	7.4	62	13	53	797	14	959	34
37.07	-109.6	4303705068	PARADOX	7.6	60	13	53	811	16	965	35
37.07	-109.6	43037005068	PARADOX	7.8	60	13	51	811	17	959	35
37.39	-109.46		ISMAY	6.6	100	10	39	870	5	1111	21
37.09	-109.61	4303705077	PARADOX	7.1	135		75	892	19	1241	26
37.09	-109.61	4303705077	PARADOX	7.1	105		53	943	19	1185	28
37.66	-109.59	43037006292	ISMAY UPPER	7.4	174		53	944	2	1326	35
37.05	-109.59	4303705057	PARADOX	6	195		117	973	9	1551	19
37.07	-109.31	4303705067	PARADOX	7.9	162		113	996	8	1467	36
38.59	-109.96	4301905035	PARADOX	5.4	182		97	1044	1	1574	16
37.04	-109.22	4303705041	ISMAY LOWER	8	73	8	53	1059	6	1308	7
			DESERT CREEK	7.2	187	7	70	1171	2	1664	13
37.42	-109.42	4303706216	PARADOX	7.4	105		70	1179	2	1805	21
37.3	-109.25		PARADOX	7.2	267		97	1249	2	1946	14
37.09	-109.08	4303705080	ISMAY LOWER	7.3	133	8	91	1393	4	1828	10
37.03	-109.53	4303720291	ISMAY LOWER	7.3	82		56	1415	23	1612	28
37.32	-109.32		PARADOX	8.3	236		64	1428	4	1974	24
			DESERT CREEK	7.2	223	17	90	1544	2	2172	7
37.09	-109.08	4303705080	ISMAY LOWER	7.1	147	8	112	1554	5	2059	8
37.26	-109.1	4303706545	ISMAY UPPER LOWER	7.2	170	11	79	1611	3	2087	15
37.26	-109.1	4303706545	ISMAY UPPER LOWER	7.4	182	10	60	1652	2	2115	15
38.34	-109.59	4303706415	PARADOX	6.7	49		22	1670	8	1721	42
37.08	-109.14	4303705075	PARADOX	7.5	94		44	1687	3	1907	27
37.3	-109.14	4303705990	PARADOX	7	210		216	1689	2	2510	14
37.26	-109.1	4303706545	ISMAY UPPER LOWER	7.4	188	11	73	1693	3	2200	11
37.26	-109.1	4303706545	ISMAY UPPER LOWER	7	188	10	79	1701	2	2228	15
37.68	-109.5	43037006294	PARADOX	7.4	281		112	1706	3	2460	15
37.08	-109.14	4303705075	PARADOX	7.5	115		50	1739	7	2032	15
37.26	-109.1	4303706545	ISMAY UPPER LOWER	5.5	188	11	79	1762	1	2285	10
37.26	-109.1	4303706545	ISMAY UPPER LOWER	7.3	194	13	73	1763	3	2285	11
37.26	-109.1	4303706545	ISMAY UPPER LOWER	5	206	11	79	1781	1	2341	10

**Table A.4-I** Major solute chemistry of brine analyses from the Paradox Formaiton, Paradox Basin, compiled from the USGS produced water database Breit, (2002).

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								mmol/l			
Lat	Long	API	Interval	pН	Ca	K	Mg	Na	HCO3	Cl	<b>SO4</b>
37.29	-109.5	43037005903	PARADOX ISMAY	6.2	556		226	1806		3357	6
37.24	-109.11	4303705658	ISMAY	8.1	213		80	1826	3	2370	18
37.22	-109.11	4303705483	ISMAY LOWER	7.1	195		80	1827	3	2341	17
37.26	-109.1	4303706545	ISMAY UPPER LOWER	5.7	206	11	97	1830	1	2426	10
37.29	-109.14	4303705902	ISMAY LOWER	8.7	201	7	104	1831	1	2426	9
37.26	-109.1	4303706545	ISMAY UPPER LOWER	7	206	13	79	1838	2	2398	10
37.3	-109.14	4303705990	PARADOX	6.9	196		115	1892	2	2482	15
37.3	-109.18	4303706002	PARADOX HERMOSA	7.7	241		177	1988	5	2528	8
			PARADOX ISMAY	7.2	421		203	2012	1	3244	7
37.62	-109.48		PARADOX ISMAY	7.8	413		151	2021	3	3131	7
37.29	-109.44		PARADOX ISMAY	6.2	360		241	2028		3216	8
37.72	-109.15	4303706303	PARADOX		302		201	2030	1	3013	10
37.3	-109.31	4303705976	DESERT CREEK	6.6	451		158	2041	1	3244	7
37.22	-109.11	4303705483	ISMAY	6.7	216		83	2054	1	2629	11
37.68	-109.5	43037006294	PARADOX	6.8	358		179	2072	2	3120	13
37.22	-109.11	4303705483	ISMAY	6.6	223		87	2088	2	2686	11
37.25	-109.07	4303705704	ISMAY LOWER	5.7	221		99	2100	1	2713	13
37.31	-109.56	4303706071	ISMAY LOWER	8.2	187		100	2182	2	2708	24
37.68	-109.5	43037006294	PARADOX	6.7	377		230	2264	2	3456	10
37.24	-109.29	4303705649	DESERT CREEK	6.9	376		166	2316	2	3385	6
37.25	-109.34		DESERT CREEK	6.8	398		294	2349	1	3723	4
37.27	-109.25	4303705805	PARADOX	6.7	447		185	2388	2	3639	6
37.16	-109.57		PARADOX	5.3	357		190	2392	1	3469	9
37.22	-109.26	4303705485	DESERT CREEK	6.8	360		181	2574	2	3639	8
37.31	-109.54	4303706094	PARADOX	7.2	320		142	2596	4	3498	10
37.29	-109.25	4303705918	DESERT CREEK	6.7	518		233	2600	2	4090	6
37.29	-109.35		DESERT CREEK	7	548		196	2753	2	4231	5
37.33	-109.19	4303706157	PARADOX	6.9	629		140	2807	5	4316	12
37.24	-109.34	4303705648	PARADOX	6.6	455		270	2868	2	4299	9
37.3	-109.29	4303706000	DESERT CREEK	6.5	488		188	2887	1	4231	4
37.29	-109.52		PARADOX	6.5	548		218	2989		4513	5
37.33	-109.26		PARADOX UPPER	6.2	568		227	3068	8	4639	6
37.31	-109.32	4303706111	PARADOX P 3		517		156	3103	1	4441	4
37.3	-109.05	4303705993	PARADOX	5.2	262		80	3140	1	3808	8
37.19	-109.07	4303705304	PARADOX	6.7	771		220	3220	3	5190	5
37.28	-109.29	4303705868	PARADOX C D	7	540		194	3302	3	4752	8
37.54	-109.34	4303706269	PARADOX	5	465		188	3385		4682	4
37.54	-109.33		PARADOX	6.2	464		115	3415	1	4569	4
37.3	-109.05	4303705993	PARADOX ISMAY	6.5	308		143	3426	2	4316	6
37.28	-109.27	4303705835	PARADOX C D	7.2	417		129	3431	6	4500	9
37.3	-109.18	4303706002	PARADOX	5.8	824		281	3565	8	5745	12
38.59	-109.96	4301905035	PARADOX	6.4	192		60	3754	2	4231	14

### A.5. Uncertainty Analysis

Fully propagated errors in the calculated reaction rates were derived, using the Gaussian error propagation method (Barrante, 1974), from the elemental uncertainties of analytically determined parameters and the parametric uncertainties of all modelled components. Given that all the variables in the calculation of mineral reaction rates are uncorrelated, and therefore statistically independent, the linear error propagation method of Anderson (1976) can be used to calculate the uncertainty in reaction rates arising from uncertainty in the individual parameters used.

Uncertainty in the brine corrected fluid composition was determined using a linear error propagation method, taking into account an assumed 3% analytical uncertainty in the measured  $CO_2$ -spring fluid composition and the standard deviation in the concentration of each solute in the brine, determined from a compilation of brine compositions for fluids in Pennsylvanian strata in the northern Paradox Basin (Breit, 2002; Spangler *et al.*, 1996).

$$\sigma_{k_c}^2 = \left( \left[ \left( \frac{\sigma_{k_s}}{k_s} \right)^2 + \left( \frac{\sigma_{Cl_s}}{Cl_s} \right)^2 + \left( \frac{\sigma_{Cl_B}}{Cl_B} \right)^2 \right]^{0.5} \cdot \frac{k_s}{(1 - Cl_s / Cl_B)} \right)^2 + \left( \left[ \left( \frac{\sigma_{k_B}}{k_B} \right)^2 + \left( \frac{\sigma_{Cl_s}}{Cl_s} \right)^2 + \left( \frac{\sigma_{Cl_s}}{Cl_B} \right$$

Uncertainties in the modelled mass transfer coefficients were determined by treating the mass balance equations as a set of dependent linear equations and propagating the error on the corrected element concentrations.

$$\sigma_{M_{Kspar}}^{2} = \left\{ \frac{\sigma_{K_{f}}}{b_{K,Kspar}} \right\}^{2} + \left\{ \frac{\sigma_{K_{i}}}{b_{K,Kspar}} \right\}^{2} + \left\{ \left( b_{K,Smct} \cdot \sigma_{Mg_{f}} \right) \cdot \left( \frac{\sigma_{Mg_{f}}}{b_{Mg,Smct}} \right) \cdot \left( \frac{\sigma_{Mg_{f}}}{b_{K,Kspar}} \right) \right\}^{2} + \left\{ \left( b_{K,Smct} \cdot \sigma_{Mg_{i}} \right) \cdot \left( \frac{\sigma_{Mg_{i}}}{b_{Mg,Smct}} \right) \cdot \left( \frac{\sigma_{Mg_{i}}}{b_{K,Kspar}} \right) \right\}^{2} \right\}^{2}$$
(A2)

where  $\sigma_{m_{T,k}}^2 = \sigma_{k_{final}}^2 + \sigma_{k_{nitiali}}^2$  (A3)

Uncertainty in  $\partial M_j/\partial z$  resulting from the fit of  $M_j$ -dz was computed as
$$\left(\frac{\sigma\partial M_j/\partial z}{\partial M_j/\partial z}\right)^2 = \left(\frac{\sigma A}{A}\right)^2 + \left(\frac{\sigma B}{B}\right)^2 + \left(\frac{\sigma B}{z}\right)^2 + 2\frac{\sigma A}{A}\frac{\sigma B}{B}\rho_{AB}$$
(A4)

where 
$$\rho_{ab} = \frac{COV_{AB}}{\sqrt{COV_{AA}} \cdot \sqrt{COV_{BB}}}$$
 (A5)

and *A* and *B* are the fitting terms in equation (A4).

The uncertainty in calculated reaction rates, resulting from uncertainty in individual parameters used in the calculation can be computed as follows, assuming all parameters are statistically independent:

$$\sigma R_{j}^{2} = \left\{ \left( \frac{M_{j}\omega_{o}}{S_{j}} \right) \sigma \phi \right\}^{2} + \left\{ \left( -\frac{M_{j}\omega_{o}\phi}{S_{j}^{2}} \right) \sigma S_{j} \right\}^{2} + \left\{ \left( \frac{\omega_{o}\phi}{S_{j}} \right) \sigma M_{j} \right\}^{2} + \left\{ \left( \frac{M_{j}\phi}{S_{j}} \right) \sigma \omega_{o} \right\}^{2} \right\}^{2}$$
(A6)

Model parameters that are derived from compilations of published data have values of the mean of these compilations and uncertainties of one standard error. An average of laboratory determined hydraulic conductivities of the Navajo Sandstone (Hood and Patterson, 1984) was used, giving a mean conductivity value (n = 91) of 0.47m/day with ±0.06m/day variation. Effective porosity values for the Navajo Sandstone vary from 10% to 35% (n = 129) (Cooley *et al.*, 1969; Hood and Patterson, 1984; Weigel, 1986; Freethy 1988), with a volume-weighted average of 20.03% with ±4.4% variation. Individual mineral abundances used in these calculations were determined as the mean of the normative mineral abundances calculated from the whole rock data of this study and Bowen (2004) and the mineral compositional analyses of this study. Variation in individual mineral abundances was taken as one standard error of the mean of these analyses. The error associated with bulk surface area measurements (n = 7) was taken to be ±0.06m/g, one standard error of the BET measurements of Zhu (2005). From these the uncertainty in mineral surface area was calculated as

$$\sigma S_{j}^{2} = (\sigma s_{j} \cdot v_{j} \cdot (1-\phi) \cdot \rho)^{2} + (\sigma \phi \cdot s_{j} \cdot v_{j} \cdot \rho)^{2} + (\sigma v_{j} \cdot s_{j} \cdot (1-\phi) \cdot \rho)^{2}$$
(A7)

Uncertainties in the free energies of the reactions are determined as a square root of the sum of the products of activity uncertainties ( $\pm 5\%$  of the calculated activities) and derivatives of  $\Delta G_r$ , taken with respect to activities and equilibrium constants of equation

(20) and (23), all raised to the square. For the dissolution of K-feldspar this expression has the form

$$\sigma_{\Delta G}^{2} = RT \left[ \left( \frac{0.95\sigma_{a_{K^{+}}}}{a_{K^{+}}} \right)^{2} + \left( \frac{0.05\sigma_{a_{Na^{+}}}}{a_{Na^{+}}} \right)^{2} + \left( \frac{\sigma_{a_{Al(OH)_{2}^{+}}}}{a_{Al(OH)_{2}^{+}}} \right)^{2} + \left( \frac{3\sigma_{a_{H_{4}SIO_{4}}}}{a_{H_{4}SIO_{2}}} \right)^{2} + \left( \frac{2\sigma_{a_{H^{+}}}}{a_{H^{+}}} \right)^{2} + \left( \frac{\sigma_{a_{K_{eq}}}}{K_{eq}} \right)^{2} \right]$$
(A8)

The standard deviations of  $\Delta G_r$  are on average 0.5–1 kJ/mol.

## **Appendix B**

## **Petrographic, XRF and Petrophysical Data: Navajo Sandstone**

#### **B.1. XRF Analyses**

Table B.B-I Major element XRF analyses for Entrada and Navajo Sandstone samples.

sampla	DS026	<b>DS044</b>	<b>DS045</b> 0	<b>DS046</b>	D\$056	DS060b	SV001	SV002	SV008	SV000
sample	K3020	N3044	<b>N3043a</b>	<b>N3040</b>	KS050	KSUUU	5,001	37002	5,000	5 1 003
wt. %	Navajo	Navajo	Navajo	Navajo	Entrada	Entrada	Navajo	Navajo	Navajo	Navajo
SiO2	94.05	90.25	72.51	92.57	75.06	77.15	81.05	80.92	77.56	74.71
TiO2	0.083	0.169	0.243	0.091	0.288	0.262	0.292	0.294	0.287	0.301
Al2O3	2.77	4.08	4.43	2.87	6.76	5.88	5.80	5.53	5.95	6.04
Fe2O3	0.26	0.46	1.11	0.21	1.39	0.92	1.54	1.47	1.74	1.56
MnO	0.004	0.003	0.072	0.004	0.037	0.031	0.050	0.059	0.099	0.098
MgO	0.02	0.12	3.82	0.11	1.76	1.53	0.97	1.01	1.81	1.89
CaO	0.05	0.65	5.95	0.14	4.73	4.57	3.22	3.36	4.84	5.51
Na2O	0.06	0.07	0.09	0.15	0.45	0.40	0.18	0.26	0.31	0.33
K2O	1.52	2.05	2.16	1.83	2.36	2.09	2.30	2.14	2.20	2.18
P2O5	0.033	0.046	0.053	0.015	0.080	0.072	0.076	0.077	0.101	0.107
LOI	0.49	1.34	9.50	1.03	6.69	6.66	4.48	4.62	6.26	7.40
Total	99.35	99.24	99.93	99.02	99.60	99.57	99.96	99.73	101.14	100.12
ppm										
Ba	285	387	358	297	352	308	313	381	389	663
Cr	8	15	16	12	20	16	18	26	23	20
Ni	8	7	11	8	11	7	12	6	9	13
<b>S%</b>	0.01	0.11	0.01	0.11	0.01	0.12	0.02	0.03	0.02	0.03

Please Note: Ba, Cr, Ni and S values presented here are only approximate and are for information purposes only.

#### **B.2. Electron Probe Data: Navajo Sandstone**

**Table B.B-II** Recalculated probe data for Navajo Sandstone samples. Abbreviations: K-spar = K-feldspar,plag = plagioclase, Smct = smectite, Dolo = dolomite, Cc = calcite

wt% oxides							Sample						
Slide No.	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026
Phase	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar
Na <sub>2</sub> O	0.63	0.32	0.36	0.24	0.62	0.68	0.55	1.13	0.40	0.59	0.41	0.88	0.34
MgO	0.004	0.000	0.007	0.000	0.002	0.001	0.002	0.003	0.004	0.004	0.003	0.002	-0.001
FeO	-0.003	0.083	0.212	0.107	0.015	-0.002	0.074	0.033	0.063	0.041	0.030	0.059	0.127
CaO	0.042	0.060	0.043	0.024	0.027	0.030	0.017	0.049	0.007	0.000	0.090	0.056	0.039
BaO	0.25	0.77	0.71	0.53	0.43	0.28	0.36	0.10	0.39	0.05	0.38	0.03	0.19
K <sub>2</sub> O	15.98	16.14	16.16	16.56	16.24	16.18	16.07	15.67	16.64	16.51	16.59	16.05	16.54
SrO	0.13	0.08	0.09	0.02	0.04	0.05	0.02	-0.01	0.00	0.03	0.03	-0.01	0.01
SiO <sub>2</sub>	63.99	63.34	63.04	63.41	63.64	63.78	64.38	65.24	65.29	65.55	63.51	64.23	63.81
Al <sub>2</sub> O <sub>3</sub>	17.97	18.22	18.43	18.27	18.25	18.26	18.19	18.09	17.85	18.09	18.66	18.34	18.16
TiO <sub>2</sub>	-0.02	-0.07	-0.07	-0.05	-0.05	-0.03	-0.05	0.00	-0.05	0.00	-0.03	0.02	-0.01
Total	99.00	99.04	99.06	99.16	99.27	99.27	99.68	100.31	100.64	100.87	99.71	99.68	99.22
Na	0.057	0.029	0.033	0.022	0.056	0.062	0.050	0.101	0.036	0.052	0.037	0.079	0.031
Mg	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Ca	0.002	0.003	0.002	0.001	0.001	0.002	0.001	0.002	0.000	0.000	0.005	0.003	0.002
Ba	0.005	0.014	0.013	0.010	0.008	0.005	0.006	0.002	0.007	0.001	0.007	0.001	0.003
К	0.955	0.969	0.971	0.993	0.971	0.966	0.954	0.921	0.980	0.967	0.989	0.951	0.988
Sr	0.003	0.002	0.003	0.001	0.001	0.001	0.001	0.000	0.000	0.001	0.001	0.000	0.000
Si	2.998	2.981	2.969	2.980	2.982	2.984	2.995	3.005	3.013	3.009	2.966	2.985	2.988
Al	0.992	1.011	1.023	1.012	1.008	1.007	0.998	0.982	0.971	0.979	1.027	1.005	1.002
Sum	5.01	5.01	5.02	5.02	5.03	5.03	5.01	5.01	5.01	5.01	5.03	5.03	5.02
Slide No.	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026
Slide No. Phase	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar	RS026 K-spar
Slide No. Phase Na <sub>2</sub> O	RS026 K-spar 0.40	RS026 K-spar 0.25	RS026 K-spar 0.23	RS026 K-spar 0.51	RS026 K-spar 0.31	RS026 K-spar 0.79	RS026 K-spar 1.10	RS026 K-spar 0.16	RS026 K-spar 0.61	RS026 K-spar 0.55	RS026 K-spar 0.43	RS026 K-spar 0.57	RS026 K-spar 0.74
Slide No. Phase Na <sub>2</sub> O MgO	RS026 K-spar 0.40 -0.003	RS026 K-spar 0.25 0.006	RS026 K-spar 0.23 0.009	RS026 K-spar 0.51 0.002	RS026 K-spar 0.31 0.005	RS026 K-spar 0.79 0.005	RS026 K-spar 1.10 0.005	RS026 K-spar 0.16 -0.002	RS026 K-spar 0.61 0.003	RS026 K-spar 0.55 0.000	RS026 K-spar 0.43 0.002	RS026 K-spar 0.57 0.004	RS026 K-spar 0.74 0.003
Slide No. Phase Na2O MgO FeO	RS026 K-spar 0.40 -0.003 0.060	RS026 K-spar 0.25 0.006 0.039	RS026 K-spar 0.23 0.009 0.031	RS026 K-spar 0.51 0.002 0.035	RS026 K-spar 0.31 0.005 0.057	RS026 K-spar 0.79 0.005 0.024	RS026 K-spar 1.10 0.005 0.008	RS026 K-spar 0.16 -0.002 0.028	RS026 K-spar 0.61 0.003 0.023	RS026 K-spar 0.55 0.000 0.121	RS026 K-spar 0.43 0.002 0.064	RS026 K-spar 0.57 0.004 0.023	RS026 K-spar 0.74 0.003 0.031
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO	RS026 K-spar 0.40 -0.003 0.060 0.068	RS026 K-spar 0.25 0.006 0.039 0.037	RS026 K-spar 0.23 0.009 0.031 0.023	RS026 K-spar 0.51 0.002 0.035 0.060	RS026 K-spar 0.31 0.005 0.057 0.016	RS026 K-spar 0.79 0.005 0.024 0.063	RS026 K-spar 1.10 0.005 0.008 0.058	RS026 K-spar 0.16 -0.002 0.028 0.020	RS026 K-spar 0.61 0.003 0.023 0.036	RS026 K-spar 0.55 0.000 0.121 0.089	RS026 K-spar 0.43 0.002 0.064 0.011	RS026 K-spar 0.57 0.004 0.023 0.053	RS026 K-spar 0.74 0.003 0.031 0.054
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04	RS026 K-spar 0.25 0.006 0.039 0.037 1.18	RS026 K-spar 0.23 0.009 0.031 0.023 0.87	RS026 K-spar 0.51 0.002 0.035 0.060 0.10	RS026 K-spar 0.31 0.005 0.057 0.016 0.03	RS026 K-spar 0.79 0.005 0.024 0.063 0.05	RS026 K-spar 1.10 0.005 0.008 0.058 0.04	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10	RS026 K-spar 0.61 0.003 0.023 0.036 0.28	RS026 K-spar 0.55 0.000 0.121 0.089 0.05	RS026 K-spar 0.43 0.002 0.064 0.011 0.16	RS026 K-spar 0.57 0.004 0.023 0.053 0.74	RS026 K-spar 0.74 0.003 0.031 0.054 0.16
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04 16.38	RS026 K-spar 0.25 0.006 0.039 0.037 1.18 16.68	RS026 K-spar 0.23 0.009 0.031 0.023 0.87 16.15	RS026 K-spar 0.51 0.002 0.035 0.060 0.10 16.43	RS026 K-spar 0.31 0.005 0.057 0.016 0.03 16.48	RS026 K-spar 0.79 0.005 0.024 0.063 0.05 16.13	RS026 K-spar 1.10 0.005 0.008 0.058 0.04 15.67	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10	RS026     K-spar     0.61     0.003     0.023     0.036     0.28     16.50	RS026 K-spar 0.55 0.000 0.121 0.089 0.05 16.47	RS026 K-spar 0.43 0.002 0.064 0.011 0.16 16.54	RS026 K-spar 0.57 0.004 0.023 0.053 0.74 16.21	RS026 K-spar 0.74 0.003 0.031 0.054 0.16 16.27
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04 16.38 -0.04	RS026 K-spar 0.25 0.006 0.039 0.037 1.18 16.68 0.00	RS026 K-spar 0.23 0.009 0.031 0.023 0.87 16.15 0.00	RS026 K-spar 0.51 0.002 0.035 0.060 0.10 16.43 0.03	RS026 K-spar 0.31 0.005 0.057 0.016 0.03 16.48 0.03	RS026 K-spar 0.79 0.005 0.024 0.063 0.05 16.13 0.02	RS026 K-spar 1.10 0.005 0.008 0.058 0.04 15.67 0.01	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01	RS026 K-spar 0.61 0.003 0.023 0.036 0.28 16.50 0.01	RS026 K-spar 0.55 0.000 0.121 0.089 0.05 16.47 0.01	RS026 K-spar 0.43 0.002 0.064 0.011 0.16 16.54 0.00	RS026 K-spar 0.57 0.004 0.023 0.053 0.74 16.21 0.00	RS026 K-spar 0.74 0.003 0.031 0.054 0.16 16.27 0.02
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub>	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04 16.38 -0.04 63.25	RS026 K-spar 0.25 0.006 0.039 0.037 1.18 16.68 0.00 63.81	RS026 K-spar 0.23 0.009 0.031 0.023 0.87 16.15 0.00 62.96	RS026 K-spar 0.51 0.002 0.035 0.060 0.10 16.43 0.03 63.21	RS026 K-spar 0.31 0.005 0.057 0.016 0.03 16.48 0.03 64.54	RS026 K-spar 0.79 0.005 0.024 0.063 0.05 16.13 0.02 64.66	RS026 K-spar 1.10 0.005 0.008 0.058 0.04 15.67 0.01 63.59	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70	RS026 K-spar 0.61 0.003 0.023 0.036 0.28 16.50 0.01 65.17	RS026 K-spar 0.55 0.000 0.121 0.089 0.05 16.47 0.01 65.37	RS026 K-spar 0.43 0.002 0.064 0.011 0.16 16.54 0.00 65.78	RS026 K-spar 0.57 0.004 0.023 0.053 0.74 16.21 0.00 64.62	RS026 K-spar 0.74 0.003 0.031 0.054 0.16 16.27 0.02 64.56
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub>	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04 16.38 -0.04 63.25 18.03	RS026 K-spar 0.25 0.006 0.039 0.037 1.18 16.68 0.00 63.81 18.57	RS026 K-spar 0.23 0.009 0.031 0.023 0.87 16.15 0.00 62.96 18.26	RS026 K-spar 0.51 0.002 0.035 0.060 0.10 16.43 0.03 63.21 18.28	RS026 K-spar 0.31 0.005 0.057 0.016 0.03 16.48 0.03 64.54 17.56	RS026 K-spar 0.79 0.005 0.024 0.063 0.05 16.13 0.02 64.66 18.57	RS026 K-spar 1.10 0.005 0.008 0.058 0.04 15.67 0.01 63.59 18.27	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70 18.16	RS026 K-spar 0.61 0.003 0.023 0.036 0.28 16.50 0.01 65.17 18.31	RS026 K-spar 0.55 0.000 0.121 0.089 0.05 16.47 0.01 65.37 18.33	RS026 K-spar 0.43 0.002 0.064 0.011 0.16 16.54 0.00 65.78 18.37	RS026 K-spar 0.57 0.004 0.023 0.053 0.74 16.21 0.00 64.62 18.09	RS026 K-spar 0.74 0.003 0.031 0.054 0.16 16.27 0.02 64.56 18.65
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub>	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04 16.38 -0.04 63.25 18.03 -0.01	RS026 K-spar 0.25 0.006 0.039 0.037 1.18 16.68 0.00 63.81 18.57 -0.16	RS026 K-spar 0.23 0.009 0.031 0.023 0.87 16.15 0.00 62.96 18.26 -0.12	RS026 K-spar 0.51 0.002 0.035 0.060 0.10 16.43 0.03 63.21 18.28 -0.01	RS026 K-spar 0.31 0.005 0.057 0.016 0.03 16.48 0.03 64.54 17.56 0.00	RS026 K-spar 0.79 0.005 0.024 0.063 0.05 16.13 0.02 64.66 18.57 -0.01	RS026 K-spar 1.10 0.005 0.008 0.058 0.04 15.67 0.01 63.59 18.27 -0.01	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70 18.16 0.00	RS026 K-spar 0.61 0.003 0.023 0.036 0.28 16.50 0.01 65.17 18.31 -0.03	RS026 K-spar 0.55 0.000 0.121 0.089 0.05 16.47 0.01 65.37 18.33 -0.01	RS026     K-spar     0.43     0.002     0.064     0.011     0.16     16.54     0.00     65.78     18.37     -0.02	RS026     K-spar     0.57     0.004     0.023     0.053     0.74     16.21     0.00     64.62     18.09     -0.08	RS026 K-spar 0.74 0.003 0.031 0.054 0.16 16.27 0.02 64.56 18.65 -0.02
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04 16.38 -0.04 63.25 18.03 -0.01 98.22	RS026 K-spar 0.25 0.006 0.039 0.037 1.18 16.68 0.00 63.81 18.57 -0.16 100.57	RS026     K-spar     0.23     0.009     0.031     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55	RS026 K-spar 0.51 0.002 0.035 0.060 0.10 16.43 0.03 63.21 18.28 -0.01 98.66	RS026 K-spar 0.31 0.005 0.057 0.016 0.03 16.48 0.03 64.54 17.56 0.00 99.02	RS026 K-spar 0.79 0.005 0.024 0.063 0.05 16.13 0.02 64.66 18.57 -0.01 100.31	RS026 K-spar 1.10 0.005 0.008 0.058 0.04 15.67 0.01 63.59 18.27 -0.01 98.74	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70 18.16 0.00 100.28	RS026     K-spar     0.61     0.003     0.023     0.036     0.28     16.50     0.01     65.17     18.31     -0.03     100.95	RS026 K-spar 0.55 0.000 0.121 0.089 0.05 16.47 0.01 65.37 18.33 -0.01 101.00	RS026     K-spar     0.43     0.002     0.064     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38	RS026     K-spar     0.57     0.004     0.023     0.053     0.74     16.21     0.00     64.62     18.09     -0.08     100.32	RS026 K-spar 0.74 0.003 0.054 0.16 16.27 0.02 64.56 18.65 -0.02 100.48
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04 16.38 -0.04 63.25 18.03 -0.01 98.22 0.036	RS026 K-spar 0.25 0.006 0.039 0.037 1.18 16.68 0.00 63.81 18.57 -0.16 100.57 0.023	RS026     K-spar     0.23     0.009     0.031     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55     0.021	RS026 K-spar 0.51 0.002 0.035 0.060 0.10 16.43 0.03 63.21 18.28 -0.01 98.66 0.046	RS026 K-spar 0.31 0.005 0.057 0.016 0.03 16.48 0.03 64.54 17.56 0.00 99.02 0.028	RS026 K-spar 0.79 0.005 0.024 0.063 0.05 16.13 0.02 64.66 18.57 -0.01 100.31 0.070	RS026 K-spar 1.10 0.005 0.008 0.058 0.04 15.67 0.01 63.59 18.27 -0.01 98.74 0.100	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70 18.16 0.00 100.28 0.015	RS026 K-spar 0.61 0.003 0.023 0.036 0.28 16.50 0.01 65.17 18.31 -0.03 100.95 0.054	RS026 K-spar 0.55 0.000 0.121 0.089 0.05 16.47 0.01 65.37 18.33 -0.01 101.00 0.049	RS026     K-spar     0.43     0.002     0.064     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38     0.038	RS026     K-spar     0.57     0.004     0.023     0.74     16.21     0.00     64.62     18.09     -0.08     100.32     0.051	RS026 K-spar 0.74 0.003 0.031 0.054 0.16 16.27 0.02 64.56 18.65 -0.02 100.48 0.066
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg	RS026     K-spar     0.40     -0.003     0.060     0.068     0.04     16.38     -0.04     63.25     18.03     -0.01     98.22     0.036     0.000	RS026 K-spar 0.25 0.006 0.039 0.037 1.18 16.68 0.00 63.81 18.57 -0.16 100.57 0.023 0.000	RS026     K-spar     0.23     0.009     0.031     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55     0.021     0.001	RS026     K-spar     0.51     0.002     0.035     0.060     0.10     16.43     0.03     63.21     18.28     -0.01     98.66     0.046     0.000	RS026 K-spar 0.31 0.005 0.057 0.016 0.03 16.48 0.03 64.54 17.56 0.00 99.02 0.028 0.000	RS026     K-spar     0.79     0.005     0.024     0.063     0.05     16.13     0.02     64.66     18.57     -0.01     100.31     0.070     0.0000	RS026 K-spar 1.10 0.005 0.008 0.04 15.67 0.01 63.59 18.27 -0.01 98.74 0.100 0.000	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70 18.16 0.00 100.28 0.015 0.000	RS026 K-spar 0.61 0.003 0.023 0.036 0.28 16.50 0.01 65.17 18.31 -0.03 100.95 0.054 0.000	RS026     K-spar     0.55     0.000     0.121     0.089     0.05     16.47     0.01     65.37     18.33     -0.01     101.00     0.049     0.000	RS026     K-spar     0.43     0.002     0.664     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38     0.038     0.000	RS026     K-spar     0.57     0.004     0.023     0.74     16.21     0.00     64.62     18.09     -0.08     100.32     0.051     0.000	RS026     K-spar     0.74     0.003     0.031     0.054     0.16     16.27     0.02     64.56     18.65     -0.02     100.48     0.066     0.000
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca	RS026 K-spar 0.40 -0.003 0.060 0.068 0.04 16.38 -0.04 63.25 18.03 -0.01 98.22 0.036 0.000 0.003	RS026     K-spar     0.25     0.006     0.039     0.037     1.18     16.68     0.00     63.81     18.57     -0.16     100.57     0.023     0.000     0.002	RS026     K-spar     0.23     0.009     0.031     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55     0.021     0.001	RS026     K-spar     0.51     0.002     0.35     0.660     0.10     16.43     0.03     63.21     18.28     -0.01     98.66     0.046     0.000     0.003	RS026     K-spar     0.31     0.005     0.057     0.016     0.03     16.48     0.03     64.54     17.56     0.00     99.02     0.028     0.000     0.001	RS026     K-spar     0.79     0.005     0.024     0.063     0.05     16.13     0.02     64.66     18.57     -0.01     100.31     0.070     0.000     0.003	RS026     K-spar     1.10     0.005     0.008     0.058     0.04     15.67     0.01     63.59     18.27     -0.01     98.74     0.100     0.000     0.003	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70 18.16 0.00 100.28 0.015 0.000 0.001	RS026     K-spar     0.61     0.003     0.023     0.36     0.28     16.50     0.01     65.17     18.31     -0.03     100.95     0.054     0.000     0.002	RS026     K-spar     0.55     0.000     0.121     0.089     0.05     16.47     0.01     65.37     18.33     -0.01     101.00     0.049     0.000	RS026     K-spar     0.43     0.002     0.064     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38     0.038     0.000     0.001	RS026     K-spar     0.57     0.004     0.023     0.74     16.21     0.00     64.62     18.09     -0.08     100.32     0.051     0.000     0.003	RS026     K-spar     0.74     0.003     0.031     0.054     0.16     16.27     0.02     64.56     18.65     -0.02     100.48     0.066     0.000     0.003
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba	RS026     K-spar     0.40     -0.003     0.060     0.068     0.04     16.38     -0.04     63.25     18.03     -0.01     98.22     0.036     0.000     0.003     0.001	RS026     K-spar     0.25     0.006     0.039     0.037     1.18     16.68     0.00     63.81     18.57     -0.16     100.577     0.023     0.000     0.002	RS026     K-spar     0.23     0.009     0.031     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55     0.021     0.001     0.001	RS026     K-spar     0.51     0.002     0.035     0.060     0.10     16.43     0.03     63.21     18.28     -0.01     98.66     0.046     0.000     0.003     0.003	RS026     K-spar     0.31     0.005     0.057     0.016     0.03     16.48     0.03     64.54     17.56     0.00     99.02     0.028     0.000     0.001	RS026 K-spar 0.79 0.005 0.024 0.063 0.05 16.13 0.02 64.66 18.57 -0.01 100.31 0.070 0.000 0.003 0.001	RS026     K-spar     1.10     0.005     0.008     0.058     0.04     15.67     0.01     63.59     18.27     -0.01     98.74     0.100     0.000     0.003     0.001	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70 18.16 0.00 100.28 0.015 0.000 0.001 0.002	RS026     K-spar     0.61     0.003     0.023     0.036     0.28     16.50     0.01     65.17     18.31     -0.03     100.95     0.054     0.000     0.002     0.005	RS026     K-spar     0.55     0.000     0.121     0.089     0.05     16.47     0.01     65.37     18.33     -0.01     101.00     0.049     0.000     0.004	RS026     K-spar     0.43     0.002     0.064     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38     0.038     0.000     0.001	RS026     K-spar     0.57     0.004     0.023     0.74     16.21     0.00     64.62     18.09     -0.08     100.32     0.051     0.000     0.003     0.013	RS026     K-spar     0.74     0.003     0.031     0.054     0.16     16.27     0.02     64.56     18.65     -0.02     100.48     0.066     0.000     0.003
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba K	RS026     K-spar     0.40     -0.003     0.060     0.068     0.04     16.38     -0.04     63.25     18.03     -0.01     98.22     0.036     0.000     0.003     0.001     0.987	RS026     K-spar     0.25     0.006     0.339     0.037     1.18     16.68     0.00     63.81     18.57     -0.16     100.57     0.023     0.000     0.022     0.990	RS026     K-spar     0.23     0.009     0.31     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55     0.021     0.001     0.001     0.016	RS026     K-spar     0.51     0.002     0.35     0.060     0.10     16.43     0.03     63.21     18.28     -0.01     98.66     0.0046     0.003     0.002     0.987	RS026     K-spar     0.31     0.005     0.057     0.016     0.03     16.48     0.03     64.54     17.56     0.00     99.02     0.028     0.000     0.001     0.000     0.984	RS026     K-spar     0.79     0.005     0.024     0.063     0.05     16.13     0.02     64.66     18.57     -0.01     100.31     0.070     0.000     0.003     0.001     0.950	RS026     K-spar     1.10     0.005     0.008     0.058     0.04     15.67     0.01     63.59     18.27     -0.01     98.74     0.100     0.000     0.003     0.001     0.937	RS026 K-spar 0.16 -0.002 0.028 0.020 0.10 17.10 -0.01 64.70 18.16 0.00 100.28 0.015 0.000 0.001 0.002 1.011	RS026     K-spar     0.61     0.003     0.023     0.036     0.28     16.50     0.01     65.17     18.31     -0.03     100.95     0.054     0.000     0.002     0.005     0.968	RS026     K-spar     0.55     0.000     0.121     0.089     0.05     16.47     0.01     65.37     18.33     -0.01     101.00     0.049     0.000     0.004     0.001     0.964	RS026     K-spar     0.43     0.002     0.064     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38     0.003     0.003     0.964	RS026     K-spar     0.57     0.004     0.023     0.74     16.21     0.00     64.62     18.09     -0.08     100.32     0.051     0.000     0.013     0.959	RS026     K-spar     0.74     0.003     0.031     0.054     0.16     16.27     0.02     64.56     18.65     -0.02     100.48     0.066     0.000     0.003     0.003     0.958
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba K Sr	RS026     K-spar     0.40     -0.003     0.060     0.068     0.04     16.38     -0.04     63.25     18.03     -0.01     98.22     0.036     0.000     0.003     0.001     0.987     0.000	RS026     K-spar     0.25     0.006     0.39     0.037     1.18     16.68     0.00     63.81     18.57     -0.16     100.57     0.023     0.000     0.022     0.990     0.000	RS026     K-spar     0.23     0.009     0.031     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55     0.021     0.001     0.001     0.016     0.975     0.000	RS026     K-spar     0.51     0.002     0.35     0.060     0.10     16.43     0.03     63.21     18.28     -0.01     98.66     0.046     0.000     0.003     0.002     0.987     0.001	RS026     K-spar     0.31     0.005     0.057     0.016     0.03     16.48     0.03     64.54     17.56     0.00     99.02     0.028     0.000     0.001     0.000     0.984     0.001	RS026     K-spar     0.79     0.005     0.024     0.063     0.05     16.13     0.02     64.66     18.57     -0.01     100.31     0.070     0.000     0.003     0.001     0.950     0.001	RS026     K-spar     1.10     0.005     0.008     0.058     0.04     15.67     0.01     63.59     18.27     -0.01     98.74     0.100     0.003     0.001     0.937     0.000	RS026     K-spar     0.16     -0.002     0.28     0.020     0.10     17.10     -0.01     64.70     18.16     0.00     100.28     0.015     0.000     0.001     0.002     1.011     0.000	RS026     K-spar     0.61     0.003     0.023     0.036     0.28     16.50     0.01     65.17     18.31     -0.03     100.95     0.054     0.000     0.002     0.005     0.968     0.000	RS026     K-spar     0.55     0.000     0.121     0.089     0.05     16.47     0.01     65.37     18.33     -0.01     101.00     0.049     0.000     0.004     0.001     0.964     0.000	RS026     K-spar     0.43     0.002     0.64     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38     0.003     0.001     0.003     0.964     0.000	RS026     K-spar     0.57     0.004     0.023     0.74     16.21     0.00     64.62     18.09     -0.08     100.32     0.051     0.000     0.003     0.013     0.959     0.0000	RS026     K-spar     0.74     0.003     0.031     0.054     0.16     16.27     0.02     64.56     18.65     -0.02     100.48     0.066     0.000     0.003     0.003     0.958     0.000
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba K Sr Si	RS026     K-spar     0.40     -0.003     0.060     0.068     0.04     16.38     -0.04     63.25     18.03     -0.01     98.22     0.036     0.000     0.003     0.001     0.987     0.000     2.988	RS026     K-spar     0.25     0.006     0.039     0.037     1.18     16.68     0.00     63.81     18.57     -0.16     100.57     0.023     0.000     0.002     0.022     0.990     0.000     2.970	RS026     K-spar     0.23     0.009     0.031     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55     0.021     0.001     0.001     0.016     0.975     0.000     2.978	RS026     K-spar     0.51     0.002     0.35     0.060     0.10     16.43     0.03     63.21     18.28     -0.01     98.66     0.046     0.000     0.003     0.002     0.987     0.001     2.977	RS026     K-spar     0.31     0.005     0.057     0.016     0.03     16.48     0.03     64.54     17.56     0.00     99.02     0.028     0.000     0.001     0.000     0.984     0.001     3.019	RS026     K-spar     0.79     0.005     0.024     0.063     0.05     16.13     0.02     64.66     18.57     -0.01     100.31     0.070     0.000     0.003     0.001     0.950     0.001     2.985	RS026     K-spar     1.10     0.005     0.008     0.058     0.04     15.67     0.01     63.59     18.27     -0.01     98.74     0.100     0.003     0.001     0.937     0.000     2.982	RS026     K-spar     0.16     -0.002     0.028     0.020     0.10     17.10     -0.01     64.70     18.16     0.00     100.28     0.015     0.000     0.001     0.002     1.011     0.000     2.998	RS026     K-spar     0.61     0.003     0.023     0.36     0.28     16.50     0.01     65.17     18.31     -0.03     100.95     0.054     0.000     0.002     0.005     0.968     0.000     2.996	RS026     K-spar     0.55     0.000     0.121     0.089     0.05     16.47     0.01     65.37     18.33     -0.01     101.00     0.049     0.000     0.004     0.001     0.964     0.000     2.998	RS026     K-spar     0.43     0.002     0.064     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38     0.038     0.000     0.001     0.003     0.964     0.000     3.004	RS026     K-spar     0.57     0.004     0.023     0.77     16.21     0.00     64.62     18.09     -0.08     100.32     0.051     0.000     0.013     0.959     0.000     2.997	RS026     K-spar     0.74     0.003     0.031     0.054     0.16     16.27     0.02     64.56     18.65     -0.02     100.48     0.066     0.000     0.003     0.003     0.003     0.958     0.000     2.979
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba K Sr Si Al	RS026     K-spar     0.40     -0.003     0.060     0.068     0.04     16.38     -0.04     63.25     18.03     -0.01     98.22     0.036     0.000     0.003     0.001     0.987     0.000     2.988     1.004	RS026     K-spar     0.25     0.006     0.039     0.037     1.18     16.68     0.00     63.81     18.57     -0.16     100.57     0.022     0.900     0.002     0.990     0.000     2.970     1.019	RS026     K-spar     0.23     0.009     0.031     0.023     0.87     16.15     0.00     62.96     18.26     -0.12     98.55     0.021     0.001     0.001     0.016     0.975     0.000     2.978     1.018	RS026     K-spar     0.51     0.002     0.35     0.060     0.10     16.43     0.03     63.21     18.28     -0.01     98.66     0.046     0.000     0.003     0.002     0.987     0.001     2.977     1.014	RS026     K-spar     0.31     0.005     0.057     0.016     0.03     16.48     0.03     64.54     17.56     0.00     99.02     0.028     0.000     0.001     0.000     0.984     0.001     3.019     0.968	RS026     K-spar     0.79     0.005     0.024     0.063     0.05     16.13     0.02     64.66     18.57     -0.01     100.31     0.070     0.000     0.003     0.001     2.985     1.010	RS026     K-spar     1.10     0.005     0.008     0.058     0.04     15.67     0.01     63.59     18.27     -0.01     98.74     0.100     0.003     0.001     0.937     0.000     2.982     1.009	RS026     K-spar     0.16     -0.002     0.028     0.020     0.10     17.10     -0.01     64.70     18.16     0.00     100.28     0.015     0.000     0.001     0.002     1.011     0.000     2.998     0.992	RS026     K-spar     0.61     0.003     0.023     0.036     0.28     16.50     0.01     65.17     18.31     -0.03     100.95     0.054     0.000     0.002     0.005     0.968     0.000     2.996     0.992	RS026     K-spar     0.55     0.000     0.121     0.089     0.05     16.47     0.01     65.37     18.33     -0.01     101.00     0.049     0.000     0.004     0.001     0.964     0.0901	RS026     K-spar     0.43     0.002     0.064     0.011     0.16     16.54     0.00     65.78     18.37     -0.02     101.38     0.038     0.000     0.001     0.003     0.964     0.000     3.004     0.989	RS026     K-spar     0.57     0.004     0.023     0.74     16.21     0.00     64.62     18.09     -0.08     100.32     0.051     0.000     0.013     0.959     0.000     2.997     0.989	RS026     K-spar     0.74     0.003     0.031     0.054     0.16     16.27     0.02     64.56     18.65     -0.02     100.48     0.066     0.003     0.003     0.958     0.000     2.979     1.015

wt% oxides							Sample						
Slide No.	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS026	RS044	RS044	RS044
Phase	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar	K-spar
Na <sub>2</sub> O	0.76	0.40	0.25	0.26	0.58	0.74	0.24	0.28	0.63	1.22	0.66	1.08	0.73
MgO	0.001	0.002	0.008	0.002	0.003	0.000	0.004	0.000	0.001	0.001	0.004	0.002	0.003
FeO	0.062	0.043	0.039	0.040	0.133	0.036	0.036	0.040	0.015	0.136	0.016	0.008	0.012
CaO	0.050	0.003	0.030	0.054	0.028	0.014	0.023	0.054	0.014	0.066	0.027	0.053	0.028
MnO	0.000	0.000	0.017	0.016	0.021	0.006	-0.001	0.004	0.000	0.000	0.000	0.000	0.005
BaO	0.48	1.42	0.15	0.20	1.11	0.36	0.59	0.38	0.28	0.36	0.78	0.28	0.25
K <sub>2</sub> O	16.04	16.23	16.88	16.84	15.77	16.07	16.04	16.32	16.37	15.51	15.99	15.70	15.97
SrO	0.09	0.07	0.00	0.02	0.10	0.00	0.00	0.01	0.00	0.03	0.08	0.01	0.05
SiO <sub>2</sub>	64.79	64.06	64.72	64.90	64.25	65.76	64.76	64.71	65.00	65.24	64.28	65.30	65.18
Al <sub>2</sub> O <sub>3</sub>	18.38	18.71	18.10	18.62	18.76	18.71	18.31	18.15	18.32	18.54	17.57	18.12	18.47
TiO <sub>2</sub>	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Total	100.66	100.94	100.19	100.96	100.76	101.71	100.00	99.94	100.63	101.11	99.40	100.54	100.70
Na	0.068	0.036	0.022	0.023	0.052	0.066	0.021	0.025	0.056	0.108	0.060	0.096	0.065
Mg	0.000	0.000	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Ca	0.002	0.000	0.001	0.003	0.001	0.001	0.001	0.003	0.001	0.003	0.001	0.003	0.001
Ва	0.009	0.026	0.003	0.004	0.020	0.007	0.011	0.007	0.005	0.007	0.014	0.005	0.004
К	0.944	0.959	0.998	0.988	0.931	0.933	0.948	0.966	0.963	0.906	0.955	0.922	0.936
Sr	0.002	0.002	0.000	0.001	0.003	0.000	0.000	0.000	0.000	0.001	0.002	0.000	0.001
Si	2.989	2.970	3.000	2.985	2.972	2.993	3.001	3.002	2.996	2.988	3.010	3.005	2.995
Al	1.000	1.022	0.989	1.010	1.023	1.004	1.000	0.992	0.995	1.001	0.970	0.982	1.001
Sum	5.02	5.02	5.02	5.02	5.01	5.00	4.98	5.00	5.02	5.02	5.01	5.01	5.01
Slide No.	RS045	RS045	RS045b	RS045b	RS045b	RS045b	RS045b	RS045b	RS045b	RS045b	RS045b	RS045b	RS045b
Slide No. Phase	RS045 K-spar	RS045 K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar	RS045b K-spar
Slide No. Phase Na <sub>2</sub> O	RS045 K-spar 0.57	RS045 K-spar 0.51	RS045b K-spar 0.71	RS045b K-spar 0.49	RS045b K-spar 0.74	RS045b K-spar 0.65	RS045b K-spar 0.59	RS045b K-spar 0.38	RS045b K-spar 0.33	RS045b K-spar 0.34	RS045b K-spar 0.39	RS045b K-spar 0.65	RS045b K-spar 0.29
Slide No. Phase Na <sub>2</sub> O MgO	RS045 K-spar 0.57 0.004	RS045 K-spar 0.51 0.004	RS045b K-spar 0.71 0.004	RS045b K-spar 0.49 0.000	RS045b K-spar 0.74 0.004	RS045b K-spar 0.65 0.003	RS045b K-spar 0.59 0.002	RS045b K-spar 0.38 0.004	RS045b K-spar 0.33 0.003	RS045b K-spar 0.34 0.002	RS045b K-spar 0.39 0.000	RS045b K-spar 0.65 0.006	RS045b K-spar 0.29 0.007
Slide No. Phase Na <sub>2</sub> O MgO FeO	RS045 K-spar 0.57 0.004 0.057	RS045 K-spar 0.51 0.004 0.004	RS045b K-spar 0.71 0.004 0.073	RS045b K-spar 0.49 0.000 0.000	RS045b K-spar 0.74 0.004 0.062	RS045b K-spar 0.65 0.003 0.057	RS045b K-spar 0.59 0.002 0.016	RS045b K-spar 0.38 0.004 0.018	RS045b K-spar 0.33 0.003 0.003	RS045b K-spar 0.34 0.002 0.017	RS045b K-spar 0.39 0.000 0.029	RS045b K-spar 0.65 0.006 0.041	RS045b K-spar 0.29 0.007 0.018
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO	RS045 K-spar 0.57 0.004 0.057 0.075	RS045 K-spar 0.51 0.004 0.004 0.028	RS045b K-spar 0.71 0.004 0.073 0.043	RS045b K-spar 0.49 0.000 0.000 0.018	RS045b K-spar 0.74 0.004 0.062 0.051	RS045b     K-spar     0.65     0.003     0.057     0.061	RS045b K-spar 0.59 0.002 0.016 0.028	RS045b K-spar 0.38 0.004 0.018 0.006	RS045b K-spar 0.33 0.003 0.003 0.072	RS045b K-spar 0.34 0.002 0.017 0.084	RS045b K-spar 0.39 0.000 0.029 0.029	RS045b K-spar 0.65 0.006 0.041 0.089	RS045b K-spar 0.29 0.007 0.018 0.092
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO	RS045 K-spar 0.57 0.004 0.057 0.075 0.002	RS045 K-spar 0.51 0.004 0.004 0.028 0.000	RS045b K-spar 0.71 0.004 0.073 0.043 0.010	RS045b K-spar 0.49 0.000 0.000 0.018 0.000	RS045b K-spar 0.74 0.004 0.062 0.051 0.011	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00	RS045b K-spar 0.59 0.002 0.016 0.028 0.008	RS045b K-spar 0.38 0.004 0.018 0.006 0.000	RS045b K-spar 0.33 0.003 0.003 0.072 0.000	RS045b K-spar 0.34 0.002 0.017 0.084 0.00	RS045b K-spar 0.39 0.000 0.029 0.029 0.000	RS045b K-spar 0.65 0.006 0.041 0.089 0.000	RS045b K-spar 0.29 0.007 0.018 0.092 0.007
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32	RS045 K-spar 0.51 0.004 0.004 0.028 0.000 0.16	RS045b K-spar 0.71 0.004 0.073 0.043 0.010 0.04	RS045b K-spar 0.49 0.000 0.000 0.018 0.000 0.08	RS045b K-spar 0.74 0.004 0.062 0.051 0.011 0.10	RS045b K-spar 0.65 0.003 0.057 0.061 0.00 0.05	RS045b K-spar 0.59 0.002 0.016 0.028 0.008 0.47	RS045b K-spar 0.38 0.004 0.018 0.006 0.000 0.01	RS045b K-spar 0.33 0.003 0.003 0.072 0.000 0.05	RS045b K-spar 0.34 0.002 0.017 0.084 0.00 0.04	RS045b K-spar 0.39 0.000 0.029 0.029 0.029 0.000 0.01	RS045b K-spar 0.65 0.006 0.041 0.089 0.000 0.04	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32 15.99	RS045 K-spar 0.51 0.004 0.004 0.004 0.004 0.028 0.000 0.16 16.34	RS045b K-spar 0.71 0.004 0.073 0.043 0.010 0.04 16.25	RS045b K-spar 0.49 0.000 0.000 0.018 0.000 0.08 16.25	RS045b K-spar 0.74 0.004 0.062 0.051 0.011 0.10 15.98	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08	RS045b K-spar 0.59 0.002 0.016 0.028 0.008 0.47 15.99	RS045b K-spar 0.38 0.004 0.018 0.006 0.000 0.01 16.65	RS045b K-spar 0.33 0.003 0.003 0.072 0.000 0.05 16.04	RS045b K-spar 0.34 0.002 0.017 0.084 0.00 0.04 16.29	RS045b K-spar 0.39 0.000 0.029 0.029 0.029 0.000 0.01 16.68	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.004     15.97	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32 15.99 0.03	RS045 K-spar 0.51 0.004 0.004 0.004 0.028 0.000 0.16 16.34 0.000	RS045b K-spar 0.71 0.004 0.073 0.043 0.010 0.04 16.25 0.000	RS045b K-spar 0.49 0.000 0.000 0.018 0.000 0.08 16.25 0.000	RS045b K-spar 0.74 0.004 0.062 0.051 0.011 0.10 15.98 0.000	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     0.051	RS045b K-spar 0.59 0.002 0.016 0.028 0.008 0.47 15.99 0.01	RS045b K-spar 0.38 0.004 0.018 0.006 0.000 0.01 16.65 0.000	RS045b K-spar 0.33 0.003 0.003 0.072 0.000 0.05 16.04 0.05	RS045b K-spar 0.34 0.002 0.017 0.084 0.00 0.04 16.29 0.04	RS045b K-spar 0.39 0.000 0.029 0.029 0.029 0.000 0.01 16.68 0.00	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74 0.02
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SiO <sub>2</sub>	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32 15.99 0.03 64.30	RS045 K-spar 0.51 0.004 0.004 0.028 0.000 0.16 16.34 0.000 64.59	RS045b K-spar 0.71 0.004 0.073 0.043 0.010 0.04 16.25 0.000 64.46	RS045b K-spar 0.49 0.000 0.018 0.000 0.08 16.25 0.000 64.39	RS045b K-spar 0.74 0.004 0.062 0.051 0.011 0.10 15.98 0.000 64.64	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71	RS045b K-spar 0.59 0.002 0.016 0.028 0.008 0.47 15.99 0.01 64.58	RS045b K-spar 0.38 0.004 0.018 0.006 0.000 0.01 16.65 0.000 64.65	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23	RS045b K-spar 0.34 0.002 0.017 0.084 0.00 0.04 16.29 0.04 64.58	RS045b     K-spar     0.39     0.000     0.029     0.029     0.000     0.01     16.68     0.00     64.90	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05     64.45	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74 0.02 63.81
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub>	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32 15.99 0.03 64.30 18.05	RS045 K-spar 0.51 0.004 0.004 0.004 0.004 0.004 0.004 0.000 0.16 16.34 0.000 64.59 17.39	RS045b K-spar 0.71 0.004 0.073 0.043 0.010 0.04 16.25 0.000 64.46 17.48	RS045b     K-spar     0.49     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90	RS045b K-spar 0.74 0.004 0.051 0.011 0.10 15.98 0.000 64.64 17.64	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71     17.62	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.020	RS045b K-spar 0.38 0.004 0.018 0.006 0.000 0.01 16.65 0.000 64.65 17.65	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61	RS045b K-spar 0.34 0.002 0.017 0.084 0.00 0.04 16.29 0.04 64.58 18.30	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05     64.45     18.45	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74 0.02 63.81 18.83
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub>	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32 15.99 0.03 64.30 18.05 0.000	RS045     K-spar     0.51     0.004     0.028     0.000     0.16     16.34     0.000     64.59     17.39     0.000	RS045b K-spar 0.71 0.004 0.073 0.043 0.010 0.04 16.25 0.000 64.46 17.48 0.01	RS045b K-spar 0.49 0.000 0.018 0.000 0.08 16.25 0.000 64.39 17.90 0.00	RS045b K-spar 0.74 0.004 0.062 0.051 0.011 0.10 15.98 0.000 64.64 17.64 0.000	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71     17.62     0.01	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000	RS045b K-spar 0.38 0.004 0.018 0.006 0.000 0.01 16.65 0.000 64.65 17.65 0.01	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01	RS045b     K-spar     0.34     0.002     0.017     0.084     0.00     0.04     16.29     0.04     64.58     18.30     0.00	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     0.02	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05     64.45     18.45     0.01	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74 0.02 63.81 18.83 0.000
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32 15.99 0.03 64.30 18.05 0.000 99.41	RS045 K-spar 0.51 0.004 0.004 0.028 0.000 0.16 16.34 0.000 64.59 17.39 0.000 99.02	RS045b K-spar 0.71 0.004 0.073 0.043 0.010 0.04 16.25 0.000 64.46 17.48 0.01 99.10	RS045b     K-spar     0.49     0.000     0.018     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90     0.00     99.14	RS045b     K-spar     0.74     0.004     0.051     0.011     0.10     15.98     0.000     64.64     17.64     0.000     99.23     0.067	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71     17.62     0.01     99.24	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000     99.27     0.052	RS045b K-spar 0.38 0.004 0.018 0.006 0.000 0.01 16.65 0.000 64.65 17.65 0.01 99.37	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01     99.40	RS045b K-spar 0.34 0.002 0.017 0.084 0.00 0.04 16.29 0.04 64.58 18.30 0.00 99.69	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     99.72	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05     64.45     18.45     0.01     99.75	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74 0.02 63.81 18.83 0.000 99.88
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32 15.99 0.03 64.30 18.05 0.000 99.41 0.052 0.020	RS045 K-spar 0.51 0.004 0.004 0.028 0.000 0.16 16.34 0.000 64.59 17.39 0.000 99.02 0.046	RS045b K-spar 0.71 0.004 0.073 0.043 0.010 0.04 16.25 0.000 64.46 17.48 0.01 99.10 0.064	RS045b     K-spar     0.49     0.000     0.018     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90     0.00     99.14     0.044	RS045b     K-spar     0.74     0.004     0.062     0.051     0.010     15.98     0.000     64.64     17.64     0.000     99.23     0.067     0.002	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71     17.62     0.01     99.24     0.058	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000     99.27     0.053     0.000	RS045b K-spar 0.38 0.004 0.018 0.006 0.000 0.01 16.65 0.000 64.65 17.65 0.01 99.37 0.034	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01     99.40     0.030	RS045b     K-spar     0.34     0.002     0.017     0.084     0.00     0.04     16.29     0.04     64.58     18.30     0.00     99.69     0.030	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     99.72     0.035	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05     64.45     18.45     0.01     99.75     0.059	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74 0.02 63.81 18.83 0.000 99.88 0.026
Slide No.     Phase     Na2O     MgO     FeO     CaO     MnO     BaO     K2O     SrO     SiO2     Al2O3     TiO2     Total     Na     Mg     Ca	RS045     K-spar     0.57     0.004     0.057     0.002     0.32     15.99     0.03     64.30     18.05     0.000     99.41     0.052     0.000     0.024	RS045     K-spar     0.51     0.004     0.028     0.000     0.16     16.34     0.000     64.59     17.39     0.000     99.02     0.046     0.000	RS045b     K-spar     0.71     0.004     0.073     0.043     0.010     0.04     16.25     0.000     64.46     17.48     0.01     99.10     0.064     0.000     0.002	RS045b     K-spar     0.49     0.000     0.018     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90     0.00     99.14     0.044     0.000	RS045b     K-spar     0.74     0.004     0.051     0.011     0.10     15.98     0.000     64.64     17.64     0.000     99.23     0.067     0.000     0.003	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71     17.62     0.01     99.24     0.058     0.000	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000     99.27     0.053     0.000     0.001	RS045b     K-spar     0.38     0.004     0.018     0.006     0.000     0.01     16.65     0.000     64.65     17.65     0.01     99.37     0.034     0.000	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01     99.40     0.030     0.000	RS045b     K-spar     0.34     0.002     0.017     0.084     0.00     0.04     16.29     0.04     64.58     18.30     0.00     99.69     0.030     0.000	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     99.72     0.035     0.000	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05     64.45     18.45     0.01     99.75     0.059     0.000	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74 0.02 63.81 18.83 0.000 99.88 0.026 0.000 0.005
Slide No.     Phase     Na2O     MgO     FeO     CaO     MnO     BaO     K2O     SrO     SiO2     Al2O3     TiO2     Total     Na     Mg     Ca     Ba	RS045     K-spar     0.57     0.004     0.057     0.005     0.02     0.32     15.99     0.03     64.30     18.05     0.000     99.41     0.052     0.000     0.004	RS045     K-spar     0.51     0.004     0.028     0.000     0.16     16.34     0.000     64.59     17.39     0.000     99.02     0.046     0.000     0.001	RS045b     K-spar     0.71     0.004     0.073     0.043     0.010     0.04     16.25     0.000     64.46     17.48     0.01     99.10     0.064     0.000     0.002     0.001	RS045b     K-spar     0.49     0.000     0.018     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90     0.000     99.14     0.044     0.000     0.001	RS045b     K-spar     0.74     0.004     0.051     0.011     0.10     15.98     0.000     64.64     17.64     0.000     99.23     0.067     0.000     0.003	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71     17.62     0.01     99.24     0.058     0.000     0.033     0.003	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000     99.27     0.053     0.000     0.001     0.001	RS045b     K-spar     0.38     0.004     0.018     0.006     0.001     16.65     0.000     64.65     17.65     0.01     99.37     0.034     0.000     0.034     0.000	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01     99.40     0.030     0.000     0.000	RS045b     K-spar     0.34     0.002     0.017     0.084     0.00     0.04     16.29     0.04     64.58     18.30     0.00     99.69     0.030     0.000     0.004	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     99.72     0.035     0.000     0.011	RS045b     K-spar     0.65     0.006     0.41     0.089     0.000     0.041     15.97     0.05     64.45     18.45     0.01     99.75     0.059     0.000     0.004	RS045b     K-spar     0.29     0.007     0.018     0.092     0.007     0.05     16.74     0.02     63.81     18.83     0.000     99.88     0.026     0.000     0.005
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba K	RS045 K-spar 0.57 0.004 0.057 0.075 0.002 0.32 15.99 0.03 64.30 18.05 0.000 99.41 0.052 0.000 0.004 0.006 0.051	RS045 K-spar 0.51 0.004 0.004 0.028 0.000 0.16 16.34 0.000 64.59 17.39 0.000 99.02 0.046 0.000 0.001 0.003 0.976	RS045b     K-spar     0.71     0.004     0.073     0.043     0.010     0.04     16.25     0.000     64.46     17.48     0.01     99.10     0.064     0.000     0.002     0.001     0.070	RS045b     K-spar     0.49     0.000     0.018     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90     0.00     99.14     0.044     0.000     0.001     0.002     0.958	RS045b     K-spar     0.74     0.004     0.051     0.011     0.10     15.98     0.000     64.64     17.64     0.000     99.23     0.067     0.000     0.003     0.002     0.951	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71     17.62     0.01     99.24     0.058     0.000     0.003     0.001     0.956	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000     99.27     0.053     0.000     0.001     0.009     0.953	RS045b     K-spar     0.38     0.004     0.018     0.006     0.000     0.01     16.65     0.000     64.65     17.65     0.01     99.37     0.034     0.000     0.000     0.000     0.000	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01     99.40     0.030     0.000     0.001     0.951	RS045b     K-spar     0.34     0.002     0.017     0.84     0.00     0.04     16.29     0.04     64.58     18.30     0.00     99.69     0.030     0.000     0.004     0.001     0.965	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     99.72     0.035     0.000     0.001     0.000	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05     64.45     18.45     0.01     99.75     0.000     0.004     0.005	RS045b K-spar 0.29 0.007 0.018 0.092 0.007 0.05 16.74 0.02 63.81 18.83 0.000 99.88 0.026 0.000 0.005 0.001 0.093
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba K Sr	RS045     K-spar     0.57     0.004     0.057     0.075     0.002     0.32     15.99     0.03     64.30     18.05     0.000     99.41     0.052     0.000     0.004     0.006     0.951     0.001	RS045     K-spar     0.51     0.004     0.004     0.028     0.000     0.16     16.34     0.000     64.59     17.39     0.000     99.02     0.046     0.000     0.001     0.003     0.976	RS045b     K-spar     0.71     0.004     0.073     0.043     0.010     0.04     16.25     0.000     64.46     17.48     0.01     99.10     0.064     0.002     0.001     0.970     0.090	RS045b     K-spar     0.49     0.000     0.018     0.000     0.018     0.000     0.018     0.000     0.018     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90     0.00     99.14     0.044     0.001     0.002     0.968     0.000	RS045b     K-spar     0.74     0.004     0.062     0.051     0.011     0.10     15.98     0.000     64.64     17.64     0.000     99.23     0.067     0.000     0.003     0.002     0.951     0.000	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.5     16.08     0.000     64.71     17.62     0.01     99.24     0.058     0.000     0.003     0.001     0.956     0.002	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000     99.27     0.053     0.000     0.001     0.009     0.953     0.000	RS045b     K-spar     0.38     0.004     0.018     0.006     0.000     0.01     16.65     0.000     64.65     17.65     0.01     99.37     0.034     0.000     0.000     0.000     0.000     0.991     0.000	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01     99.40     0.030     0.000     0.004	RS045b     K-spar     0.34     0.002     0.017     0.084     0.00     0.04     16.29     0.04     64.58     18.30     0.00     99.69     0.030     0.004     0.001	RS045b     K-spar     0.39     0.000     0.029     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     99.72     0.035     0.000     0.001     0.000     0.001	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.04     15.97     0.05     64.45     18.45     0.01     99.75     0.059     0.000     0.001	RS045b     K-spar     0.29     0.007     0.018     0.092     0.007     0.05     16.74     0.02     63.81     18.83     0.000     99.88     0.026     0.001     0.993     0.001
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba K Sr Si	RS045     K-spar     0.57     0.004     0.057     0.002     0.32     15.99     0.03     64.30     18.05     0.000     99.41     0.052     0.000     0.004     0.006     0.951     0.001     2 999	RS045     K-spar     0.51     0.004     0.028     0.000     0.16     16.34     0.000     64.59     17.39     0.000     99.02     0.046     0.000     0.001     0.003     0.976     0.000     3.023	RS045b     K-spar     0.71     0.004     0.073     0.043     0.010     0.04     16.25     0.000     64.46     17.48     0.01     99.10     0.064     0.002     0.001     0.970     0.000     3.015	RS045b     K-spar     0.49     0.000     0.018     0.000     0.018     0.000     0.018     0.000     0.018     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90     0.00     99.14     0.044     0.000     0.001     0.002     0.968     0.000     3.007	RS045b     K-spar     0.74     0.004     0.051     0.011     0.10     15.98     0.000     64.64     17.64     0.000     99.23     0.067     0.000     0.003     0.002     0.951     0.000     3.015	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.5     16.08     0.000     64.71     17.62     0.01     99.24     0.058     0.000     0.003     0.001     0.956     0.000     3.017	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000     99.27     0.053     0.000     0.001     0.009     0.953     0.000     3.017	RS045b     K-spar     0.38     0.004     0.018     0.006     0.000     0.01     16.65     0.000     64.65     17.65     0.01     99.37     0.034     0.000     0.000     0.000     0.991     0.000     3.015	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01     99.40     0.030     0.004     0.001     2.987	RS045b     K-spar     0.34     0.002     0.117     0.084     0.00     0.04     16.29     0.04     64.58     18.30     0.00     99.69     0.030     0.004     0.001     0.965     0.001     2.997	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     99.72     0.035     0.000     0.001     0.002     0.001     0.000     0.989     0.000     3.016	RS045b     K-spar     0.65     0.006     0.041     0.089     0.000     0.041     15.97     0.05     64.45     18.45     0.01     99.75     0.059     0.000     0.004     0.001     0.945     0.001     2.988	RS045b     K-spar     0.29     0.007     0.018     0.092     0.007     0.05     16.74     0.02     63.81     18.83     0.000     99.88     0.026     0.000     0.005     0.001     0.993     0.001     2.967
Slide No. Phase Na <sub>2</sub> O MgO FeO CaO MnO BaO K <sub>2</sub> O SrO SiO <sub>2</sub> Al <sub>2</sub> O <sub>3</sub> TiO <sub>2</sub> Total Na Mg Ca Ba K Sr Si Al	RS045     K-spar     0.57     0.004     0.057     0.075     0.002     0.32     15.99     0.03     64.30     18.05     0.000     99.41     0.052     0.000     0.004     0.005     0.004     0.005     0.004     0.005     0.951     0.001     2.999     0.992	RS045     K-spar     0.51     0.004     0.028     0.000     0.16     16.34     0.000     64.59     17.39     0.000     99.02     0.046     0.000     0.001     0.003     0.976     0.000     3.023     0.959	RS045b     K-spar     0.71     0.004     0.073     0.043     0.010     0.04     16.25     0.000     64.46     17.48     0.01     99.10     0.064     0.000     0.001     0.970     0.000     3.015     0.964	RS045b     K-spar     0.49     0.000     0.018     0.000     0.018     0.000     0.018     0.000     0.018     0.000     0.08     16.25     0.000     64.39     17.90     0.000     99.14     0.044     0.000     0.001     0.002     0.968     0.000     3.007     0.985	RS045b     K-spar     0.74     0.004     0.051     0.011     0.10     15.98     0.000     64.64     17.64     0.000     99.23     0.067     0.000     0.002     0.951     0.000     3.015     0.970	RS045b     K-spar     0.65     0.003     0.057     0.061     0.00     0.05     16.08     0.000     64.71     17.62     0.01     99.24     0.058     0.000     0.001     0.003     0.001     0.956     0.000     3.017     0.968	RS045b     K-spar     0.59     0.002     0.016     0.028     0.008     0.47     15.99     0.01     64.58     17.57     0.000     99.27     0.053     0.000     0.001     0.009     0.953     0.000     3.017     0.957	RS045b     K-spar     0.38     0.004     0.018     0.006     0.010     0.011     16.65     0.000     64.65     17.65     0.01     99.37     0.034     0.000     0.000     0.000     0.000     0.991     0.000     3.015	RS045b     K-spar     0.33     0.003     0.072     0.000     0.05     16.04     0.05     64.23     18.61     -0.01     99.40     0.030     0.000     0.001     0.951     0.001     2.987     1.020	RS045b     K-spar     0.34     0.002     0.117     0.084     0.00     0.04     16.29     0.04     64.58     18.30     0.00     99.69     0.030     0.000     0.001     0.965     0.001     2.997     1.001	RS045b     K-spar     0.39     0.000     0.029     0.000     0.01     16.68     0.00     64.90     17.68     0.00     99.72     0.035     0.000     0.001     0.000     0.989     0.000     3.016     0.968	RS045b     K-spar     0.65     0.006     0.41     0.089     0.000     0.041     15.97     0.05     64.45     18.45     0.01     99.75     0.059     0.000     0.001     0.945     0.001     0.945     0.001	RS045b     K-spar     0.29     0.007     0.018     0.092     0.007     0.05     16.74     0.02     63.81     18.83     0.000     99.88     0.026     0.000     0.005     0.001     0.993     0.001     2.967     1.032

wt% oxides							Sample						
Slide No.	RS045b	RS045b	RS045b	RS046	SV009								
Phase	K-spar	K-spar	K-spar	K-spar	plag								
Na <sub>2</sub> O	0.69	0.55	0.73	0.50	7.95	6.99	6.11	7.35	6.69	7.78	6.43	7.13	6.82
MgO	0.002	0.003	0.002	0.002	0.00	0.00	0.02	0.00	0.00	0.00	0.00	0.00	0.00
FeO	0.025	0.017	0.004	0.027	0.05	0.05	0.10	0.03	0.03	0.03	0.03	0.06	0.07
CaO	0.058	0.023	0.050	0.023	6.78	7.74	8.71	7.33	7.98	6.88	8.31	7.63	7.47
MnO	0.003	0.021	0.009	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01	-0.02	0.01
BaO	0.28	0.17	0.27	0.55	0.02	0.02	0.00	0.00	0.00	0.04	0.05	0.02	0.03
K <sub>2</sub> O	16.26	16.60	16.19	16.37	0.37	0.57	0.39	0.25	0.47	0.15	0.64	0.51	0.39
SrO	0.06	0.00	0.06	0.07	0.06	0.06	0.03	0.06	0.06	0.02	0.00	0.01	0.03
SiO <sub>2</sub>	64.91	65.34	65.06	64.57	58.87	58.87	58.93	58.88	58.73	57.94	58.29	58.50	59.10
Al <sub>2</sub> O <sub>3</sub>	18.27	17.87	18.31	17.56	26.84	26.84	26.45	26.60	26.70	26.54	26.79	26.34	26.50
TiO <sub>2</sub>	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.00	0.01
Total	100.56	100.59	100.69	99.67	100.94	101.14	100.68	100.44	100.63	99.38	100.53	100.18	100.42
Na	0.062	0.049	0.065	0.045	0.683	0.600	0.525	0.633	0.576	0.679	0.555	0.618	0.587
Mg	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.000	0.000	0.000	0.000	0.000	0.000
Ca	0.003	0.001	0.002	0.001	0.322	0.367	0.414	0.349	0.380	0.332	0.397	0.365	0.356
Ba	0.005	0.003	0.005	0.010	0.000	0.000	0.000	0.000	0.000	0.001	0.001	0.000	0.000
K	0.957	0.976	0.951	0.975	0.021	0.032	0.022	0.014	0.026	0.008	0.036	0.029	0.022
Sr	0.002	0.000	0.002	0.002	0.001	0.001	0.001	0.001	0.001	0.001	0.000	0.000	0.001
Si	2.995	3.012	2.996	3.013	2.609	2.606	2.615	2.617	2.609	2.606	2.597	2.614	2.626
Al	0.994	0.971	0.994	0.966	1.402	1.400	1.383	1.394	1.398	1.407	1.407	1.387	1.388
Sum	5.02	5.01	5.02	5.01	5.04	5.01	4.97	5.01	4.99	5.03	4.99	5.02	4.98
Slide No.	GS006												
Phase	Illite												
Na <sub>2</sub> O	0.11	0.10	0.09	0.12	0.08	0.09	0.09	0.11	0.09	0.09	0.11	0.10	0.09
MgO	0.66	0.67	0.68	0.65	0.66	0.66	0.66	0.67	0.67	0.66	0.66	0.66	0.67
FeO	1.08	1.10	1.08	1.11	1.09	1.11	1.12	1.14	1.12	1.11	1.09	1.12	1.13
CaO	0.14	0.14	0.14	0.14	0.14	0.14	0.15	0.15	0.15	0.15	0.15	0.15	0.15
MnO	0.000	0.03	0.000	0.00	0.000	0.000	0.000	0.01	0.02	0.01	0.02	0.000	0.00
BaO	0.000	0.000	0.00	0.02	0.000	0.04	0.00	0.00	0.00	0.04	0.03	0.01	-0.04
K <sub>2</sub> O	8.67	8.85	8.66	9.03	8.68	8.85	8.83	8.71	8.93	8.89	8.90	9.01	8.77
SrO	0.000	0.02	0.03	0.02	0.000	0.01	0.000	0.000	0.000	0.000	0.000	0.000	0.000
SiO <sub>2</sub>	47.62	47.46	47.72	47.49	47.70	47.19	47.23	47.97	47.56	47.37	47.80	47.51	47.63
Al <sub>2</sub> O <sub>3</sub>	19.83	20.01	20.04	20.13	20.00	19.96	20.07	20.04	20.22	20.00	19.99	20.09	20.07
TiO <sub>2</sub>	0.02	0.03	0.03	0.03	0.02	0.03	0.02	0.03	0.02	0.02	0.03	0.02	0.02
Total	78.13	78.42	78.47	78.74	78.38	78.09	78.17	78.81	78.78	78.34	78.76	78.67	78.54
Na	0.034	0.032	0.027	0.038	0.026	0.029	0.028	0.032	0.027	0.028	0.035	0.031	0.029
Mg	0.157	0.160	0.161	0.154	0.156	0.158	0.158	0.158	0.159	0.158	0.155	0.156	0.158
Fe	0.143	0.147	0.144	0.147	0.145	0.149	0.150	0.150	0.149	0.148	0.144	0.149	0.150
Ca	0.023	0.024	0.024	0.024	0.024	0.024	0.025	0.025	0.025	0.025	0.026	0.026	0.026
К	1.763	1.798	1.755	1.829	1.761	1.807	1.799	1.756	1.806	1.809	1.799	1.826	1.778
Sr	0.000	0.002	0.003	0.002	0.000	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000
51	7.593	7.557	7.576	7.543	7.581	7.551	7.543	7.585	7.540	7.554	7.577	7.549	7.564
Al	3.727	3.756	3.750	3.768	3.746	3.764	3.778	3.735	3.779	3.759	3.734	3.762	3.757
Sum	13.4	13.5	13.4	13.5	13.4	13.5	13.5	13.4	13.5	13.5	13.5	13.5	13.5

Shile ho.SYU00	wt% oxides							Sample						
Phase   Suxt   Suxt <thsuxt< th="">   Suxt   Suxt   <th< th=""><th>Slide No.</th><th>SV009</th><th><u>S</u>V009</th><th><u>S</u>V009</th><th><u>S</u>V009</th><th><u>S</u>V009</th><th><u>S</u>V009</th><th>SV009</th><th><u>S</u>V009</th><th>SV009</th><th>SV009</th><th><u>S</u>V009</th><th>SV009</th><th><u>S</u>V009</th></th<></thsuxt<>	Slide No.	SV009	<u>S</u> V009	SV009	<u>S</u> V009	SV009	SV009	<u>S</u> V009	SV009	<u>S</u> V009				
Na.00.1810.2840.1990.1840.2140.1940.1940.1820.1830.1730.1710.194MeO1.7271.8633.7003.7103.7143.7143.7143.7143.7183.7073.6557.7775.6221.6751.675FeO1.6901.6900.0000	Phase	Smct	Smet	Smet	Smct	Smet	Smet	Smct	Smct	Smct	Smct	Smct	Smct	Smet
nypo12773.853.7013.7143.7143.7143.8193.8193.6353.7173.8223.8671.728Fo16921.6071.7151.7291.7121.6841.7771.6451.7261.6861.7351.7351.738Cuo0.1030.1000.00<	Na <sub>2</sub> O	0.181	0.226	0.199	0.186	0.214	0.168	0.194	0.182	0.163	0.183	0.178	0.171	0.184
Pred1.4921.4971.7131.7131.6841.771.4841.7261.6861.7351.7351.7381.738CaO0.1880.1510.1520.1530.1540.1550.1560.1560.1560.1570.1580.1500.000BaO0.0140.0250.0050.0000.0000.0040.0060.0000.0000.0000.0060.0000.	MgO	3.727	3.685	3.701	3.743	3.714	3.734	3.819	3.739	3.635	3.717	3.632	3.667	3.678
Ca00.1480.1510.1520.1530.1530.1550.1560.1560.1570.1580.1580.1580.1580.1590.	FeO	1.692	1.667	1.715	1.729	1.712	1.684	1.777	1.645	1.726	1.686	1.705	1.723	1.738
Made0.0130.0160.0000.0000.0000.0000.0010.0130.0040.0010.0000.0000.0000.000BoC0.0140.0130.0060.000 <th>CaO</th> <th>0.148</th> <th>0.151</th> <th>0.152</th> <th>0.153</th> <th>0.154</th> <th>0.155</th> <th>0.155</th> <th>0.156</th> <th>0.156</th> <th>0.157</th> <th>0.158</th> <th>0.158</th> <th>0.158</th>	CaO	0.148	0.151	0.152	0.153	0.154	0.155	0.155	0.156	0.156	0.157	0.158	0.158	0.158
Be00.0410.0250.0060.0000.0000.0130.0000.0000.0000.0010.0000.0010.0000.0010.0000.0010.0000.0010.0000.0010.0000.0000.0010.0000.	MnO	0.013	0.016	0.000	0.000	0.002	0.000	0.004	-0.026	0.004	0.000	0.009	0.000	0.000
Ko03.1853.1973.1993.1993.1933.1733.2103.1803.2073.1313.1903.180Sr00.0000.0000.0000.0000.0000.0000.0100.0160.0010.0000.000SiO5.7075.73653.87753.87728.5828.8827.97527.87782.7428.0528.8827.97527.87782.7428.0528.0827.97527.87793.6795.6095.2095.2094.7795.6095.2095.2094.7795.6095.2095.2094.7795.6095.2095.2094.7795.6095.2095.2094.7795.6095.2094.7294.7095.2095.2095.2095.2095.2094.7795.6095.2095.2094.72Tota0.020.030.02 <t< th=""><th>BaO</th><th>0.041</th><th>0.025</th><th>0.006</th><th>0.000</th><th>0.000</th><th>0.014</th><th>0.013</th><th>-0.006</th><th>0.008</th><th>0.021</th><th>0.002</th><th>0.000</th><th>0.049</th></t<>	BaO	0.041	0.025	0.006	0.000	0.000	0.014	0.013	-0.006	0.008	0.021	0.002	0.000	0.049
Sr00.0000.0000.0000.0000.0000.0000.0010.0160.0010.	K <sub>2</sub> O	3.185	3.205	3.197	3.199	3.195	3.197	3.173	3.210	3.189	3.207	3.153	3.193	3.180
SiO155.7056.4056.8456.34956.37056.3655.84055.84055.46756.36057.47358.34055.84055.84056.36756.36757.47358.36028.03028.03028.12328.01710028.02028.12328.01710028.02028.12328	SrO	0.000	0.000	0.000	0.000	0.000	0.010	0.000	0.000	0.015	0.016	0.003	0.000	0.000
Alob28.00227.98028.08828.07328.06027.97527.87528.27428.07528.08027.97928.1228.017Trop0.0220.0290.0240.0140.0210.0240.0210.0210.0210.0240.0220.0260.022Toial94.71095.57095.57095.30095.32095.32095.32095.32097.7795.6300.020.0<	SiO <sub>2</sub>	55.730	56.601	56.018	56.264	56.184	56.349	55.377	56.336	55.804	56.540	54.425	56.032	55.467
TO2,0.0220.0240.0240.0240.0240.0240.0240.0240.0240.0220.0250.022Tatal94.71095.57495.50595.30895.23695.30094.38795.52794.77795.63093.26695.02594.443Na0.020.0320.0320.020.020.0200.020.00	$Al_2O_3$	28.002	27.986	28.088	28.073	28.060	27.975	27.875	28.274	28.056	28.083	27.979	28.123	28.017
Total94.71095.7395.06395.30895.30894.33094.38795.32794.77795.63093.26695.20294.443Na0.020.030.02 <th>TiO<sub>2</sub></th> <th>0.022</th> <th>0.029</th> <th>0.024</th> <th>0.018</th> <th>0.021</th> <th>0.021</th> <th>0.024</th> <th>0.020</th> <th>0.021</th> <th>0.024</th> <th>0.022</th> <th>0.026</th> <th>0.022</th>	TiO <sub>2</sub>	0.022	0.029	0.024	0.018	0.021	0.021	0.024	0.020	0.021	0.024	0.022	0.026	0.022
Na0.020.030.020.030.020.020.020.020.020.020.020.020.02Mg0.360.350.360.360.360.360.370.360.350.350.360.360.36Fe0.0910.0890.0920.0900.0900.0900.0900.0900.0900.0900.0900.0910.0110.0	Total	94.710	95.574	95.065	95.308	95.236	95.300	94.387	95.527	94.777	95.630	93.266	95.025	94.443
Mg0.360.350.360.360.360.370.360.350.360.350.360.350.360.350.360.36Fe0.0910.0910.0920.0920.0910.0910.011 <th< th=""><th>Na</th><th>0.02</th><th>0.03</th><th>0.02</th><th>0.02</th><th>0.03</th><th>0.02</th><th>0.02</th><th>0.02</th><th>0.02</th><th>0.02</th><th>0.02</th><th>0.02</th><th>0.02</th></th<>	Na	0.02	0.03	0.02	0.02	0.03	0.02	0.02	0.02	0.02	0.02	0.02	0.02	0.02
Fe0.0910.0890.0920.0930.0920.0930.0940.0930.0940.0930.094Ca0.0100.0100.0100.0100.0110.0010.000<	Mg	0.36	0.35	0.35	0.36	0.36	0.36	0.37	0.36	0.35	0.35	0.36	0.35	0.36
Ca0.0100.0100.0100.0100.0110.0100.0000.0	Fe	0.091	0.089	0.092	0.093	0.092	0.090	0.096	0.088	0.093	0.090	0.094	0.093	0.094
Nn0.0010.0010.0000.0	Ca	0.010	0.010	0.010	0.010	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011	0.011
Ba0.0010.0010.0000.0000.0000.0000.0000.0000.0010.0010.0000.0000.001K0.260.212.132.132.132.132.132.132.132.142.132.142.132.142.142.132.122.172.132.142.14Sund6.476.406.476.406.476.406.476.406.476.406.476.	Mn	0.001	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.000	0.000
K0.26<	Ba	0.001	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.000	0.000	0.001
Si3.603.623.603.613.613.613.593.603.603.613.573.603.59Al2.132.112.132.122.112.132.132.132.122.172.132.14Sum6.486.476.486.476.486.476.496.476.476.476.496.476.496.476.496.476.496.476.496.476.496.476.496.476.496.476.496.476.496.476.48Suide No.Sv002Sv002Sv002Sv002Sv002GR007	К	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26	0.26
Al2.132.112.132.122.122.112.132.132.132.122.172.132.14Sum6.486.476.486.476.486.476.496.476.476.476.496.476.48Sude No.Sv02Sv02Sv02Sv02Sv02Sv02Sv02Sv02GR07	Si	3.60	3.62	3.60	3.61	3.61	3.61	3.59	3.60	3.60	3.61	3.57	3.60	3.59
Sum   6.48   6.47   6.48   6.47   6.49   6.47   6.47   6.47   6.49   6.47   6.48     Slide No.   SV002   SV002   SV002   SV002   SV002   SV002   SV002   SV002   SV002   GR007	Al	2.13	2.11	2.13	2.12	2.12	2.11	2.13	2.13	2.13	2.12	2.17	2.13	2.14
Silde No.   SV002   SV002   SV002   SV002   SV002   SV002   SV002   GR007	Sum	6.48	6.47	6.48	6.47	6.48	6.47	6.49	6.47	6.47	6.47	6.49	6.47	6.48
Silde No.   SV002   SV002   SV002   SV002   SV002   SV002   GR007   GR07   GR07 <tho< th=""><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th><th></th></tho<>														
Phase   Dolo   Dolo   Dolo   Dolo   Dolo   Cc	Slide No.	SV002	SV002	SV002	SV002	SV002	SV002	GR007	GR007	GR007	GR007	GR007	GR007	GR007
Na <sub>2</sub> O   0.000   0.013   0.003   0.022   0.025   0.039   0.004   0.000   0.008   0.002   0.000   0.000     MgO   20.68   20.05   20.34   20.95   22.30   21.34   0.24   0.25   0.09   0.41   0.10   0.36   0.12     FeO   0.05   0.22   0.12   0.18   0.26   0.31   0.02   0.01   0.02   0.18   0.10   0.46   0.01     CaO   32.02   30.78   31.92   30.33   30.65   30.13   55.14   56.51   56.08   57.44   56.14   52.37   54.60     MnO   0.032   0.166   0.002   0.000   0.023   0.045   0.031   0.168   0.738   0.000     KgO   0.031   0.123   0.057   0.003   0.012   0.025   0.008   0.034   0.074   0.005   0.025   0.020     BaO   0.000   0.001   0.002   0.001   0.000 <th>Phase</th> <th>Dolo</th> <th>Dolo</th> <th>Dolo</th> <th>Dolo</th> <th>Dolo</th> <th>Dolo</th> <th>Cc</th> <th>Cc</th> <th>Cc</th> <th>Cc</th> <th>Cc</th> <th>Cc</th> <th>Cc</th>	Phase	Dolo	Dolo	Dolo	Dolo	Dolo	Dolo	Cc	Cc	Cc	Cc	Cc	Cc	Cc
MgO 20.68 20.05 20.34 20.95 22.30 21.34 0.24 0.25 0.09 0.41 0.10 0.36 0.12   FeO 0.05 0.22 0.12 0.18 0.26 0.31 0.02 0.01 0.02 0.18 0.10 0.46 0.01   CaO 32.02 30.78 31.92 30.33 30.65 30.13 55.14 56.08 57.44 56.14 52.37 54.60   MnO 0.032 0.166 0.002 0.000 0.025 0.013 0.178 0.068 0.268 0.133 0.168 0.738 0.000   K <sub>2</sub> O 0.031 0.123 0.057 0.003 0.018 0.025 0.001 0.046 0.127 0.057 0.077 0.041   SrO 0.033 0.000 0.012 0.000 0.016 -0.045 0.019 0.054 0.000 0.021   BaO 0.000 0.001 0.002 0.002 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	Na <sub>2</sub> O	0.000	0.013	0.003	0.022	0.025	0.039	0.004	0.000	0.008	0.002	0.002	0.000	0.000
FeO   0.05   0.22   0.12   0.18   0.26   0.31   0.02   0.01   0.02   0.18   0.10   0.46   0.01     CaO   32.02   30.78   31.92   30.33   30.65   30.13   55.14   56.51   56.08   57.44   56.14   52.37   54.60     MnO   0.032   0.166   0.002   0.000   0.025   0.013   0.178   0.068   0.268   0.133   0.168   0.738   0.000     K2O   0.031   0.123   0.057   0.003   0.018   0.022   0.045   0.031   0.046   0.127   0.057   0.077   0.041     SrO   0.033   0.000   0.016   0.002   0.000   0.012   0.025   0.008   0.034   0.074   0.005   0.025   0.020     BaO   0.000   0.001   0.002   0.000   0.001   0.016   0.034   0.074   0.053   0.025   0.202     BaO   0.000   0.00	MgO	20.68	20.05	20.34	20.95	22.30	21.34	0.24	0.25	0.09	0.41	0.10	0.36	0.12
CaO   32.02   30.78   31.92   30.33   30.65   30.13   55.14   56.08   57.44   56.14   52.37   54.60     MnO   0.032   0.166   0.002   0.000   0.025   0.013   0.178   0.068   0.268   0.133   0.168   0.738   0.000     K2O   0.031   0.123   0.057   0.003   0.018   0.025   0.031   0.046   0.127   0.057   0.077   0.041     SrO   0.033   0.000   0.012   0.025   0.008   0.034   0.074   0.005   0.020   0.021     BaO   0.000   0.042   0.000   0.021   0.000   0.016   -0.045   0.019   0.054   0.000   0.020     Co2   47.14   48.64   47.50   48.51   46.71   48.14   44.17   43.05   43.34   41.40   43.27   45.38   45.04     Na   0.000   0.001   0.002   0.002   0.000   0.000	FeO	0.05	0.22	0.12	0.18	0.26	0.31	0.02	0.01	0.02	0.18	0.10	0.46	0.01
MnO   0.032   0.166   0.002   0.000   0.025   0.013   0.178   0.068   0.268   0.133   0.168   0.738   0.000     K_O   0.031   0.123   0.057   0.003   0.018   0.023   0.045   0.031   0.046   0.127   0.057   0.077   0.041     SrO   0.033   0.000   0.016   0.005   0.000   0.012   0.025   0.008   0.034   0.074   0.005   0.025   0.020     BaO   0.000   0.000   0.042   0.000   0.011   0.000   0.016   -0.045   0.019   0.054   0.000   0.000     CO2   47.14   48.64   47.50   48.51   46.71   48.14   44.17   43.05   43.34   41.40   43.27   45.38   45.04     Total   52.86   51.36   52.50   51.49   53.29   51.86   55.84   56.95   56.66   58.60   56.73   54.62   54.90     Ma	CaO	32.02	30.78	31.92	30.33	30.65	30.13	55.14	56.51	56.08	57.44	56.14	52.37	54.60
K <sub>2</sub> O 0.031 0.123 0.057 0.003 0.018 0.023 0.031 0.046 0.127 0.057 0.077 0.041   SrO 0.033 0.000 0.016 0.005 0.000 0.012 0.025 0.008 0.034 0.074 0.005 0.025 0.000   BaO 0.000 0.000 0.042 0.000 0.021 0.000 0.016 -0.045 0.019 0.054 0.000 0.000   CO2 47.14 48.64 47.50 48.51 46.71 48.14 44.17 43.05 43.34 41.40 43.27 45.38 45.04   Total 52.86 51.36 52.50 51.49 53.29 51.86 55.84 56.95 56.66 58.60 56.73 54.62 54.96   Na 0.000 0.001 0.002 0.002 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	MnO	0.032	0.166	0.002	0.000	0.025	0.013	0.178	0.068	0.268	0.133	0.168	0.738	0.000
SrO 0.033 0.000 0.016 0.005 0.000 0.012 0.025 0.008 0.034 0.074 0.005 0.025 0.020   BaO 0.000 0.000 0.042 0.000 0.021 0.000 0.016 -0.045 0.019 0.054 0.000 0.000   CO2 47.14 48.64 47.50 48.51 46.71 48.14 44.17 43.05 43.34 41.40 43.27 45.38 45.04   Total 52.86 51.36 52.50 51.49 53.29 51.86 55.84 56.95 56.66 58.60 56.73 54.62 54.96   Na 0.000 0.001 0.002 0.002 0.000	K <sub>2</sub> O	0.031	0.123	0.057	0.003	0.018	0.023	0.045	0.031	0.046	0.127	0.057	0.077	0.041
BaO 0.000 0.000 0.042 0.000 0.021 0.000 0.016 -0.045 0.019 0.054 0.000 0.000   CO2 47.14 48.64 47.50 48.51 46.71 48.14 44.17 43.05 43.34 41.40 43.27 45.38 45.04   Total 52.86 51.36 52.50 51.49 53.29 51.86 55.84 56.95 56.66 58.60 56.73 54.62 54.96   Na 0.000 0.001 0.000 0.002 0.002 0.000	SrO	0.033	0.000	0.016	0.005	0.000	0.012	0.025	0.008	0.034	0.074	0.005	0.025	0.020
CO2 47.14 48.64 47.50 48.51 46.71 48.14 44.17 43.05 43.34 41.40 43.27 43.28 45.04   Total 52.86 51.36 52.50 51.49 53.29 51.86 55.84 56.95 56.66 58.60 56.73 54.62 54.96   Na 0.000 0.001 0.000 0.001 0.002 0.002 0.000 <th>BaO</th> <th>0.000</th> <th>0.000</th> <th>0.042</th> <th>0.000</th> <th>0.021</th> <th>0.000</th> <th>0.000</th> <th>0.016</th> <th>-0.045</th> <th>0.019</th> <th>0.054</th> <th>0.000</th> <th>0.000</th>	BaO	0.000	0.000	0.042	0.000	0.021	0.000	0.000	0.016	-0.045	0.019	0.054	0.000	0.000
Total   52.86   51.36   52.30   51.39   53.29   51.86   55.84   56.95   56.66   58.60   56.73   54.62   54.96     Na   0.000   0.001   0.000   0.001   0.002   0.002   0.000<		47.14	48.64	47.50	48.51	46.71	48.14	44.17	43.05	43.34	41.40	43.27	45.38	45.04
Na   0.000   0.001   0.001   0.002   0.002   0.000   0.	Total	52.86	51.36	52.50	51.49	53.29	51.86	55.84	56.95	56.66	58.60	56.73	54.62	54.96
Mg   0.934   0.915   0.936   0.934   1.029   0.975   0.006   0.006   0.002   0.010   0.003   0.009   0.009     Fe   0.001   0.006   0.003   0.004   0.007   0.008   0.000   0.000   0.003   0.001   0.006   0.003   0.001   0.006   0.000   0.000   0.003   0.001   0.006   0.003   0.001   0.006   0.000   0.000   0.003   0.001   0.006   0.000   0.000   0.001   0.006   0.000   0.001   0.006   0.000   0.001   0.001   0.001   0.002   0.002   0.002   0.010   0.000     K   0.001   0.004   0.002   0.002   0.001   0.001   0.001   0.001   0.004   0.002   0.002   0.002   0.000   0.000     K   0.001   0.002   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.000   0.	Na	0.000	0.001	0.000	0.001	0.002	0.002	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Fe 0.001 0.006 0.003 0.004 0.007 0.008 0.000 0.000 0.003 0.001 0.006 0.006   Ca 1.061 1.009 1.056 0.993 1.016 0.989 0.983 1.017 1.008 1.051 1.010 0.927 0.966   Mn 0.001 0.004 0.000 0.001 0.000 0.001 0.002 0.002 0.010 0.000   K 0.001 0.005 0.002 0.000 0.001 0.001 0.001 0.001 0.002 0.002 0.001 0.000   Sr 0.001 0.000 0.	Mg	0.954	0.915	0.936	0.954	1.029	0.975	0.006	0.006	0.002	0.010	0.003	0.009	0.003
Ca 1.001 1.000 1.000 0.000 0.000 0.989 0.985 1.017 1.008 1.011 1.010 0.927 0.966   Mn 0.001 0.004 0.000 0.000 0.001 0.000 0.003 0.001 0.002 0.002 0.010 0.000   K 0.001 0.005 0.002 0.000 0.001 0.000	ге	1.001	1.000	1.054	0.004	1.016	0.008	0.000	1.017	1.000	1.051	1.010	0.000	0.000
Kin   0.001   0.004   0.000   0.000   0.001   0.003   0.001   0.002   0.002   0.002   0.001   0.000   0.000     K   0.001   0.005   0.000   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.001   0.002   0.002   0.002   0.000   0.000     Sr   0.001   0.000	ua Mu	0.001	0.004	0.000	0.993	0.001	0.989	0.985	0.001	0.004	0.002	0.002	0.927	0.900
K   0.001   0.002   0.002   0.001   0.000   0.0	win	0.001	0.004	0.000	0.000	0.001	0.000	0.003	0.001	0.004	0.002	0.002	0.010	0.000
Ba   0.001   0.000   0.	л с.,	0.001	0.000	0.002	0.000	0.001	0.001	0.001	0.001	0.001	0.003	0.001	0.002	0.001
Da   0.000   0.	or	0.001	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.001	0.000	0.000	0.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Ба	1.001	0.000	2,002	2.024	1.072	0.000	1.004	0.000	0.000	0.000	0.000	1.022	1.015
	CU <sub>3</sub>	1.991	2.032	2.002	2.024	1.973	2.013	1.004	0.987	0.992	0.966	0.991	1.023	1.015

Table B.II. continued

### **B.3.** Petrophysical Data: Navajo Sandstone

	(ft/	'day)		%				(f	t/day)	%		
ре	rm	Hyd	r Cond	Poro	Ref		ре	erm	Hydr	Cond	Poro	Ref
Hor	Ver	Hor	Ver				Hor	Ver	Hor	Ver		
1.8	7.9	11	9.9	30.8	1				0.58	0.055	20.9	1
		1.2	0.18	12.8	1					1.6	26.8	1
1.6	1.1	0.72	0.46	23.2	1				0.7	0.089		1
				13.7	1					1.5	25.2	1
				15.5	1				0.34	0.27	21.3	1
				13.3	1		0.64	0.54			24.3	1
			0.011	13	1						13.4	1
			1.3	15.1	1			0.017			14.3	1
				12.5	1			1.2		0.75	21.3	1
0.063	0.039	0.038	0.024	11.6	1						23	1
	2.7		0.93	18	1		1.3	1.2	0.52		21.4	1
				28.6	1		1.2				18	1
3.5	4.7	2.8		20.7	1				2.2			1
4.7	2.4			18.5	1				0.64			1
3.8				20	1				0.89		22.8	1
8.7				20.7	1				0.56		21.9	1
9.6	8.4	5.8		20	1				0.78	0.52	20.5	1
1.2		0.19		20.6	1				0.41	0.52	20.7	1
	0.83		0.22	19.2	1				2.5		25.9	1
				21	1				0.33	0.17	20.4	1
3.1	0.79	0.55		22.1	1				0.47	0.12	20.4	1
				15.6	1				1		24.3	1
	3.1		1.3	19.1	1				1.4		25	1
0.034	0.032	0.013	0.0041	14.1	1				1.4		25.9	1
				10.5	1				0.17	0.067	22.3	1
				19.8	1				0.45	0.43	22.3	1
				21.2	1				0.78		22	1
		0.91		20.7	1				0.66		23.1	1
				27.4	1				0.4		24.1	1
2.8	2.1	1.8	1.2	26.8	1				0.015	0.035	22.5	1
	2.6		42	15.8	1				0.38	0.25	22.5	1
				17.6	1				0.55		24.7	1
0.43	0.29			17.5	1				0.43		25.2	1
				22	1					0.24	13.8	1
3.7	0.7	1.5		21.2	1					1.1	26.1	1
				19.9	1				0.0079	0.021		1
0.76				16.5	1					1.7	13.9	1
2.4				16.4	1					1.5	20.9	1
1.7				15.9	1				2.7	0.91	17.4	1
2.4				12.7	1					0.91	14	1
2.3				14.1	1				0.0022	0.0011	16.1	1

**Table B.B-III** Porosity, permeability and hydraulic conductivity of the Navajo Sandstone, compiled from Weigel,  $(1986)^1$  and Hood and Patterson,  $(1984)^2$ . Abbreviations: perm = permability, Hydr Cond = hydraulic conductivity, Poro = effective porosity, Hor = horizontal, Ver = vertical, Ref = reference.

	(1	ft/day)		%	
ре	rm	Hydr	Cond	Poro	Ref
Hor	Ver	Hor	Ver		
		0.88	0.46	14.2	1
		0.43	0.25	25.6	1
		5.2		26.5	1
		1.4			1
5.5	6.5	2.4	2.4	28.3	1
		1.1			1
		0.93			1
		0.49			1
		1			1
				25	1
		0.0022		22.1	1
		0.64	0.41	23	1
		0.38	0.22	26	1
		2	0.24		1
		7.5	0.53	22	1
		0.78	0.27		1
		7.6	0.5	22	1
				22	1
		3.4	2	25	1
		3.2	0.7	15	1
		1.9	5	24	1
		3	0.8	17	1
		1.6	3	15	1
		2.4			1
		0.33			1
		1.7			1
		0.006			1
		0.055			1
		0.21			1
		4.2	2.2	28	1
				30	1
		5	2.3	19	1
		4.5	4.6	27	1
		0.002	0.005	15	1
		0.12	0.099	11	1
			0.17	14	1
		6.1	4.5	30	1
		0.3	0.11	11	1
		0.034		11.5	2
		0.029		11.4	2
		2.5		19.4	2
		1.6			2
				18.5	2
		5.1		19.6	2
		0.17		20.6	2
		0.49		22.1	2

	(	ft/day)		%	
pe	rm	Hydr Co	ond	Poro	Ref
Hor	Ver	Hor	Ver		
		0.011		14.1	2
		0.0089		13.8	2
		< 0.00002		6.7	2
		< 0.00002		6.7	2
		0.8		20.7	2
		1.6		26.3	2
		1.5			2
				17.5	2
		1.4		21.2	2
				24.3	2
				24.1	2
				23.1	2
				22.8	2
		0.46		21.4	2

Table B.III continued

#### **B.4. Sample Details**

**Table B.B-IV** Sample localities, rock types and analyses. Abbreviations: Lat = latitude, Long = longitude, Alt = altitude, PWD = powder, TS = thin section, MW = micro-wafer, XRF = x-ray florescence. 'Lithology' describes the unit/formation type and whether the samples are of the bulk host rock (Rock), a vein (vein) or a travertine (trav). 'Type' describes whether the sample is bleached (B), unbleached/red (R) or obviously bleached and carbonate cemented Y-B.

Code	Lat.	Long.	Alt (m)	Location	PWD	TS	MW	XRF	Lithology		Туре
RS001	38.96618	-110.22624	*	Green River Airport Well	х				Travertine	Trav	N/A
RS004	38.96618	-110.22624	*	Green River Airport Well	х				Travertine	Trav	N/A
RS005	38.76350	-110.12744	*	Chaffin Ranch	х				Travertine	Trav	N/A
RS006	38.86272	-110.10125	*	Tenmile Geyser	х				Travertine	Trav	N/A
RS007	38.85873	-110.07277	*	Torreys Spring	х				Travertine	Trav	N/A
RS020	38.98344	-110.53357	1680	San Rafael River	х	х			White Rim	Rock	В
RS021	38.98347	-110.53360	1657	San Rafael Swell	х	х			White Rim	Rock	В
RS024	38.93354	-110.45022	1454	San Rafael Swell	х	х			White Rim	Rock	R-B
RS026	38.93353	-110.41688	1409	Black Dragon Canyon	х	х		х	Navajo Sst	Rock	R
RS027	38.92959	-110.41925	1314	Black Dragon Canyon	х	х			Entrada Sst	Rock	Y-B
RS029	38.92959	-110.41925	1318	Black Dragon Canyon	х				Entrada Sst	Rock	R
RS041	38.94825	-110.44040	*	Black Dragon Canyon	х				Wingate Sst.	Rock	В
RS044	38.94586	-110.43100	1345	Black Dragon Canyon		х		х	Navajo Sst	Rock	В
RS045a	38.94544	-110.42973	1341	Black Dragon Canyon		х		х	Navajo Sst	Rock	R
RS045b	38.94544	-110.42973	1341	Black Dragon Canyon		х			Navajo Sst	Rock	R
RS046	38.94548	-110.42975	*	Black Dragon Canyon		х		х	Navajo Sst	Rock	R
RS048	38.87023	-110.11190	1248	Near Big Bubbling Spring		х			Entrada Sst	Rock	Y-B
RS052a	38.86842	-110.10816	1286	Near Big Bubbling Spring	х	х			Entrada Sst	Rock	Y-B
RS052b	38.86842	-110.10816	1286	Near Big Bubbling Spring	х	х			Entrada Sst	Rock	Y-B
RS053	38.86622	-110.10348	1263	Tenmile Butte	х	х			Entrada Sst	Rock	В
RS054a	38.86824	-110.10208	1269	Tenmile Butte	х				Entrada Sst	Vein	В
RS055	38.86717	-110.09952	1261	Tenmile Butte	х	х			Entrada Sst	Rock	В
RS056a	38.86696	-110.09933	1268	Tenmile Butte	х	х		х	Entrada Sst	Vein	В
RS056b	38.86696	-110.09933	1268	Tenmile Butte	х	х			Entrada Sst	Rock	В
RS057	38.86756	-110.10040	1278	Tenmile Butte	х	х			Entrada Sst	Rock	В
RS058	38.86770	-110.10076	1268	Tenmile Butte	х	х			Entrada Sst	Rock	В

Table B.IV continued

Code	Lat.	Long.	Alt (m)	Location	Location PWD TS MW XRF I		Litholog	Lithology			
RS059	38.86770	-110.10076	1268	Tenmile Butte					Entrada Sst	Rock	R
RS060	38.86731	-110.10248	1257	Tenmile Butte	Х	х		х	Entrada Sst	Rock	R-B
RS061	38.86731	-110.10248	1257	Tenmile Butte	Х	х			Entrada Sst	Rock	В
RS062	38.86780	-110.10178	*	Tenmile Butte	х	х			Entrada Sst	Rock	В
RS063	38.86643	-110.10234	*	Tenmile Butte	х	х			Entrada Sst	Rock	В
RS065	38.86493	-110.09981	1277	Tenmile Butte					Entrada Sst	Rock	В
RS066	38.86488	-110.09982	1267	Tenmile Butte	х	х	х		Entrada Sst	Vein	В
RS067	38.86487	-110.09982	1266	Tenmile Butte	х				Entrada Sst	Vein	В
RS068	38.86550	-110.10105	1262	Tenmile Butte	х				Entrada Sst	Rock	В
RS069a	38.86532	-110.10098	1277	Tenmile Butte	х	х	х		Entrada Sst	Vein	В
RS069b	38.86532	-110.10098	*	Tenmile Butte		х			Entrada Sst	Vein	В
RS070	38.86514	-110.10070	1277	Tenmile Butte	х	х			Entrada Sst	Vein	В
RS071a	38.86543	-110.10160	1274	Tenmile Butte	х	х	х		Entrada Sst	Vein	В
RS071b	38.86563	-110.10152	1274	Tenmile Butte	х	х	х		Entrada Sst	Vein	В
RS071c	38.86563	-110.10139	1274	Tenmile Butte	х		х		Entrada Sst	Vein	В
RS072	38.86563	-110.10139	1274	Tenmile Butte	х				Entrada Sst	Vein	В
RS073	38.86655	-110.10241	1281	Tenmile Butte	х	х	х		Entrada Sst	Rock	В
RS090a	38.87023	-110.11190	*	Big Bubbling Spring	х	х	х		Entrada Sst	Vein	R-B
RS090b	38.87023	-110.11190	*	Big Bubbling Spring	х				Entrada Sst	Vein	R-B
RS090c	38.87023	-110.11190	*	Big Bubbling Spring	х				Entrada Sst	Vein	R-B
RS090d	38.87023	-110.11190	*	Big Bubbling Spring	х				Entrada Sst	Vein	R-B
RS091a	38.87265	-110.11662	*	Small Bubbling Spring	х				Travertine	Trav	N/A
RS091b	38.87265	-110.11662	*	Small Bubbling Spring	х				Travertine	Trav	N/A
RS092a	38.87023	-110.11190	*	Big Bubbling Spring	х				Entrada Sst	Vein	В
RS092b	38.87023	-110.11190	*	Big Bubbling Spring	х				Entrada Sst	Vein	В
RS093a	38.86717	-110.09952	*	Tenmile Butte	х				Entrada Sst	Vein	В
RS093b	38.86717	-110.09952	*	Tenmile Butte	Х				Entrada Sst	Vein	В
RS093c	38.86717	-110.09952	*	Tenmile Butte	Х				Entrada Sst	Vein	В
RS094	38.86272	-110.10125	*	Tenmile Geyser	Х				Travertine	Trav	N/A

	Green River					
	Unit 1.	Mt Fuel	Grand			
	(Amerada	Supply	Fault	Government	Salt Valley	Sharp
Well Name	Hess)	Geyser	14-24	Smoot #2	22-34	State #1
API	4301910030	4301930124	4301511182	4301916048	430191118	8 4301910817
Latitude	38.9331	38.8749	38.9661	38.8086	38.8563	38.8599
Longitude	-110.1307	-110.1128	-110.2262	-110.0668	-110.0341	-110.0621
Elevation (m)	1244	1259	1284	1311	1319	1372
Sample Form.	Navajo Sst.	Navajo Sst.	Navajo Sst.	Navajo Sst.	Navajo Sst	. Navajo Sst.
Start Depth (m)	445	381	640	195	137	149
End Depth (m)	539	430	765	274	293	216
Thickness (m)	94	49	125	79	155	67
Smpl Spcing (m)	3	3	3	3	3	6
Samples	7	6	9	6	12	5
Code	GR00X	MF00X	GF00X	GS00X	SV00X	SS00X
Well Name	Salt Wash #1	Silliman #1	Culburtson #1	Forest Gover	rnmnt #1 1	North Salt Wash
API	4301910831	4301910406	4301911521	4301510	)373	4301930282
Latitude	38.8087	38.9331	38.9409	38.88	37	38.8232
Longitude	-110.0390	-110.1410	-110.1221	-110.13	334	-110.0526
Elevation (m)	1310	1259	1349	1329	)	1352
Sample Form.	Navajo Sst.	White Rim	White Rim	Leadvi	lle	Leadville
Start Depth (m)	143	756	938	1685	5	2700
End Depth (m)	271	799	1026	1713	3	2705
Thickness (m)	128	43	88	28		5
Smpl Spcing (m)	6	3	2	2		1
Samples	9	6	6	4		4
Code	SW00X	SI00X	CU00X	FG00	х	NSW00X

**Table B.B-V** Details for petroleum exploration wells sampled in this study, including; well details, API No., localities, rock types and the intervals from which samples where collected. The 'code' at the bottom of each table is the generic sample code for that well.

## **B.5. Rock Isotope Data**

Table B.B-VI  $\delta^{18}O,\,\delta^{13}C$  and  $^{87}Sr/^{86}Sr$  for rock samples

		VSMOW	PDB	%		%			
Code	Location	δ <sup>18</sup> Ο	δ <sup>13</sup> C	Carbonate	<sup>87</sup> Sr/ <sup>86</sup> Sr	error	Lithology	у	Туре
RS001	Airport Well, east side of geyser	17.8	7.8		0.713342	7	Travertine	Trav	N/A
RS004	Airport Well, north side of geyser	16.7	6.6	97%			Travertine	Trav	N/A
RS005	Chaffin Ranch	20.9	9.1	98%			Travertine	Trav	N/A
RS006	Tenmile Geyser, west of vent	20.2	3.4				Travertine	Trav	N/A
RS007	Torreys Spring	20.7	8.3	76%			Travertine	Trav	N/A
RS020	San Rafael River		3.5	0%			White Rim	Rock	В
RS021	San Rafael Swell		0.1	0%			White Rim	Rock	В
RS024	San Rafael Swell		-1.0	5%			White Rim	Rock	R-B
RS026	Black Dragon Canyon		4.3	8%			Navajo Sst	Rock	R
RS027	Black Dragon Canyon		-3.1	6%			Entrada Sst	Rock	Y-B
RS029	Black Dragon Canyon		-2.9	5%			Entrada Sst	Rock	R
RS041	Black Dragon Canyon		-6.0	11%			Wingate Sst.	Rock	В
RS044	Black Dragon Canyon						Navajo Sst	Rock	R
RS045a	Black Dragon Canyon		-2.4	4%			Navajo Sst	Rock	R
RS045b	Black Dragon Canyon		-4.2	0%			Navajo Sst	Rock	R
RS046	Black Dragon Canyon						Navajo Sst	Rock	R
RS048	Near Big Bubbling Spring		3.3				Entrada Sst	Rock	Y-B
RS052a	Near Big Bubbling Spring	19.8	4.6	44%			Entrada Sst	Rock	Y-B
RS052b	Near Big Bubbling Spring	19.8	5.7	63%			Entrada Sst	Rock	Y-B
RS053	Tenmile Butte	21.2	-2.5	2%			Entrada Sst	Rock	В
RS054a	Tenmile Butte	18.7	6.1	89%			Entrada Sst	Vein	В
RS055	Tenmile Butte	18.8	6.2	65%			Entrada Sst	Rock	В
RS056a	Tenmile Butte	19.2	5.8				Entrada Sst	Vein	В
RS056b	Tenmile Butte	20.9	-2.4	7%			Entrada Sst	Rock	В
RS057	Tenmile Butte	20.0	-2.7	5%			Entrada Sst	Rock	В
RS058	Tenmile Butte	21.4	-1.9	5%			Entrada Sst	Rock	В

#### Table B.IV continued

		VSMOW	PDB	%		%			
Code	Location	δ <sup>18</sup> Ο	δ <sup>13</sup> C	Carbonate	<sup>87</sup> Sr/ <sup>86</sup> Sr	error	Litholog	y	Туре
RS059	Tenmile Butte	16.8	-4.4				Entrada Sst	Rock	R
RS060	Tenmile Butte		2.9	1%			Entrada Sst	Rock	R-B
RS061	Tenmile Butte	20.0	-2.2	4%			Entrada Sst	Rock	В
RS062	Tenmile Butte	21.6	-1.9	2%			Entrada Sst	Rock	В
RS063	Tenmile Butte	21.5	-2.4	6%			Entrada Sst	Rock	В
RS065	Tenmile Butte, southern cliff	19.9	-2.8				Entrada Sst	Rock	В
RS066	Tenmile Butte, southern cliff		-2.9	0%			Entrada Sst	Vein	В
RS067	Tenmile Butte, southern cliff	19.6	0.6	2%	0.712645	8	Entrada Sst	Vein	В
RS068	Tenmile Butte, southern cliff	20.5	-2.4	8%			Entrada Sst	Rock	В
RS069a	Tenmile Butte, southern cliff	18.7	5.8	91%			Entrada Sst	Vein	В
RS069b	Tenmile Butte, southern cliff						Entrada Sst	Vein	В
RS070	Tenmile Butte	20.5	4.6	43%			Entrada Sst	Vein	В
RS071a	Tenmile Butte	18.6	5.8	100%	0.713035	10	Entrada Sst	Vein	В
RS071b	Tenmile Butte	18.8	5.9	87%			Entrada Sst	Vein	В
RS071c	Tenmile Butte	18.5	5.7	96%			Entrada Sst	Vein	В
RS072	Tenmile Butte	18.7	5.9	61%			Entrada Sst	Vein	В
RS073	Tenmile Butte	20.7	-2.5	16%	0.711829	7	Entrada Sst	Rock	В
RS090a	Near Big Bubbling Spring	19.5	6.4	54%			Entrada Sst	Vein	R-B
RS090b	Near Big Bubbling Spring		6.6	49%			Entrada Sst	Vein	R-B
RS090c	Near Big Bubbling Spring		6.7	87%			Entrada Sst	Vein	R-B
RS090d	Near Big Bubbling Spring		6.6	111%			Entrada Sst	Vein	R-B
RS091a	Small Bubbling Spring	18.7	4.2	34%	0.712115	7	Travertine	Trav	N/A
RS091b	Small Bubbling Spring		5.0	44%			Travertine	Trav	N/A
RS092a	Near Big Bubbling Spring	19.7	6.1	62%			Entrada Sst	Vein	В
RS092b	Near Big Bubbling Spring		6.3	85%			Entrada Sst	Vein	В
RS093a	Tenmile Butte	18.2	5.3	52%			Entrada Sst	Vein	В
RS093b	Tenmile Butte		4.8	100%			Entrada Sst	Vein	В
RS093c	Tenmile Butte		4.9	103%			Entrada Sst	Vein	В
RS094	Tenmile Geyser	19.6	6.0	59%			Travertine	Trav	N/A

#### Table B.B-VII

		Thin				<i>(m)</i>	VSMOW	PDB	%
Code	Powder	Section	Location	Sample Description	Lithology	Depth	δ <sup>18</sup> Ο	δ <sup>13</sup> C	Carb
SV001	Х	Х	Green River Anticline	Salt Valley 22-34	Navajo Sst	137	20.0	-3.7	5.4%
SV002	Х	Х	Green River Anticline	Salt Valley 22-35	Navajo Sst	149	19.6	-3.4	7.1%
SV003	Х		Green River Anticline	Salt Valley 22-36	Navajo Sst	168	20.9	-3.1	5.9%
SV004	Х		Green River Anticline	Salt Valley 22-37	Navajo Sst	183	20.1	-2.9	9.6%
SV005	Х		Green River Anticline	Salt Valley 22-38	Navajo Sst	201	19.2	-3.2	12.1%
SV006	Х		Green River Anticline	Salt Valley 22-39	Navajo Sst	213	20.6	-2.8	17.4%
SV007	Х		Green River Anticline	Salt Valley 22-40	Navajo Sst	229	19.6	-3.4	10.2%
SV008	Х		Green River Anticline	Salt Valley 22-41	Navajo Sst	241	19.8	-2.9	8.4%
SV009	Х	Х	Green River Anticline	Salt Valley 22-42	Navajo Sst	259	22.5	-2.3	10.4%
SV010	Х		Green River Anticline	Salt Valley 22-43	Navajo Sst	274	22.7	-2.2	12.0%
SV011	Х	Х	Green River Anticline	Salt Valley 22-44	Navajo Sst	290	21.0	-2.6	16.0%
SV012			Green River Anticline	Salt Valley 22-45	Navajo Sst	305			
SW001	Х		Green River Anticline	Salt Wash #1	Navajo Sst	143	23.0	-2.8	
SW002	Х		Green River Anticline	Salt Wash #1	Navajo Sst	158	20.8	-3.3	
SW003	Х		Green River Anticline	Salt Wash #1	Navajo Sst	174	21.8	-3.1	
SW004	Х		Green River Anticline	Salt Wash #1	Navajo Sst	189	21.0	-2.9	
SW005	Х		Green River Anticline	Salt Wash #1	Navajo Sst	204	21.7	-2.1	
SW006	Х		Green River Anticline	Salt Wash #1	Navajo Sst	219	20.6	-3.4	
SW007	Х		Green River Anticline	Salt Wash #1	Navajo Sst	235	22.8	-2.7	
SW008	Х		Green River Anticline	Salt Wash #1	Navajo Sst	250	22.0	-3.0	
SW009	Х		Green River Anticline	Salt Wash #1	Navajo Sst	265	21.1	-3.4	

#### **B.6.** Point Counting Data: Entrada Sandstone

**Table B.B-VIII** Point count estimates (expressed as vol% of thin section) for major mineral phases in Entrada Sandstone Samples averaged over 200 counts perslide. Abbreviations: Qrtz = Quartz, Otz Ovgrth = Quartz Overgrowth, Feld = feldspar, Dol = dolomite, Cc = calcite, Hem = hematite cryptocrystalline, CrysOxides = coarse Fe-oxides, Illite Coat = illite grain coating, Illite Pore = pore filling illite, Kaol = kaolinite, Poro = porosity

	vol% of slide									<b>T11</b>		
Sample	Туре	Qrtz	Qtz Ovgrth	Feld	Dol	Cc	Hem	Crys Oxide	Illite Coat	lliite Pore	Kaol	Poro
RS057	В	71.9	3.3	4.1	2.6	7.3	0.1	0.9	1.4	2.1	0.3	5.9
RS073	В	73.9	2	3.7	3.7	12.2	0.2	1.1	1.8	0.8	0.6	0.8
RS062	В	67.7	1.5	6.2	4.3	7.7	0.3	0.6	1.1	1.4	1.1	8.1
RS061	В	70.9	2.1	9.8	3.2	4.8	0.4	2.3	0.3	0.7	0.4	5.1
RS058	В	69.5	1	7.3	2.8	8.9	0.1	1.3	3.2	1.6	3.3	1.5
RS027	R	73.9	0.2	9.1	4.5	0.1	1.3	0.1	1.7	1.7	0.3	7.9
RS029	R	70.4	0	10.4	10.6	0	1.1	0	1.8	1.3	0.1	3.4
RS069	Y-B	66.2	3.2	5.4	0.2	16.6	0.1	1.8	1.8	1.3	0.8	3.2
RS052	Y-B	67.3	2.6	5.6	0.4	13.5	0.6	3	1.9	0.9	0.5	4
RS090	Y-B	62.9	1.5	8.6	0.1	10.9	0.5	2.9	1.6	2.5	0.2	10

<b>B.7.</b> Aragonite	Vein	Isotope	Data	
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Table B-IX Aragonite vein isotope data, travertine volumes and distance along fault trace from most									
westerly (up groundwater flow direction) travertine, for Salt Wash Graben and Little Grand Fault.									
Distance									

Sample/Travertine	Age	σ	Along Fault	Travertine Volume	<sup>87</sup> Sr/ <sup>86</sup> Sr	σ	δ <sup>13</sup> C	δ <sup>18</sup> Ο
Salt Wash Cash an	(ka)	(ka)	( <i>km</i> )	$(m^3)$			(PDB)	(VSMOW)
Sau wasn Graden	0.11	0.63	2.04	9162				
SW1 SW2	4.70	0.03	3.94	8102 2741				
SW2	4.79	0.05	5.88	2041				
SWJ SWJ	9.75	0.03	J.88 1.76	2041				
SW4 SW5	13.07	0.04	1.70	7081				
SW 03 52K	28.38	0.00	1.40	1275	0 712812	1 /E 05	5 74	18.02
SW6	28.58	0.24	0.00	1700	0.712012	1.41-05	5.74	10.92
SW 06 27 A	51 20	0.10	1.64	1700	0 712851	1 /E 05	5.61	10.22
SW7	57.01	0.23	2 70	6802	0.712031	1.41-05	5.01	19.22
SW03 65N	60 10	0.41	2.70	10101	0 712872	1.6F.05	5 87	10 10
SW8	65.09	0.44	2.04	9353	0.712072	1.01-05	5.67	19.19
SW 03 56H	03.07 02.70	1.12	1.63	10203	0 713019	1.6E-05	5 40	18 64
SW06 17D	100 38	0.56	1.05	5510	0.712047	1.6E-05	5.40	18.04
SW 06 18C	106.09	0.30	1.44	6122	0.712947	1.0E-05	5.16	18.47
SW02 361	112.80	0.42	3 23	14879	0.712213	1.4E 05	5.63	19.54
SW9	116.79	0.69	4 07	1700	0.715175	1.01 05	5.05	17.51
SW10	130.67	0.83	3 39	20406				
SW 06 19C	135.14	1 14	1 50	5986	0 712834	1 4E-05	4 64	17 76
SW 06 22 A	291 31	5 59	1.36	816	0.712979	1.1E-05	6.13	20.16
SW.06.16B	413.47	15.13	1.40	6122	0.712998	1.4E-05	5.00	21.01
Little Grand Fault								
LG1	5.03	0.04	0.00	240				
LG.03.50A	5.06	0.04	0.22	2047	0.712731	1.4E-05	5.19	17.87
LG.03.510	27.41	0.08	0.66	1588	0.712703	1.6E-05	5.61	19.13
LG2	31.22	0.08	0.66	36				-,
LG3	49.09	0.30	0.66	335				
LG4	50.89	0.32	1.62	388				
LG.03.48F	58.80	0.40	2.89	10213	0.712680	1.4E-05	5.71	18.63
LG5	75.50	0.46	0.42	1621				
LG.03.42AX	106.00	0.50	0.50	69660	0.712750	1.4E-05	5.99	18.48
LG.03.42AF	109.00	0.50	1.55		0.712883	1.8E-05	5.20	17.36
LG.03.42AD	113.91	0.60	1.70		0.712907	1.4E-05	4.76	16.99
LG6	9.48	0.04	0.22					
LG7	103.17	0.50	0.66					

# Appendix C Eh-pH Diagrams

#### C.1. Calculation of Mn-oxyhydroxide solubility

Fluid-mineral equilibrium with 'typical' well crystalline Mn-oxyhydroxide suggests that Mn<sup>2+</sup> concentrations in groundwater at any given Eh and pH should be much higher than  $Fe^{2+}$ , but this is rarely observed. It has commonly been noted that when Mn<sup>2+</sup> and Fe<sup>2+</sup> solution concentrations for typical clastic and carbonate groundwater systems are superimposed on their respective activity contours the redox conditions defined from the Mn content (assuming equilibrium with a 'typical' Mn-oxyhydroxide) do not coincide with those defined on the basis of Fe (e.g. Barnaby and Rsimstidt, 1989; Edmunds et al., 1986). A similar phenomenon is observed in CO2-charged fluids suggesting that groundwaters are not in equilibrium with any of the Mn-oxyhydroxide phases considered in construction of typical Eh-pH stability diagrams. This could reflect a) the absence of a true Mn-oxyhydroxide phase 2) disequilibrium between porewater Mn<sup>2+</sup> and Mnoxyhydroxides 3) pore waters are in equilibrium with Mn-oxyhydroxides of different thermodynamic stability than those used to construct stability diagrams. Given the ubiquitous presence of Mn-oxyhydroxide minerals in sedimentary environments (1) is unlikely (e.g. Bricker, 1965; Potter and Rossman 1979). The compatibility with measured aFe<sup>2+</sup>, pH and Eh with know Fe-oxyhydroxides suggests equilibrium is maintained. Thus (3) seems the most likely explanation given the variable composition, crystallinity and thermodynamic stability of naturally occurring Mn-oxyhydroxide minerals.

Manganese chemistry in natural systems is complex and not well understood. Mn exists in several possible oxidation states and commonly forms complex nonstoichiometric oxyhydroxides, with highly variable crystallinity (Ponnamperuma *et al.*, 1969). Detailed studies of Mn oxide mineralogy from various sedimentary environments indicate that Mn oxides other than pyrolusite (MnO<sub>2</sub>) are dominant (see

Taylor *et al.*, 1964). Consequently it is valid to assume that  $Mn^{2+}$  concentrations are controlled by equilibrium with a relatively insoluble 'complex' MnO<sub>2</sub> phase.

The thermodynamic stability of the Mn-oxyhydroxides governing  $Mn^{2+}$  solubility in the CO<sub>2</sub> charged fluids can be evaluated by estimating the *apparent* standard free energy of formation of a *hypothetical* Mn-oxide phase in equilibrium with the CO<sub>2</sub> charged fluids using the Nernst equation, measured fluid  $aMn^{2+}$ , pH and assuming Ptelectrode-measured Eh potentials approximate the actual Eh. Assuming the controlling redox reaction;

$$MnO_2 + 4H^+ + 2e^- \leftrightarrow Mn^{2+} + 2H_2O \tag{C.1}$$

For which the equilibrium constant  $(K_{MnO2})$  can be written as;

$$K_{MnO_2} = \frac{a_{Mn^{2+}} \cdot a_{H_2O}^2}{a_{H^+}^4 \cdot a_{e^-}^2}$$
(C.2)

Where  $Eh = 10^{-a_{e^-}}$  (C.3)

And using the Nernst equation

$$\Delta E^{\circ} = \frac{RT}{nF} \ln[K] \tag{C.4}$$

The apparent standard state free energy of formation can be defined as

$$\Delta G_f^{\circ} = -nF\Delta E^{\circ} \tag{C.5}$$

Where  $\Delta E^{\circ}$  is the standard state cell potential, *n* is the number of electrons involved in the reaction, *F* is the Farady constant, *R* is the gas constant and *T* is temperature (°K). This yields an average estimated  $\Delta G_f MnO_2 = -144640$  kJ mol<sup>-1</sup>. Stability diagrams constructed using this estimated  $\Delta G_f$  (Fig. C.1-1) demonstrate that the Mn<sup>2+</sup> activity contours are depressed towards more reducing conditions and define Eh conditions consistent with those predicted from the iron equilibria discussed in Chapter 2 section 2.4.7.



**Figure C.1-1** Eh-pH stability fields for the important Mn-oxyhydroxides in typical clastic aquifers, at  $25^{\circ}$ C,  $\log(Mn_{TOT})$ =-3 and -4. Calculated using CHNOSZ (Dick, 2008). MnO<sub>2</sub>,cplx is the *hypothetical* Mn-oxide phase whose solubility has been calculated from measured spring pH, Eh and Mn concentrations.